




STEP AP209 ed2 Linear Static Structural FEA Handbook

 Volume 1: FEA Input for
LOTAR EAS Pilot Study #1

LOTAR
LONG TERM ARCHIVING AND RETRIEVAL

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Trademark Acknowledgments

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VERSION LOG

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1 Introduction

This document is a handbook describing the finite element models (FEM) used for the LOTAR International Engineering Analysis and Simulation (EAS) pilot studies. These pilot studies focused on development of converter implementations of the International Standards Organization (ISO) 10303-209 ed2 (AP209 ed2) Standard, one Part of the 10303 family of Standards commonly known as STEP (Standard for The Exchange of Product data). The implementations were subsequently used to generate AP209 ed2 STEP files used as input to the initial test round of the Computer Aided Engineering Implementer Forum (CAE_IF) .

This handbook can also be used as training material for an introduction to the AP209 ed2 data model for finite element models. The document requires at least a cursory understanding of the Finite Element Method, finite element models and the information technologies involved in applying the AP209 ed2 application protocol. Familiarity with the details of the EXPRESS data modeling language and fundamental concepts of the STEP standard parts are not necessarily a prerequisite for using this document, but will greatly improve the readers understanding. The handbook can also help the reader focus on those parts of STEP needed to encode FEM information and the documentation resources available to producers, consumers and implementers of this information.

2 Pilot Study Overview

The pilot study was created to encourage software providers to participate in an initial effort to develop commercial tools capable of converting traditional finite element model information, expressed in solver ASCII format, to the AP209 ed2 format. A second goal of the pilot study was to produce a reference set of AP209 ed2 STEP files that have been validated with the AP209 ed2 EXPRESS schema and have been checked for semantics with respect to the Recommended Practices for AP 209 ed2 10303-209:2014 and the document, Geometric Founding and Associativity in ISO 10303-209, Rev. B, 2/15/2001.

The pilot study provides a small test suite of FEA models to be translated from a native solver format, in this case NASTRAN, to the STEP AP209 ed2 ASCII file representation (Part 21). These models are prismatic beam models with various linear element types, boundary conditions, load cases, and output requests. The overall geometry for each model is the same and is simple (see Figure 1). This simplicity was intentional to focus the effort on the interpretation of the FEM definitions and constructs, not the geometric abstractions related to meshing techniques.

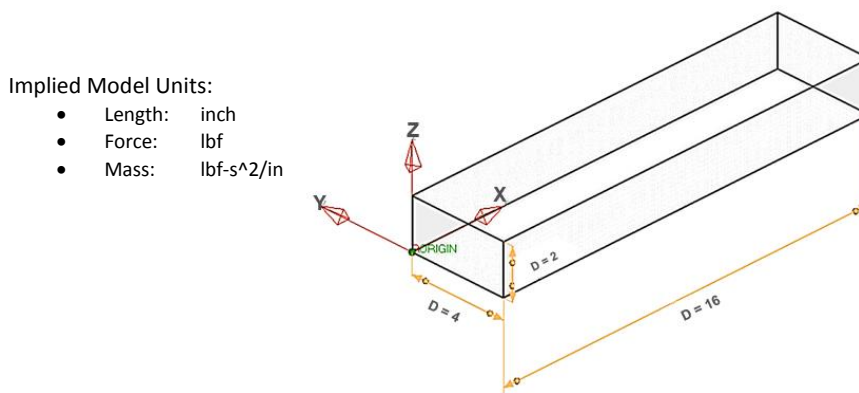


Figure 1 Pilot Model Geometry

Discretization of the geometry to the finite element model domain was accomplished through the abstractions and resulting finite element models shown in Figure 2. The finite element models were exported in NASTRAN bulk data format for use in this pilot study.

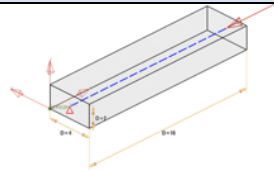
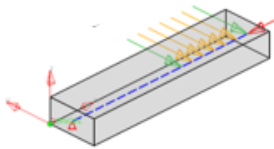
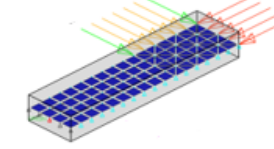
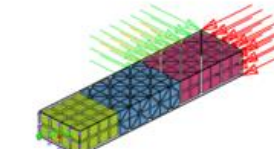
Abstraction - Geometry	NASTRAN Element Type	Pilot Model
1 Dimensional - Line	Linear CROD [Axial Stiffness – 1 DOF]	
1 Dimensional - Line	Linear CBAR [Bending/Axial/Shear – 5 DOF]	
2 Dimensional - Surface	Linear CQUAD4/CTRIA3 [Bending/Membrane/Shear – 5 DOF]	
3 Dimensional - Solid	Linear CHEXA/CPENTA/CTETRA [Bending/Membrane/Shear – 3 DOF]	

Figure 2 Pilot Model Abstractions

The boundary conditions of the pilot models were established so that there is no constraint to Poisson’s expansion or contraction. This modeling of the boundary conditions was used to model correctly the classical solution of the bar in compression and bending. This is critical to having a ‘correct’ solution easily available to check the analysis results.

The first load case for all of the pilot models is a simple axial compression case where the compression loads are kinematically consistent. The deflection and stress of the beam are calculated by the following formula:

$$\text{Stress} = \text{Load}/\text{Cross-sectional area}$$

$$\text{Strain} = \text{Stress}/\text{Modulus of Elasticity}$$

$$\text{Axial Deflection} = \text{Strain} * \text{Length}$$

In the remainder of this document each pilot model is discussed in detail, where complete listings of the solver input and the STEP output are included in the Appendices.

3 AP209 Overview

This section introduces several of the information technologies used in working with the STEP standard, and in particular those standards used via AP209 ed2. The reader can use this introduction to locate and explore in detail the topics highlighted herein. The links provided in Section 9 References and Links are a good starting place for additional reading.

AP209, formally known as ISO-10303-209 ed2, Application Protocol: Multidisciplinary Analysis and Design, provides the data structures for the exchange of part and configuration identification with configuration control data, with or without associated 3D part model information. AP209 was developed under the auspices of the International Organization for Standardization (ISO), Technical Committee 184, Sub-Committee 4, and is one of a series of parts comprising the full STandard for the Exchange of Product model data (STEP) standard known as ISO 10303.

3.1 STEP Module and Resource Library

Application Protocols such as AP209 ed2 are published in HTML format. All STEP Application Protocols are built from common modules in the SMRL (STEP Module and Resource Library) thus assuring integration and interoperability. The HTML format provides a convenient web browser format to locate definitions for all the entities, types and rules needed for this pilot study, along with the associated EXPRESS schemas. These documents are copyrighted and published by ISO, so therefore the reader is referred to the ISO web site for access information.

The SMRL contains all the 10303 STEP standards other than the Application Protocols themselves, and consists of the following 10303 Parts:

- Integrated resources series of parts: ISO 10303 Parts 41 to 112;
- Application modules series of parts: ISO 10303 Parts 401 to 499 and 1001 to 1999;
- Application interpreted constructs series of parts: ISO 10303 Parts 501 to 599;
- Logical model of expressions: ISO 13584 Part 20;
- Business object models series of parts: ISO 10303 Parts 3001 to 3099.

The initial architecture of ISO 10303 did not use the Application Modules in SMRL. That architecture was more monolithic and resulted in consistency issues as the standards grew in scope. The Application Modules SMRL architecture was introduced to solve these scalability issues.

As shown in Figure 3, AP209 ed2 is a modular STEP standard focused on multidisciplinary analysis and simulation information, along with related design (primarily shape) and PDM/PLM information. As such, it is built from smaller building blocks such as application modules which are used to form a multi-layered set of schema definitions.

STEP Module and Resource Library

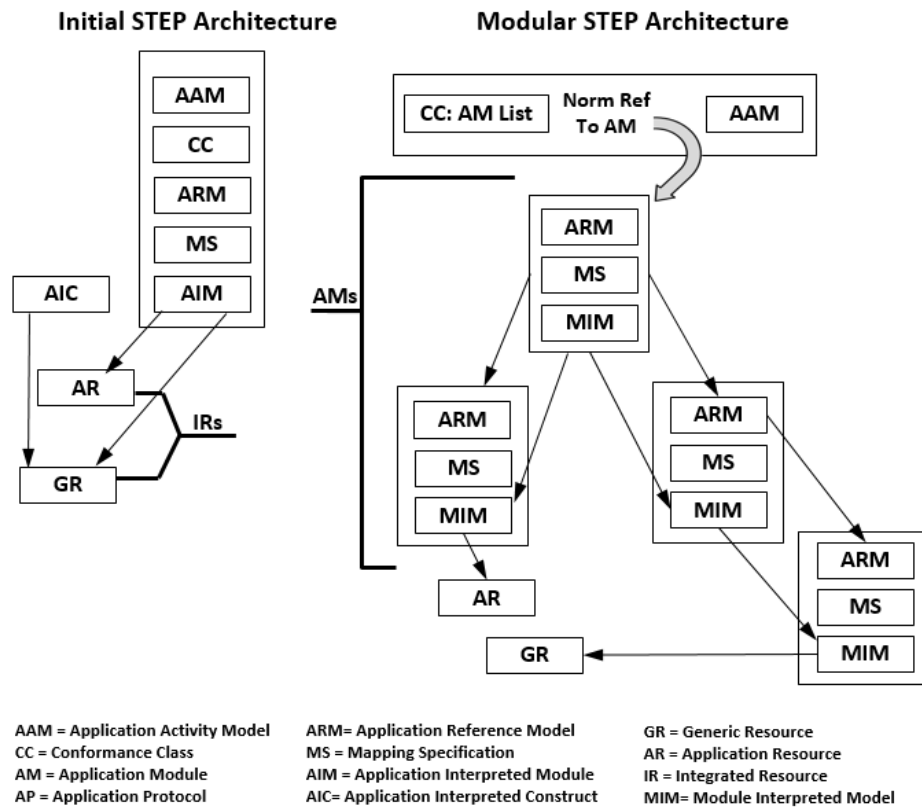


Figure 3 Evolution of the STEP Architecture and Current SMRL

These building blocks are documented in the SMRL Part documents. The schemas in these building blocks are defined using the EXPRESS schema modeling language (Part 10303-11). In this document, EXPRESS schema fragments are presented that relate to the specific constructs used for each pilot model.

A fundamental concept of the STEP architecture is the use of various higher level data models that are mapped to lower level data models. This concept is illustrated in Figure 3 and in the AP209 ed2 Recommended Practice discussion of how standards support the user community needs. This is accomplished by documenting the flow of the everyday engineering actions put forth in the AP209 ed2 Application Activity Model (AAM) using data elements defined in the Application Reference Model (ARM). The ARM documents these information requirements in terms of the application experts vernacular. The ARM is in turn tied by mappings to the constructs in the Integrated Resources to create the interpreted Application Model (AIM). The AIM EXPRESS model is used to implement the physical data sharing, typically by using the implementation format specified by the 10303-21 clear text (ASCII) encoding.

The ARM and AIM data model schemas are related to each other through mapping specifications that are accessible in the SMRL. There is no discussion of the mapping specifications in this document. The schema fragments used in this document are all AIM schema definitions.

There are two views of the AP209 ed2 ARM and AIM schemas that are available: a short form and a long form. A short form schema includes all the building blocks through the recursive 'USE FROM' EXPRESS construct that references other modular building blocks. The long form view is the result of resolving all the references and concatenating the resulting schema constructs into a single schema file. Both are available in the SMRL. The short form of AP209 ed2 is shown in Figure 4. Note that the first line includes the AP 242 standard in its entirety. Also note that only the AIM long form EXPRESS schema is used for implementations.

```

SCHEMA Ap209_multidisciplinary_analysis_and_design_mim;
  USE FROM Ap242_managed_model_based_3d_engineering_mim; -- ISO/TS 10303-442
  USE FROM Analysis_assignment_mim; -- ISO/TS 10303-1474
  USE FROM Analysis_characterized_mim; -- ISO/TS 10303-1475
  USE FROM Analysis_identification_mim; -- ISO/TS 10303-1476
  USE FROM Analysis_product_relationships_mim; -- ISO/TS 10303-1373
  USE FROM Analysis_mim; -- ISO/TS 10303-1372
  USE FROM Analysis_representation_mim; -- ISO/TS 10303-1785
  USE FROM Cfd_model_mim; -- ISO/TS 10303-1377
  USE FROM Finite_elements_mim; -- ISO/TS 10303-1383
  USE FROM Mesh_connectivity_mim; -- ISO/TS 10303-1384
  USE FROM Mesh_topology_mim; -- ISO/TS 10303-1386
  USE FROM Product_analysis_mim; -- ISO/TS 10303-1387
  USE FROM Analysis_shape_mim; -- ISO/TS 10303-1374
  USE FROM Finite_element_shape_mim; -- ISO/TS 10303-1382
  USE FROM Cfd_specified_general_property_mim; -- ISO/TS 10303-1379
  USE FROM Fea_definition_relationships_mim; -- ISO/TS 10303-1380
  USE FROM Fea_material_aspects_mim; -- ISO/TS 10303-1769
  USE FROM Cfd_equations_mim; -- ISO/TS 10303-1376
  USE FROM Cfd_results_mim; -- ISO/TS 10303-1378
  USE FROM Finite_element_analysis_mim; -- ISO/TS 10303-1381
  USE FROM Mesh_function_mim; -- ISO/TS 10303-1385
  USE FROM mathematical_functions_schema; -- ISO 10303-50
  USE FROM iso13584_generic_expressions_schema; -- ISO 13584-20
  USE FROM iso13584_expressions_schema; -- ISO 13584-20
  USE FROM Part_view_definition_mim; -- ISO/TS 10303-1023
  USE FROM Collection_identification_and_version_mim; -- ISO/TS 10303-1396
  TYPE ap209e2_analysed_item <details removed for clarity> END_TYPE;
  TYPE ap209e2_analysis_approval_item <details removed for clarity> END_TYPE;
  TYPE ap209e2_analysis_identification_item <details removed for clarity> END_TYPE;
  TYPE ap209e2_groupable_item <details removed for clarity> END_TYPE;
END_SCHEMA; -- Ap209_multidisciplinary_analysis_and_design_mim

```

Figure 4 ISO 10303 AP209 ed2 Short Form Schema

3.2 External Physical File – Part 21

As noted above, the typical way to externalize an AP209 ed2 data model instance is via a physical file that is an ASCII encoding of the data based on the EXPRESS constructs in AP209 ed2 mapped through ISO 10303-21 (see Figure 5).

```

/*****
* STEP Physical File Fragment
*****/
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,CARTESIAN,'FEA_BASIC_COORD_SYSTEM.0');
#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));

```

Figure 5 STEP Physical File Fragment (Part 21)

This physical file format is called a Part 21 STEP file. The reader is referred to the ISO 10303-21 document for complete syntax rules. Basic syntax rules will be introduced as needed in the context of the pilot model being discussed. The pilot models in this document are all encoded as Part 21 STEP files. Validation of the contents of these STEP files is accomplished by reading the Part 21 files into tools that can assess adherence to the underlying schema definitions and/or semantics.

4 AP209 ed2 Data Model Organization

Due to the large scope of the Standard, the AP209 ed2 schema is large and complex. Many views of the data model are presented in the application protocol (AP209 ed2) and recommended practices (RP) documents. In addition to the figures in the RP, Figure 6 shown below illustrates refinements of the RP information to show how the data model can be considered as smaller conceptual topics and how those topics are related to the pilot models.

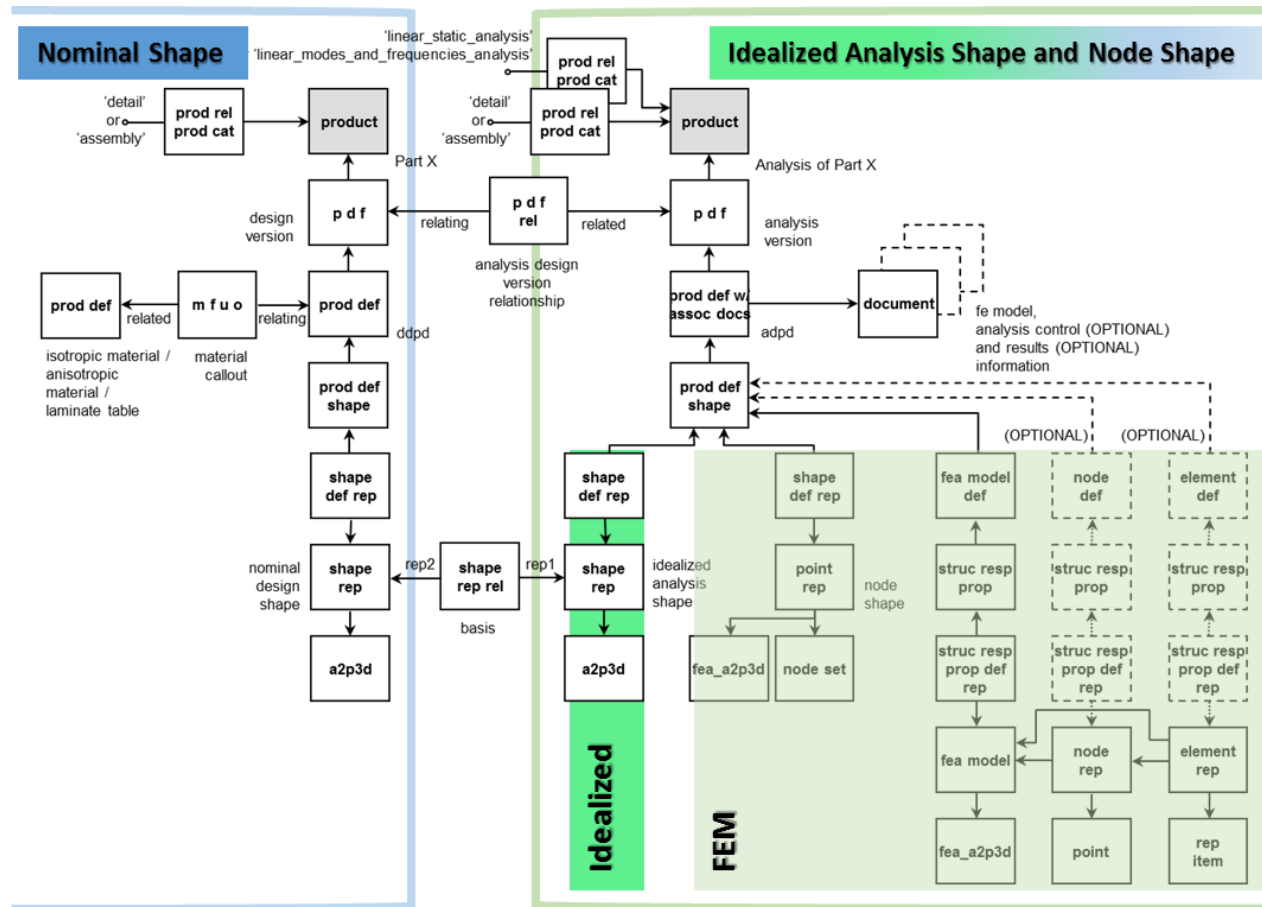


Figure 6 AP209 ed2 Relationship Between Design and Analysis

This view clearly illustrates how the design geometry (nominal shape) is related to the abstracted analysis geometry (idealized analysis shape) and the finite element model (node shape).

The pilot models in this Handbook use a native solver format (NASTRAN) as the FEM information source and therefore no nominal design or idealized analysis geometry is captured. However, the tools being

developed under this pilot study will eventually be required to include the AP209 ed2 constructs that are used to capture the full FEA model definition and solution results. Full FEA model definition includes associativity to nominal design geometry or the idealized analysis geometry used for mesh generation and for loads and boundary condition specifications.

Traditionally, FEA solver models do not specify a system of units but are required to be internally consistent. Recent practices have begun to define explicitly a consistent set of units as part of the solver input for FEA model definition. The STEP standard can capture this information when constructing model contexts and associated unit entities. The pilot models do not explicitly specify a system of units, however, there is an implied use of the English inch-pound force-second system due to the existence of recognized material property values. While it may be possible to deduce a likely system of units for a given input file, it is recommended that direct user input define explicitly which system of units applies. How to specify this information for the conversion process is an active area of development and discussion.

4.1 Analysis Product Metadata

The right side of Figure 6 represents the AP209 ed2 analysis product. The figure hides many entities that deal with metadata about the product for the sake of clarity. Figure 7 includes more of these entities and categorizes the metadata of the analysis product; this figure was created from an early STEP file generated for the pilot study using the 1st pilot model.

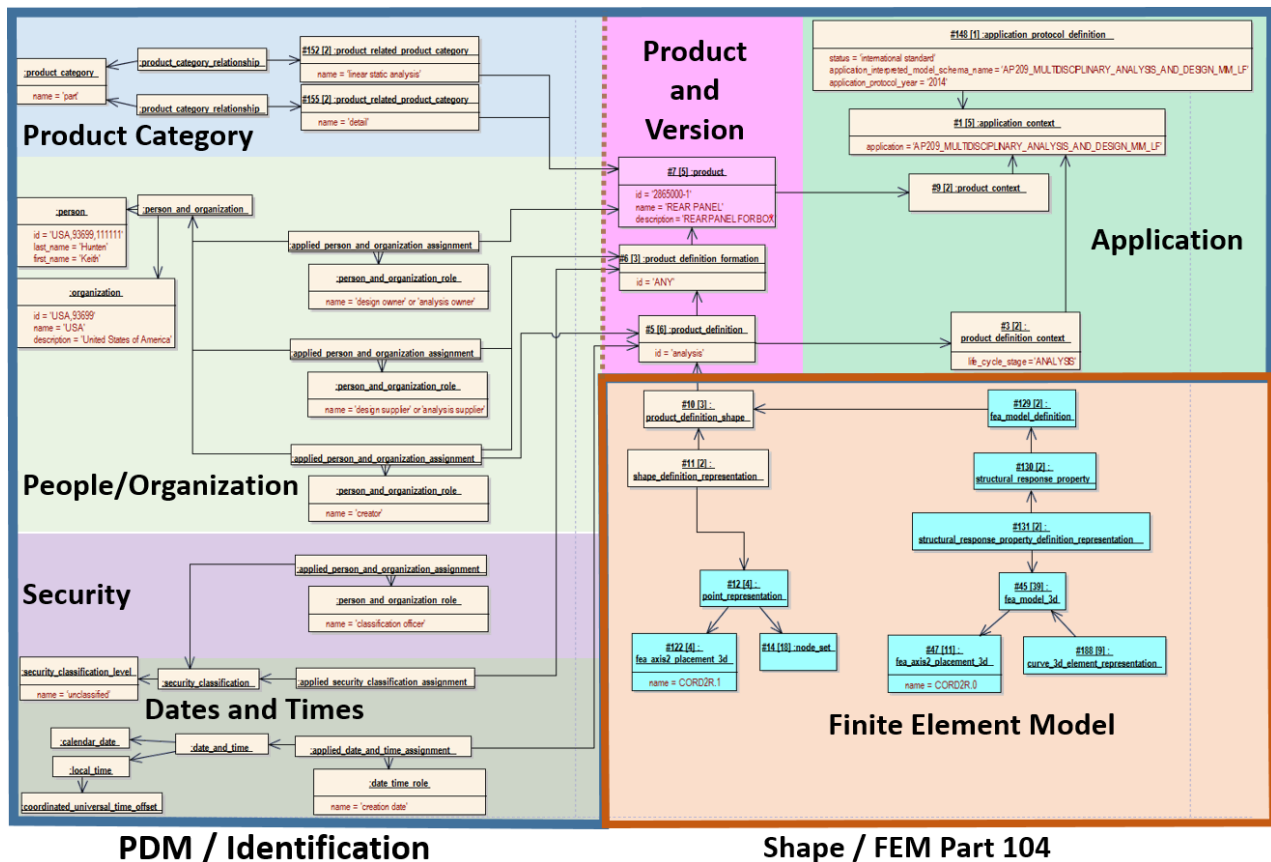


Figure 7 AP209 ed2 Analysis Product Categories

The ‘PDM/Identification’ area of Figure 7 represents much of the metadata that is used to understand the pedigree of the analysis product. Metadata such as who authored it, who owns it, who reviewed and approved it, security and retention statements and important dates can be defined here. None of this information will be directly available from the NASTRAN solver decks used as the information source for the pilot project. However, the metadata can either be supplied by the conversion process or defaulted to a minimal set sufficient for further workflow processing.

An important characteristic to note about Figure 7 is that all the instances of ‘PDM/Identification’ metadata point inward to the entities contained in the ‘Product and Version’ area. This implies that from an EXPRESS entity definition point of view, all the ‘PDM/Identification’ entities are optional. While some commercial CAD tools offer options to specify these entities in the tool’s graphical user interface (GUI), if the option is not selected, the AP242 STEP file written will not contain this information. This produces a well-formed STEP file, but it is not semantically correct and complete.

This information may appear optional by looking only at the referencing direction, but the EXPRESS definition may also include rules which require existence of these entities. Additionally, the AP209 ed2 Recommended Practices documentation may dictate that these entities should exist and may provide enumerations of acceptable attribute values.

The ‘Product Category’ area of Figure 7 illustrates this requirement. The EXPRESS schema fragment from the AP209 ed2 long form for the Product_Category entity is shown in Figure 8. These entities are defined in the ISO 10303-41 Integrated generic resource: Fundamentals of product description and support (Part 41).

```

ENTITY Product_Category;
    name          : Label;
    description   : OPTIONAL Text;
    DERIVE
        id : Identifier := Get_Id_Value( SELF );
    WHERE
        wr1: ( SIZEOF( USEDIN( SELF, 'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' +
ID_ATTRIBUTE.IDENTIFIED_ITEM' ) ) <= 1 );
END_ENTITY;

ENTITY Product_Category_Relationship;
    name          : Label;
    description   : OPTIONAL Text;
    category      : Product_Category;
    sub_category  : Product_Category;
    WHERE
        wr1: Acyclic_Product_Category_Relationship( SELF, [SELF.sub_category] );
END_ENTITY;

ENTITY Product_Related_Product_Category
    SUBTYPE OF ( Product_Category );
    products      : SET [1 : ?] OF Product;
END_ENTITY;

```

Figure 8 EXPRESS Schema for Product Category and Related Entities

The relationship object enables a hierarchy of product category information to be specified for any product. The Product_Category super-type only requires the ‘name’ attribute be present while the Product_Related_Product_Category sub-type requires a reference to at least one Product. In addition to these structural requirements, the AP209 ed2 Recommended Practice states:

- [Section 2.8.2.2] – “It is strongly recommended that all implementations of AP 209 ed2 establish an instance of **product_category** with a **name** attribute value of `'part'`.”
- [Section 2.11.1.1] – “AP 209 ed2 requires that all **products** exist in at least one **product_related_product_category**. This restriction (**product_requires_product_category**) forces all parts into one of the following categories: `'detail'`, `'assembly'`, `'inseparable assembly'`, or `'customer furnished equipment'`.”
- [Section 2.11.1.1] – “An analysis **product** should also be assigned to a **product_related_product_category** that indicates the type of analysis. The appropriate categories in AP 209 ed2 are: `'linear static analysis'` and `'linear modes and frequencies analysis'`.”

The EXPRESS schema and recommended practice declarations translate to a structure that at a minimum should look like the instance diagram shown in Figure 9 with the ‘name’ attribute being populated as shown.

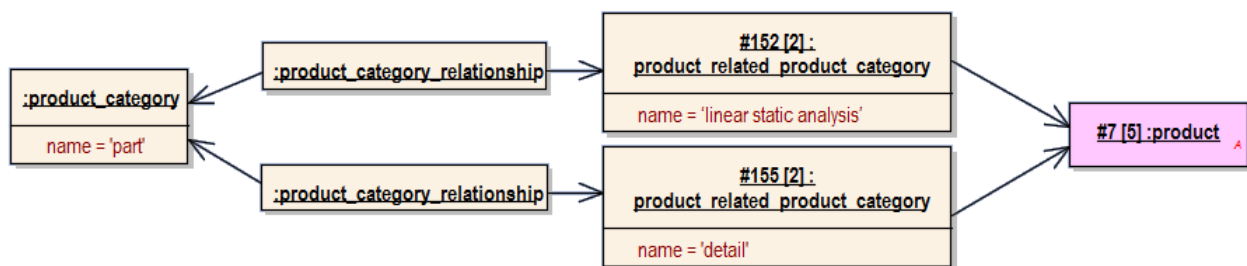


Figure 9 Product Category Instance Diagram

For the pilot study, a minimal set of metadata should be included but is not the primary focus. It is discussed in this handbook to introduce how the implementation requirements are expressed in the schemas and recommended practice, and the inherent problem with using native solver information as the source for the ‘PDM/Identification’ metadata.

4.2 Application Protocol and Analysis Product Identification

Identification of the data model and the analysis product itself are accomplished using the same methods as a typical part design product. The application protocol definition and application context define the schema used to construct the data model, whereas the product and related product definition entities provide for identification and independent versioning of the analysis product. Again, the recommended practice document provides guidance as to how these entities should be populated. To summarize:

- The **application_context** entity identifies the application that defines the data. The **application** attribute, based on its definition in ISO 10303-41, should have the value `'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF'`
- The **application_protocol_definition** entity further identifies the AP. For AP 209 ed2, the **status** attribute, based on its definition in ISO 10303-41, should have the value `'international standard'`. The **application_interpreted_model_schema_name** attribute should have the value `'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF'` and the **application_protocol_year** attribute should have the value `'2014'`
- The **product** should contain identifying information about the part being analyzed

- The **product_definition_formation** should contain a unique identifier or the string '**ANY**' if it is a generic un-versioned part or analysis
- The **product_definition** should have an identifier populated with the string '**analysis**'

All these constructs are included in AP209 ed2 through the EXPRESS 'USE FROM' statement and are defined in ISO 10303-41 Integrated generic resource: Fundamentals of product description and support (Part 41). As noted above the USE FROM technique enforces the common use of the data constructs in the Integrated Resources amongst all Application Protocols providing interoperability.

Unlike metadata discussed in the prior section of this handbook, these elements of the AP209 ed2 standard are not optional and must be included for a STEP file to be valid. Figure 10 illustrates a sample instance diagram.

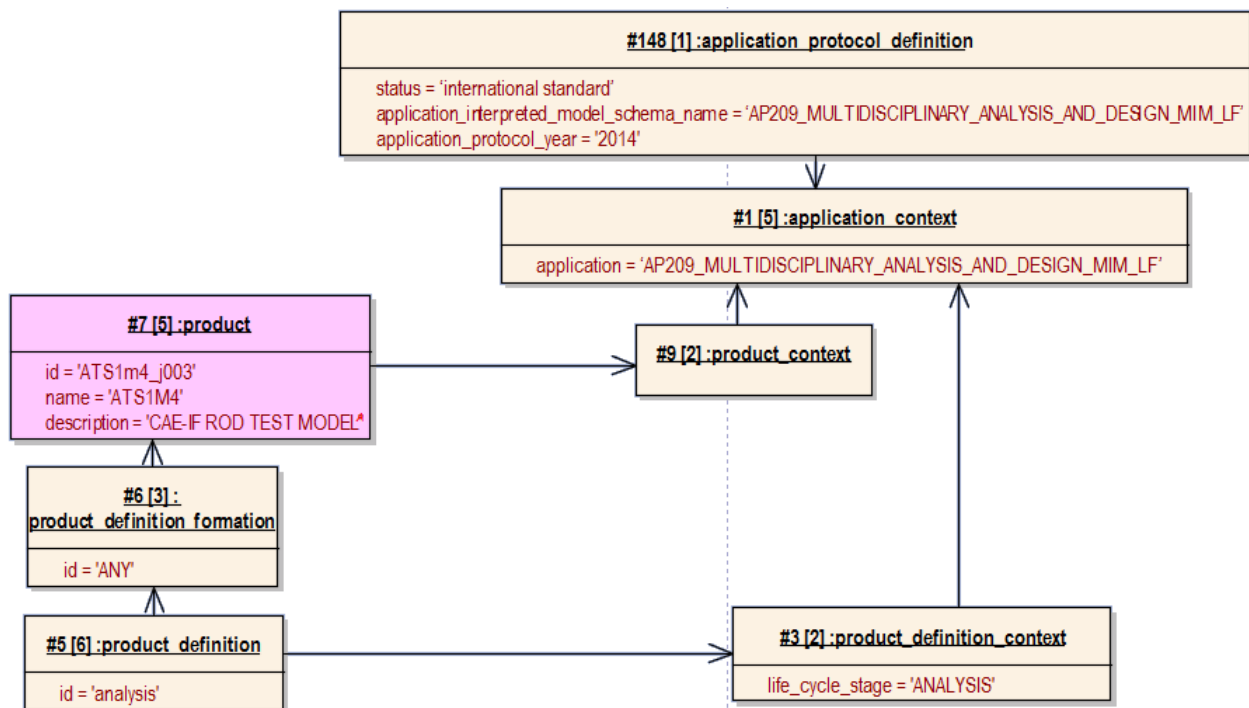


Figure 10 Example Analysis Protocol and Product Identification

There are other aspects of the product information that can be expressed with the AP209 ed2 standard such as the details of all the possible captured metadata, but that is not the focus of this document or the pilot study. The preceding discussion is only an introduction to the topics and the reader is encouraged to refer to the actual standard documents and recommended practices for complete coverage.

The remainder of this document focuses on the lower right corner of Figure 7; it captures the definitions of the finite element pilot models. The contents of this part of the data model are documented in detail in the ISO 10303-104 Integrated application resource: Finite element analysis document (Part 104). Part 104 and the associated schema definitions are the primary sources of information needed to map the

native solver information (NASTRAN) found in the pilot project input files, to the AP209 ed2 data models and produce the familiar Part 21 STEP file representation.

Each pilot model is discussed in a similar format. For each topic, such as grid points, an instance diagram is shown to illustrate how the information appears in the AP209 ed2 data model, followed by the source NASTRAN information, and then the STEP file entities listed along with the related AP209 ed2 schema fragments.

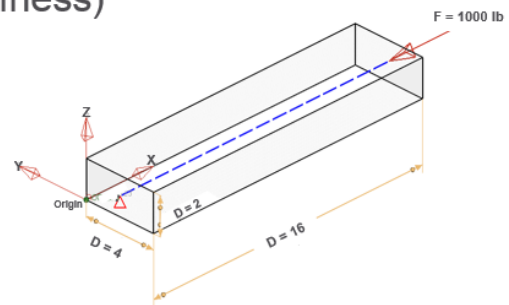
5 Pilot Model ATS1 – 1D Rod Element

The ATS1 pilot model composition is illustrated in Figure 11. While simplistic, this model is sufficient to demonstrate a basic understanding of the AP209 ed2 data model requirements.

■ Axial stiffness element (no torsional stiffness)

■ FE model composition

■ Elements:	16	CROD
■ Nodes:	17	GRID
■ Loads:	1	FORCE
■ Boundary:	1	SPC1
■ Property:	1	PROD
■ Material:	1	MAT1 (aluminum)
■ System:	1	CORD2R (at origin)



$$\begin{aligned} \text{Axial stress:} & \quad 1000 / 8 = 125 \text{ psi} \\ \text{Axial strain:} & \quad 125 / 10e+6 = 1.25e-5 \text{ in/in} \\ \text{Axial defl:} & \quad 1.25e-5 \times 16 = 0.0002 \text{ in} \end{aligned}$$

■ Subcase and output requests

■ Subcases:	1	SUBCASE
■ Boundary:	1	SPC
■ Loads:	1	LOAD
■ Output:	4	GPFORCE (global)
		DISPLACEMENT
		SPCFORCES
		STRESS

*See listing for output parameters

Figure 11 Pilot Model Content Summary for ATS1

Additional details of the model are:

- Single Isotropic aluminum material property at 70 deg F.
- 1000 lb axial load in compressive (-x) direction
- Single rectangular coordinate system located at the origin (0,0,0)
- All nodes and elements are on a line defined as y=-2 and z=1 in the local system.

5.1 Product Definition Shape

The AP209 ed2 data model treats the finite element model (FEM) as an analysis product that follows a defined structure for STEP products. This was discussed in Section 4. That discussion is extended here to illustrate the path from the product entity to the primary entities used to capture the finite element model information. Figure 12 illustrates this structure, wherein the entity instances follow the naming convention, **#id [number of references] : entity type**.

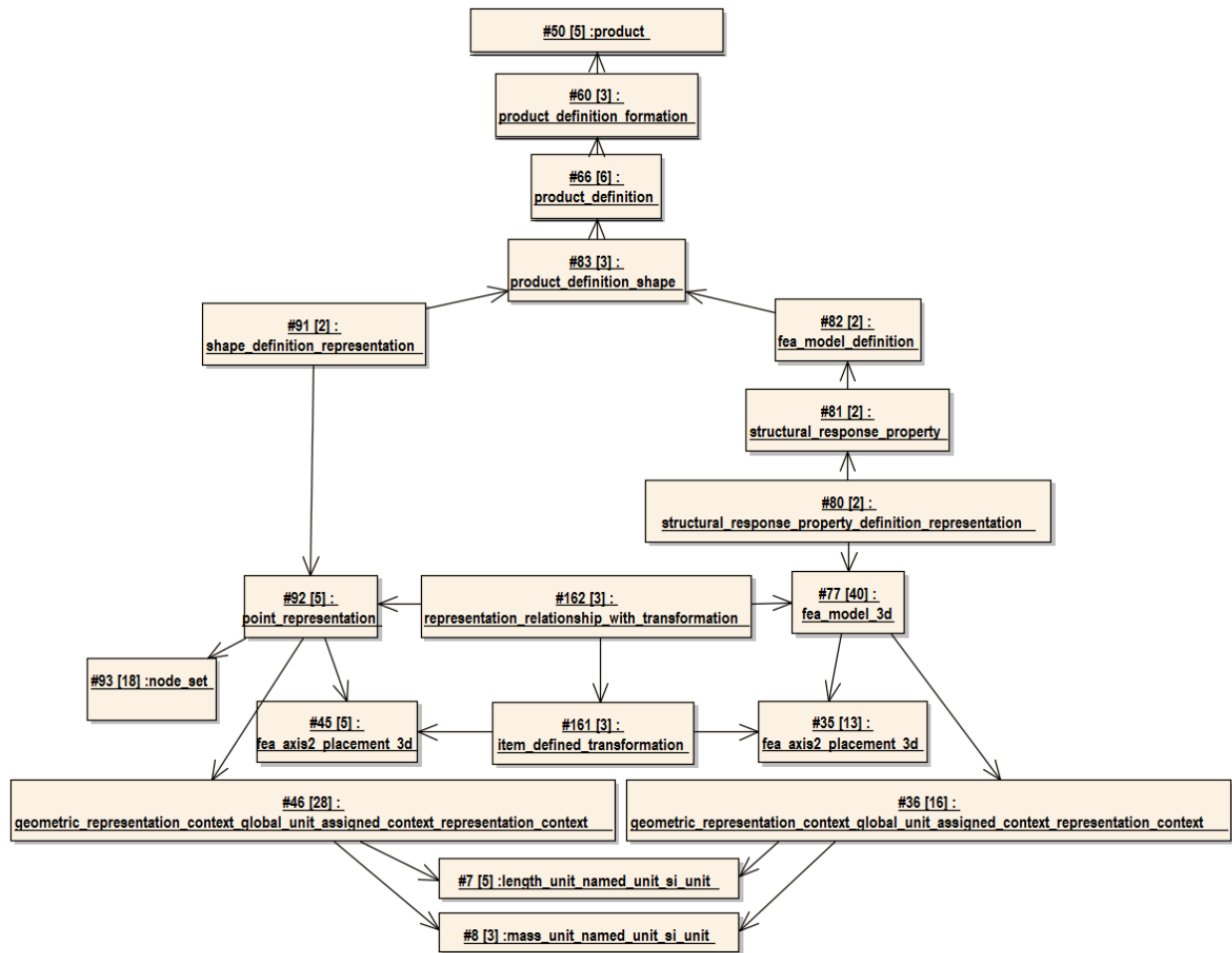


Figure 12 Overall Data Model Structure From Analysis Product to Contexts and Units

The product_definition_shape links the standard product identification and versioning to the details of the FE model. The two entities that refer to this entity link the representational aspects and definitional aspects of the finite element model, respectively. These are important topics but again, not the focus of this pilot study.

This handbook is concerned with the entities related to the point_representation and the fea_model_3d. The remainder of this discussion deals with information associated with these two entities.

Figure 12 shows the overall framework used to structure the details of this pilot model and illustrates the basic geometric founding aspects of AP209 ed2. A basic tenant of the STEP data model is that any

schema entity in the representation.items list of a representation entity has an appropriate context (specified in representation.context_of_items) to describe how to interpret the information related to the representation. For geometric entities such as points, nodes and coordinate systems, a complex context is used to define the dimension of the geometric space; it can reference a set of units and can also define a global uncertainty tolerance. The use of the EXPRESS type context_dependent_measure which is simply a REAL value indicates that the using representation identifies the context of the measure. In this manner, the units associated with the measure can be ascertained. However, in some cases, the entity type measure_with_unit is specified directly in the EXPRESS schema. In this case, explicit instancing of a measure_value and a unit is required. Lastly, there is the concept of 'unspecified' that indicates there is no appropriate value for the attribute.

5.2 FEA Model

The fea_model_3d represents the existence of the FEA model and the implied (or asserted) basic coordinate frame of reference it is described in. There is no explicit input data that maps to this STEP entity; it is used for identification of the FEA model, what software may have been used to create it and the name of the intended analysis code. The Part 21 fragment for this pilot model is shown in Figure 13.

```
#77= FEA_MODEL_3D('Identification', (#35),#36,
'NASTRAN BDF Converter v0.0.0', ('NASTRAN'),'AnalysisModelType');
```

Figure 13 STEP File Fragment for FEA Model 3D

The corresponding flattened EXPRESS schema entity definition for fea_model_3d is shown in Figure 14.

```
ENTITY fea_model_3d;
  ENTITY representation;
    name : LABEL;
    items : SET [1:?] OF representation_item;
    context_of_items : representation_context;
  DERIVE
    id : IDENTIFIER;
    description : TEXT;
  ENTITY fea_model;
    creating_software : TEXT;
    intended_analysis_code : SET [1:?] OF TEXT;
    analysis_type : TEXT;
  ENTITY fea_model_3d;
END ENTITY;
```

Figure 14 Flattened EXPRESS Schema for FEA_Model_3D

A flattened EXPRESS schema definition shows the inheritance hierarchy and which super-type an attribute is defined in. Derived attributes do not appear in the Part 21 file explicitly.

In the Part 21 fragment, note that a specification of a SET of things (items and intended_analysis_code) result in the use of parenthesis around a comma separated list of items. In this case, each attribute is a list of only one entity. This syntactical rule also applies to a LIST of things, and appears often in the example model Part 21 file fragments. The list of nodes in the connectivity of an element follows this syntax and is shown in the element definition section

5.3 Coordinate Systems

The two complex contexts that are shown in the product_definition_shape diagram result from the basic frame of reference that the FEA model exists in (the basic coordinate system) and local frames of reference created by local coordinate systems. When multiple coordinate systems are used in a model such as this one, there must be a relationship that exists that can be used to transform information in one coordinate system to another. An FEA example of this would be transforming a node defined in a local coordinate system to the basic coordinate system of the FEM.

5.3.1 STEP Diagram

Figure 15 illustrates the coordinate transformation concept showing only the local instances related to the transformation.

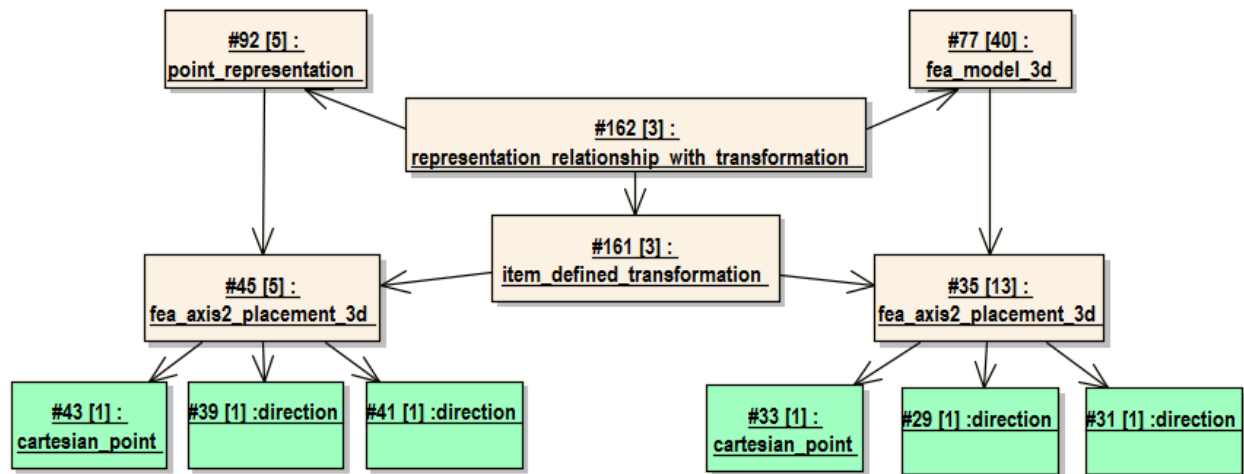


Figure 15 Details of item_defined_transformation Relating Coordinate Systems

An item_defined_transformation represents the fact that the two items it references are related to each other through a transformation operator that can be constructed from the information contained in the actual items being transformed. In this case, the item_defined_transformation relates the two fea_axis2_placement_3d (representation_items) entities to each other. It is also referenced by a representation_relationship_with_transformation that specifies which owning representations are to be used to access the related context information (such as system of units or uncertainty) for the item being transformed. This structure is convenient because the definition of the fea_axis2_placement_3d origin location and direction can be used to reconstruct the transformation operator without using trigonometric calculations that would be required if angular rotations were used to define the transformation.

5.3.2 FE Model Input

The NASTRAN specification of the local coordinate system and the input data schema is shown in Figure 16. The A, B and C points refer to the origin, a point on the Z axis and a point in the X-Z plane. In this case, the local coordinate system is coincident with the basic coordinate system.

	1	2	3	4	5	6	7	8	9	10
CORD2R	CID	RID	A1	A2	A3	B1	B2	B3		
	C1	C2	C3							
CORD2R	1		0.	0.	0.	0.	0.	1.		
	1.	0.	0.							

Figure 16 NASTRAN Card Image for Rectangular Coordinate System

5.3.3 STEP Entities

The Part 21 instance data for the coordinate systems and transformation is shown in Figure 17.

NASTRAN does not define the basic coordinate system for a model; it is implied. However, an explicit definition for the basic coordinate system is used in the AP209 ed2 data model. The axis2_placement_3d instance referenced in the set of items for the fea_model_3d instance, is the basic coordinate system.

```
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,.CARTESIAN.,'FEA_BASIC_COORD_SYSTEM.0');

#36= /* GEOMETRIC_REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT('FEA_BASIC_COORD_SYSTEM.0','3d'));

#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));

#45= FEA_AXIS2_PLACEMENT_3D('1',#43,#41,#39,.CARTESIAN.,'CORD2R.1');

#46= /* GEOMETRIC_REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT('CORD2R.1','3d'));

#39= DIRECTION('RefX',(1.,0.,0.));
#41= DIRECTION('AxisZ',(0.,0.,1.));
#43= CARTESIAN_POINT('',(0.,0.,0.));

#92= POINT_REPRESENTATION('point_representation_name_1',(#93,#45),#46);
#93= NODE_SET('node_set_name_1',(#90,#99,#103,#107,#111,#115,#119,#123,
#127,#131,#135,#139,#143,#147,#151,#155,#159));

#161= ITEM_DEFINED_TRANSFORMATION('', '#35,#45');
#162= REPRESENTATION_RELATIONSHIP_WITH_TRANSFORMATION('', '#77,#92,#161');
```

Figure 17 STEP File Fragment for Coordinate System Relationships

The node_set entity in the listing aggregates all the nodes that are using the local coordinate system for their geometric location identified by a point_representation. If additional coordinate systems are present, additional point_representations with fea_axis2_placement_3d and their associated node_sets will exist with the requisite item_defined_transformation. The EXPRESS schema entities for a fea_axis2_placement_3d are shown in Figure 18.

```

ENTITY fea_axis2_placement_3d;
  ENTITY representation_item;
    name : LABEL;
  ENTITY geometric_representation_item;
    DERIVE
      dim : DIMENSION_COUNT;
  ENTITY placement;
    location : cartesian_point;
  ENTITY axis2_placement_3d;
    axis : OPTIONAL direction;
    ref_direction : OPTIONAL direction;
    DERIVE
      p : LIST [3:3] OF direction;
  ENTITY fea_axis2_placement_3d;
    system_type : COORDINATE_SYSTEM_TYPE;
    description : TEXT;
END_ENTITY;

```

Figure 18 EXPRESS Schema for STEP Coordinate System Definition

5.4 Node Definition

FEA models use grid points and a mesh of finite elements to discretize the continuous domain of the physical model into smaller regions that have numerical approximations that allow finite element solvers to produce calculated responses at these grid points. The cloud of grid points defines the basic shape of the finite element model. In AP209 ed2, grid points are mapped to node entities. The node entities in STEP use a reference to a point entity sub-type that defines the spatial location (coordinates) of the particular type of node.

NOTE: Do not confuse the title of this clause with the node_definition ENTITY in AP209 ed2.

5.4.1 STEP Diagram

The relationship of the AP209 ed2 node entity to the basic model and local coordinate system entities is shown in Figure 19.

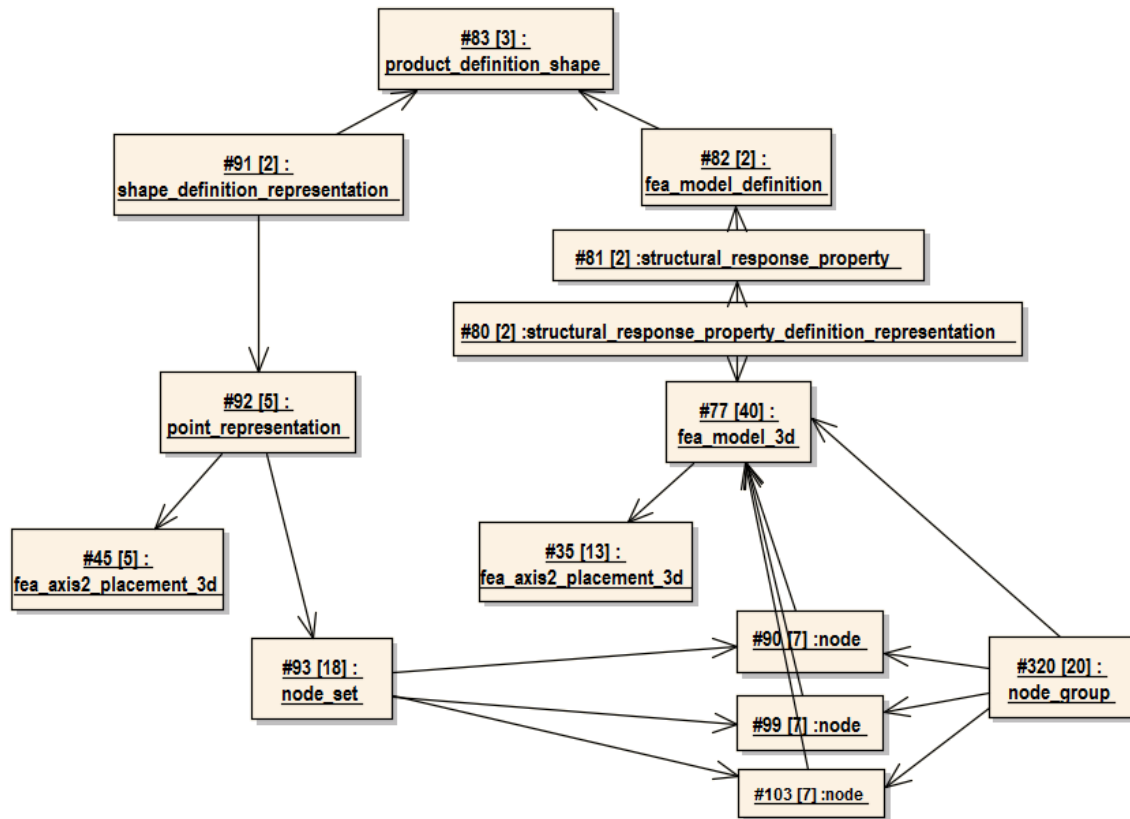


Figure 19 STEP Node Entity Relationships to other FEA Instances

The node instances all refer to the owning fea_model_3d and are referenced by other entities such as the node_set for geometric founding discussed in Section 5.1 and the node_group which represents the concept of a set of nodes from the solvers perspective. Do not confuse the node_set entity with a solver node 'set' or 'group' definition. The AP209 ed2 node_set is a STEP geometric founding construct related to coordinate system assignment.

Solver definitions of a 'set' or 'group' of grid points are used for model sub-domains, boundary conditions, loads, output requests and other solver dependent purposes. These are all mapped to instances of node_group.

5.4.2 FE Model Input

The pilot model consists of 17 equally spaced grid points with the first at $x=0, y=-2, z=1$ and the last at $x=16, y=-2, z=1$ in the local coordinate system. These grid points define the end points of the 1 dimensional rod element used in this model. The NASTRAN listing of the first 3 grid points is shown in Figure 20.

	1	2	3	4	5	6	7	8	9	10
	GRID	ID	CP	X1	X2	X3	CD	PS	SEID	
GRID	1	1	1	0.	-2.	1.				
GRID	2	1	1	1.	-2.	1.				
GRID	3	1	1	2.	-2.	1.				

Figure 20 NASTRAN Card Image for Grid Points

The 'CP' field is a reference to the ID of the coordinate system that the X1, X2, X3 coordinate values should be interpreted in. The 'CD' field specifies the coordinate system that the degrees of freedom at this point are defined in as well as the reference system for output data at the grid point. The 'PS' is a permanent constraint applied to the degrees of freedom at this grid point and the 'SEID' is the super element identifier. These two additional fields are not relevant to this pilot model.

5.4.3 STEP Entities

The equivalent STEP listing for these 3 grid points is shown in Figure 21.

```
#90= NODE('1', (#88), #46, #77);
#88= CARTESIAN_POINT('1', (0., -2., 1.));

#99= NODE('2', (#97), #46, #77);
#97= CARTESIAN_POINT('2', (1., -2., 1.));

#103= NODE('3', (#101), #46, #77);
#101= CARTESIAN_POINT('3', (2., -2., 1.));

#320= NODE_GROUP('', 'ALL', #77, (#90, #99, #103, #107, #111, #115, #119, #123,
#127, #131, #135, #139, #143, #147, #151, #155, #159));
#321= ID_ATTRIBUTE('ALL', #320);
```

Figure 21 STEP File Fragment for Nodes and Node Groups

Each node refers to a 3-dimensional context for geometric founding and a point entity sub-type to define the coordinates of the point. The label attribute is used to specify the node ID.

These entities can be located in Figure 19 for reference. The 'ALL' node_group resulted from an output request that indicated all nodal displacements or grid point forces be output. The EXPRESS flattened schema for these entities is shown in Figure 22.

```

ENTITY node;
  ENTITY representation;
    name : LABEL;
    items : SET [1:?] OF representation_item;
    context_of_items : representation_context;
  DERIVE
    id : IDENTIFIER;
    description : TEXT;
  ENTITY node_representation;
    model_ref : fea_model;
  ENTITY node;
END_ENTITY;

ENTITY cartesian_point;
  ENTITY representation_item;
    name : LABEL;
  ENTITY geometric_representation_item;
  DERIVE
    dim : DIMENSION_COUNT;
  ENTITY point;
  ENTITY cartesian_point;
    coordinates : LIST [1:3] OF LENGTH_MEASURE;
END_ENTITY;

ENTITY node_group;
  ENTITY group;
    name : LABEL;
    description : OPTIONAL TEXT;
  DERIVE
    id : IDENTIFIER;
  ENTITY fea_group;
    model_ref : fea_model;
  ENTITY node_group;
    nodes : SET [1:?] OF node_representation;
END_ENTITY;

ENTITY node_set;
  ENTITY representation_item;
    name : LABEL;
  ENTITY geometric_representation_item;
  DERIVE
    dim : DIMENSION_COUNT;
  ENTITY node_set;
    nodes : SET [1:?] OF node_representation;
END_ENTITY;

```

Figure 22 Flattened EXPRESS Schema for Node and Related Entities

The node entity inherits items attribute from the representation super-type which is a set of 1 or more representation_items. For a node entity, the set contains a single cartesian_point entity which defines the node location (a cartesian_point is a kind of representation_item). The context_of_items attribute contains the requisite reference to the context of the point entity. Additionally, the super-type node_representation adds the reference to the fea_model to a node entity. This pattern of context-<-representation-> representation_item is a common theme throughout the STEP data model and the reader is encouraged to become familiar with this concept in the Part 43 reference document.

5.5 Element Definition

A simple linear rod element is defined between each grid point to supply stiffness to the grid points. Even though this is a simple 2 degree of stiffness element, it is a good illustration of how FEM elements are mapped to the STEP AP209 ed2 data model.

NOTE: Do not confuse the title of this clause with the element_definition ENTITY in AP209 ed2.

5.5.1 STEP Diagram

An overall view of the STEP implementation of element definition and relationships to the FEA model concepts such as element coordinate systems, physical properties and material properties is illustrated in Figure 23.

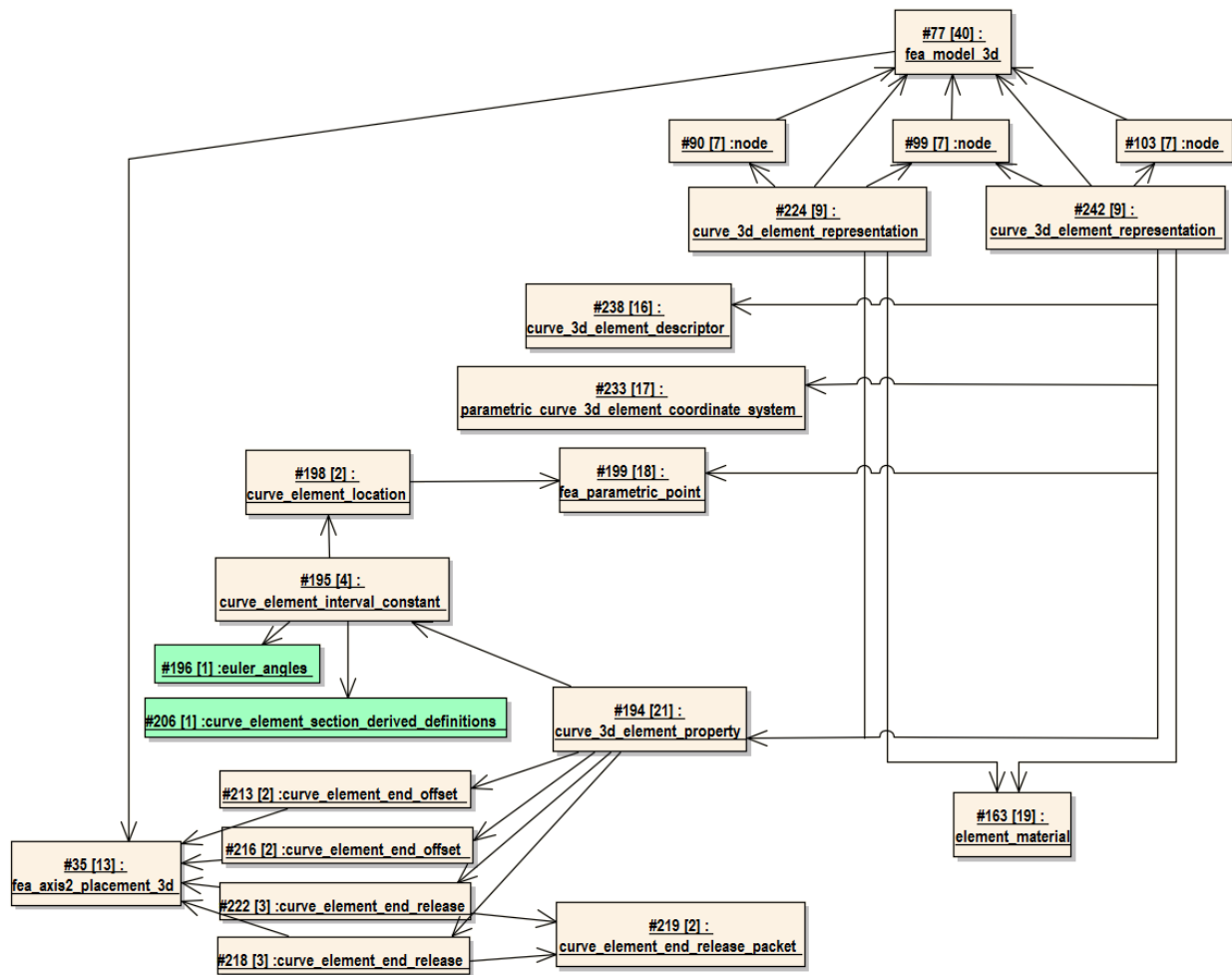


Figure 23 STEP Element Definition and Related Data Model Structures

This diagram starts with the fea_model_3d instance, shows the relevant nodes used in the items list for connectivity, and then the basic layout of the element properties. The element information is discussed in logical groupings below.

5.5.2 FE Model Input

There are 16 NASTRAN elements defined using the CROD input card image shown in Figure 24. The rod element used in this model supplies stiffness for only 2 degrees of freedom at each grid point.

	1	2	3	4	5	6	7	8	9	10
	CROD	EID	PID	G1	G2					
CROD	1	1	1	1	2					
CROD	2	1	2	2	3					

Figure 24 NASTRAN Card Image for Rod Element

Therefore, the element acts as a simple axial and torsional spring between the grid points. There are no additional options to be specified for this element.

5.5.3 STEP Entities

The 1-dimensional linear spring element maps to a `curve_3d_element_representation`. The behavioral aspects of the element are specified by the `curve_3d_element_descriptor` which is a set of enumerated capabilities for the element as shown in Figure 25.

```
#224= CURVE_3D_ELEMENT_REPRESENTATION('1', (#233,#199),#225, (#90,#99),#77,#238,#194,#163);
#242= CURVE_3D_ELEMENT_REPRESENTATION('2', (#233,#199),#225, (#99,#103),#77,#238,#194,#163);

#238= CURVE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER., 'LINEAR_CURVE.CROD', (
(ENUMERATED_CURVE_ELEMENT_PURPOSE(.AXIAL.)),
(ENUMERATED_CURVE_ELEMENT_PURPOSE(.TORSION.))
));
```

Figure 25 STEP File Fragment for Element and Element Descriptor

The flattened EXPRESS schema shown in Figure 26 defines, in order, what each attribute in the element instances represent.

```
ENTITY curve_3d_element_representation;
  ENTITY representation;
    name : LABEL;
    items : SET [1:?] OF representation_item;
    context_of_items : representation_context;
  DERIVE
    id : IDENTIFIER;
    description : TEXT;
  ENTITY element_representation;
    node_list : LIST [1:?] OF node_representation;
  ENTITY curve_3d_element_representation;
    model_ref : fea_model_3d;
    element_descriptor : curve_3d_element_descriptor;
    property : curve_3d_element_property;
    material : element_material;
END_ENTITY;
```

Figure 26 EXPRESS Schema for Curve 3D Element Representation

The name attribute has been used to hold the solver element ID while the items set is a list of entity references used to establish a parametric element coordinate system. The `context_of_items` reference

follows. Next, connectivity is specified by an ordered set of 2 node references. While the linear rod element node list order is straight forward, the higher dimension elements are more complicated as each solver has its own unique way of ordering the connectivity array.

The Part 104 document explicitly specifies how the node list should be ordered for all element types and orders. It is the translator's responsibility to map the solver order to the Part 104 order. This also includes supplying placeholder dummy nodes in the node list for a connectivity location that the solver may not support (such as mid-face nodes for solids in NASTRAN). The last four attributes are references to the owning fea_model_3d, the element descriptor, the physical properties and material properties.

The element descriptor specifies how the curve_3d_element_representation behavior is specialized to match the particular solver element type that this instance represents. In this case, a simple axial and torsional 1-dimensional spring element is the solver element behavior specified. The description field can be used to identify what type of element this descriptor represents. However, FEA solvers should not place any processing logic in this field unless agreed to and documented in the recommended practices.

As a note of caution, even though the solver element usage may allow for degrees of freedom to be released or a specific stiffness to be set to zero, the descriptor for that element should define the full capabilities of the element type and not the individual element options that are represented elsewhere in the STEP data model. This pilot model illustrates this issue by specifying a zero torsional stiffness property, however, the descriptor still includes the possible existence of torsional stiffness with the ENUMERATED_CURVE_ELEMENT_PURPOSE(.TORSION.) enumeration item.

The EXPRESS schema for the descriptor is shown in Figure 27.

```
ENTITY curve_3d_element_descriptor;  
  ENTITY element_descriptor;  
    topology_order          : ELEMENT_ORDER;  
    description             : TEXT;  
  ENTITY curve_3d_element_descriptor;  
    purpose                 : SET [1:?] OF SET [1:?] OF CURVE_ELEMENT_PURPOSE;  
END_ENTITY;  
  
TYPE Curve_Element_Purpose = SELECT  
  ( Enumerated_Curve_Element_Purpose,  
    Application_Defined_Element_Purpose );  
END_TYPE;  
  
TYPE Enumerated_Curve_Element_Purpose = ENUMERATION OF  
  ( Axial,  
    Y_Y_Bending,  
    Z_Z_Bending,  
    Torsion,  
    X_Y_Shear,  
    X_Z_Shear,  
    Warping );  
END_TYPE;
```

Figure 27 EXPRESS Schema for Curve 3D Element Descriptor

The first two references in the elements items list referred to entities needed to establish the parametric coordinate system for the element. Therefore, the context_of_items must relate to a parametric_context (or at least a parametric_context must be part of the full complex context for the element). These items are shown in Figure 28.

```
#233= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#236);
#236= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#234);
#234= DIRECTION('undefined',(1.,0.,0.));

#199= FEA_PARAMETRIC_POINT('',(1.,0.,0.));

#225= /* GEOMETRIC_REPRESENTATION_CONTEXT+PARAMETRIC_REPRESENTATION_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)PARAMETRIC_REPRESENTATION_CONTEXT()
REPRESENTATION_CONTEXT('REP_CONTEXT_FEA','3D'));
```

Figure 28 STEP File Fragment for Curve 3D Parametric Coordinate System

These instances define a parametric element coordinate system where the parametric coordinate ξ represents the position and direction along the length of the element from (-1,0,0) to (1,0,0) as shown in Figure 29.

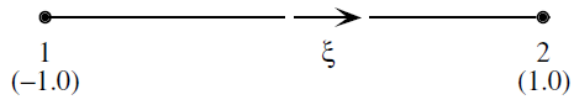


Figure 29 Curve Parametric Element Coordinates

The parametric point shown is used to define a parametric curve_element_location that defines the end of a curve_element_interval_constant where the physical properties are defined along the length of the overall element. This is discussed in the next section.

5.6 Property Definition

The property definition for curve elements can be complex. This simple model does not hide all the complexity but it simplifies the population of the required attributes. The pilot model uses a single NASTRAN property that is shared by all the rod elements. This is possible since there are no element unique attributes that must be captured in the STEP AP209 ed2 property representation. Examples of attributes that would require unique properties are offsets and releases or tapering that is specified uniquely on an element. The CROD element does not support any of these additional attributes.

5.6.1 STEP Diagram

The property section from the top level diagram shown in Figure 23 for this pilot model is repeated as Figure 30 for reference.

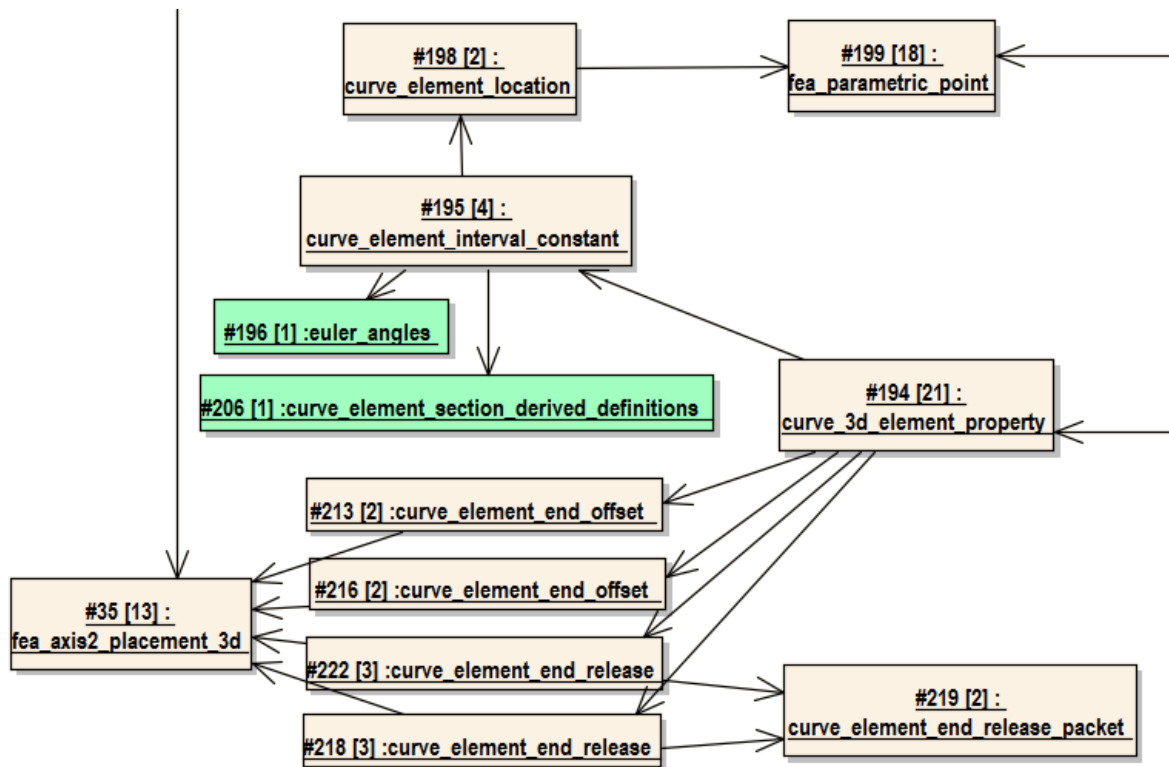


Figure 30 Details of Curve 3D Element Property

5.6.2 FE Model Input

The PROD property is defined and shared by all the elements in this pilot model. The input supplied for this model is shown in Figure 31.

1	2	3	4	5	6	7	8	9	10
PROD	PID	MID	A	J	C	NSM			
PROD	1	1	8.	0.					

Figure 31 NASTRAN Card Image for Rod Property

The rod has a cross sectional area of 8. length units squared. In this problem the implied unit is inch. No assumption about cross sectional geometry is to be implied. The torsional constant 'J' has been set to 0 which will result in no torsional stiffness between the element grid points. The 'C' field is a coefficient used to compute torsional stress from the torsional moment and 'J'. Lastly, the 'NSM' field represents non-structural mass that for a 1-dimensional element translates into additional mass per unit length of the element.

5.6.3 STEP Entities

The AP209 ed2 representation of the input data shown in Figure 31 is listed in Figure 32.

```
#194= CURVE_3D_ELEMENT_PROPERTY('PROD.1','',( #195), (#213,#216), (#218,#222));

#195= CURVE_ELEMENT_INTERVAL_CONSTANT(#198,#196,#206);
#198= CURVE_ELEMENT_LOCATION(#199);
#199= FEA_PARAMETRIC_POINT('',(1.,0.,0.));
#196= EULER_ANGLES((0.,0.,0.));

#206= CURVE_ELEMENT_SECTION_DERIVED_DEFINITIONS(
    '',
    0.,
    8.,
    (CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
    (0.,0.,0.),
    0.,
    CONTEXT_DEPENDENT_MEASURE(0.),
    (CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
    (CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
    (CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
    CONTEXT_DEPENDENT_MEASURE(0.),
    CONTEXT_DEPENDENT_MEASURE(0.)
);

#213= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#216= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));

#218= CURVE_ELEMENT_END_RELEASE(#35,(#219));
#222= CURVE_ELEMENT_END_RELEASE(#35,(#219));
#219= CURVE_ELEMENT_END_RELEASE_PACKET(ENUMERATED_CURVE_ELEMENT_FREEDOM('NONE. '),0.);
```

Figure 32 STEP File Fragment for Curve 3D Element Property Structure (PROD)

The curve_3d_element_property entity is referenced by each element and in turn references all the particular instances that contribute to this property representation. Since the CROD only supports uniform properties throughout the element (beginning to end), a single constant interval is used. Multiple intervals could be used for stepped multi-section beams or multi-section tapered beams, but in this case there is only one constant section. Hence the use of a single curve_element_interval_constant reference in the curve_3d_element_property.

An interval is defined only by its endpoint so a single parametric point defines the interval as ending at the +1.0 parametric location. There is no twist specified so the euler_angle is 0.

The cross section property definition is specified on this interval. Again, only a single section definition is specified and many of the attributes are unspecified due to the simplicity of the element type. The listing above is formatted for readability and should match the EXPRESS listing shown in Figure 33.

```

ENTITY curve_3d_element_property;
  property_id                : IDENTIFIER;
  description                : TEXT;
  interval_definitions       : LIST [1:?] OF curve_element_interval;
  end_offsets                : ARRAY [1:2] OF curve_element_end_offset;
  end_releases               : ARRAY [1:2] OF curve_element_end_release;
END_ENTITY;

ENTITY curve_element_section_derived_definitions;
  ENTITY curve_element_section_definition;
    description              : TEXT;
    section_angle            : PLANE_ANGLE_MEASURE;
  ENTITY curve_element_section_derived_definitions;
    cross_sectional_area     : CONTEXT_DEPENDENT_MEASURE;
    shear_area               : ARRAY [1:2] OF MEASURE_OR_UNSPECIFIED_VALUE;
    second_moment_of_area    : ARRAY [1:3] OF CONTEXT_DEPENDENT_MEASURE;
    torsional_constant       : CONTEXT_DEPENDENT_MEASURE;
    warping_constant         : MEASURE_OR_UNSPECIFIED_VALUE;
    location_of_centroid     : ARRAY [1:2] OF MEASURE_OR_UNSPECIFIED_VALUE;
    location_of_shear_centre : ARRAY [1:2] OF MEASURE_OR_UNSPECIFIED_VALUE;
    location_of_non_structural_mass : ARRAY [1:2] OF MEASURE_OR_UNSPECIFIED_VALUE;
    non_structural_mass      : MEASURE_OR_UNSPECIFIED_VALUE;
    polar_moment             : MEASURE_OR_UNSPECIFIED_VALUE;
  END_ENTITY;
END_ENTITY;

ENTITY curve_element_end_offset;
  coordinate_system          : CURVE_ELEMENT_END_COORDINATE_SYSTEM;
  offset_vector              : ARRAY [1:3] OF CONTEXT_DEPENDENT_MEASURE;
END_ENTITY;

ENTITY curve_element_end_release;
  coordinate_system          : CURVE_ELEMENT_END_COORDINATE_SYSTEM;
  releases                   : LIST [1:?] OF curve_element_end_release_packet;
END_ENTITY;

ENTITY curve_element_end_release_packet;
  release_freedom            : CURVE_ELEMENT_FREEDOM;
  release_stiffness          : CONTEXT_DEPENDENT_MEASURE;
END_ENTITY;

```

Figure 33 EXPRESS Schema for Curve 3D Element Property and Related Entities

The offset and release entities do not apply to this element type but are required so the value 0. is used. The release packet uses the .NONE. enumeration for the release freedom to indicate that this characteristic does not apply to this element property. The interpretation of which end of the element that an instance of end offset or end release applies to, is determined by the order in the array of end offsets and array of end releases in the curve_3d_element_property.

5.7 Material Definition

The ROD element in NASTRAN only supports isotropic element usage so a single instance of the NASTRAN MAT1 element type was used in the pilot model. This material represents typical aluminum property values which implies a unit system of inch-pound force-second. However, the units in this STEP file instance do not reflect this implied system. When processing solver files that do not explicitly specify

units, an external mechanism should be employed to augment the reading of the source model information.

5.7.1 STEP Diagram

The material data model in AP209 ed2 is complex. However, the isotropic material model used for the pilot models is the simplest instantiation possible for a 3 dimensional problem. The overall diagram of the material property model is shown in Figure 34.

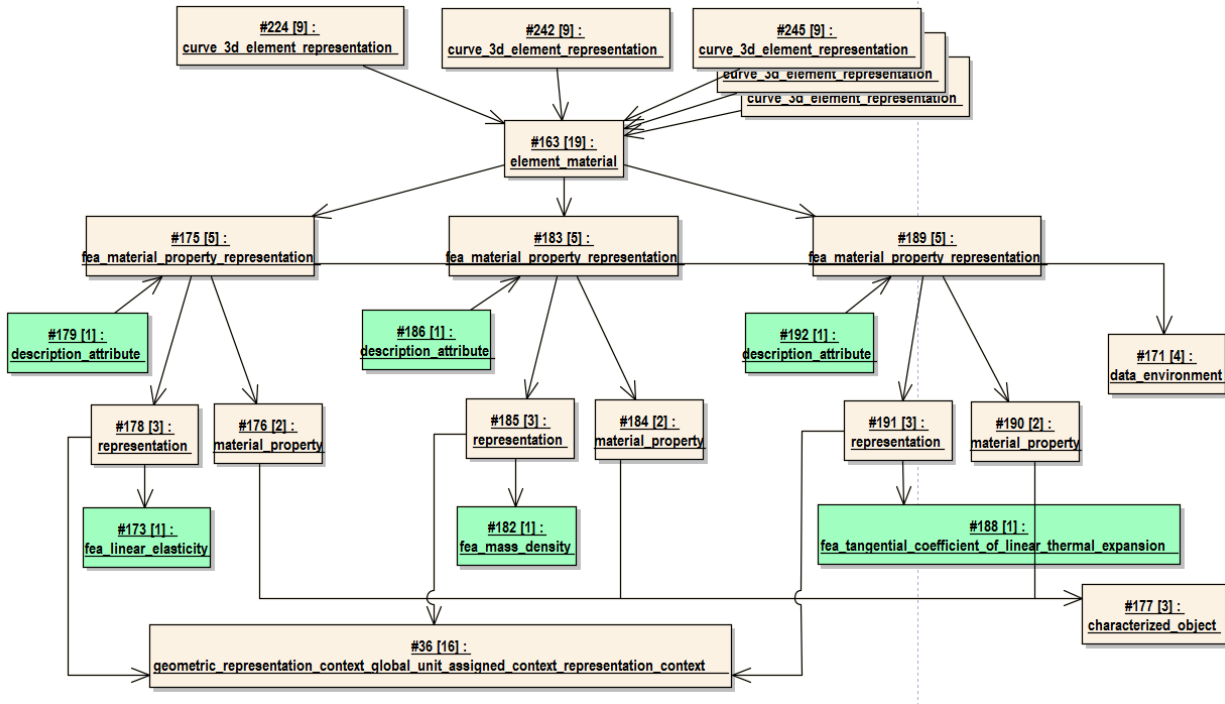


Figure 34 Overall Structure of Element Material Property

This figure shows the elements referring directly to a single element_material instance. This element material in turn references 3 fea_material_property_representations that form the set of properties aggregated into this element_material instance. Each of these generic entities also references a generic representation instance. This representation has an items [2] list that is populated with a single instance of an fea_material_property_representation_item entity. This super-type is the parent of all the familiar material property entities used to package the material constants into the proper tensor type (green entities #173, #182, #188). The FEM input and EXPRESS schema fragments presented in the following sections will further explain the use of super-type sub-type and SELECT type for material property modeling.

Each of the fea_material_property_representation_item instances also refers to a single data_environment that defines the conditions under which the material constants were determined. Information such as temperature or moisture conditions can be specified under this entity. Additional data_environments can be defined if needed.

5.7.2 FE Model Input

The isotropic linear material is specified as shown in Figure 35.

1	2	3	4	5	6	7	8	9	10
MAT1	MID	E	G	NU	RHO	A	TREF	GE	
	ST	SC	SS	MCSID					

MAT1	1	1.+7		.33	2.54-4	1.3-5	70.		
------	---	------	--	-----	--------	-------	-----	--	--

Figure 35 NASTRAN Card Image for Isotropic Material

The “E” field represents the modulus of elasticity, whereas, G represents the shear modulus. NU is Poisson’s ratio, A is the coefficient of thermal expansion and TREF is the reference strain free temperature. The other solver specific fields are not used for this pilot model but are described in the NASTRAN documentation available on-line.

This input also illustrates a quirk of NASTRAN history. To maximize the number of significant digits possible in an 8-character field with a signed exponent, the use of the ‘E’ or ‘e’ preceding the exponent was eliminated. This can lead to erroneous parsing if not accounted for. Even “cut and paste” to familiar spread sheet tools can lead to unexpected results.

5.7.3 STEP Entities

The simple one-line MAT1 input card encodes a tremendous amount of information. It makes specification of the material in the solver deck simpler but can lead to ambiguous interpretation. The STEP data model expresses this in an un-ambiguous way as shown in Figure 36.

```
#163= ELEMENT_MATERIAL('MAT1.1','Fea Material',(#175,#183,#189));

#175= FEA_MATERIAL_PROPERTY_REPRESENTATION(#176,#178,#171);
#179= DESCRIPTION_ATTRIBUTE('Elasticity',#175);
#176= MATERIAL_PROPERTY('MAT1.1.0',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#178= REPRESENTATION('representation_id_2',(#173),#36);
#173= FEA_LINEAR_ELASTICITY('',FEA_ISOTROPIC_SYMMETRIC_TENSOR4_3D((10000000.,0.33)));

#183= FEA_MATERIAL_PROPERTY_REPRESENTATION(#184,#185,#171);
#186= DESCRIPTION_ATTRIBUTE('MassDensity',#183);
#184= MATERIAL_PROPERTY('MAT1.1.1',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#185= REPRESENTATION('representation_id_3',(#182),#36);
#182= FEA_MASS_DENSITY('',0.000254);

#189= FEA_MATERIAL_PROPERTY_REPRESENTATION(#190,#191,#171);
#192= DESCRIPTION_ATTRIBUTE('TangentCTE',#189);
#190= MATERIAL_PROPERTY('MAT1.1.2',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#191= REPRESENTATION('representation_id_4',(#188),#36);
#188= FEA_TANGENTIAL_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION('',ISOTROPIC_SYMMETRIC_TENSOR2_3D(1.30E-5));
```

Figure 36 STEP File Fragment for Element Material

The element material entity references 3 material properties that are grouped together in Figure 36. Each group is defined by an instance of an fea_material_property_representation. The name and description attributes are useful for reading or displaying information about a single property, but are not part of the formal data identification. The existence of the fea_linear_elasticity, the fea_mass_density and the fea_tangential_coefficient_of_linear_thermal_expansion instances at the bottom of each property grouping as shown in Figure 37 is the proper way to identify what each fea_material_property_representation represents.

```

ENTITY element_material;
  material_id          : IDENTIFIER;
  description          : TEXT;
  properties           : SET [1:?] OF material_property_representation;
END_ENTITY;

ENTITY fea_material_property_representation;
  ENTITY property_definition_representation;
    definition          : REPRESENTED_DEFINITION;
    used_representation : representation;
  DERIVE
    description        : TEXT;
    name               : LABEL;
  ENTITY material_property_representation;
    dependent_environment : data_environment;
  ENTITY fea_material_property_representation;
END_ENTITY;

TYPE Represented_Definition = SELECT
( General_Property,
  Property_Definition,
  Property_Definition_Relationship,
  Shape_Aspect,
  Shape_Aspect_Relationship );
END_TYPE;

ENTITY material_property;
  ENTITY property_definition;
    name          : LABEL;
    description   : OPTIONAL TEXT;
    definition     : CHARACTERIZED_DEFINITION;
  DERIVE
    id            : IDENTIFIER;
  ENTITY material_property;
END_ENTITY;

```

Figure 37 EXPRESS Schema for Element Material

The 'properties' attribute of the element_material is a set of material_property_representations. Since the fea_material_property_representation is a sub-type of this entity type, they are valid members of the set of properties for the element_material. The full list of possible entity types for these specific properties are found in the 'fea_material_property_representation_item' sub-types shown in Figure 38.

```

ENTITY Fea_Material_Property_Representation_Item
  SUPERTYPE OF ( ONEOF (
    Fea_Linear_Elasticity,
    Fea_Mass_Density,
    Fea_Area_Density,
    Fea_Tangential_Coefficient_Of_Linear_Thermal_Expansion,
    Fea_Secant_Coefficient_Of_Linear_Thermal_Expansion,
    Fea_Moisture_Absorption,
    Fea_Shell_Membrane_Stiffness,
    Fea_Shell_Bending_Stiffness,
    Fea_Shell_Membrane_Bending_Coupling_Stiffness,
    Fea_Shell_Shear_Stiffness ) )
  SUBTYPE OF ( Representation_Item );
END_ENTITY;

```

Figure 38 Valid Material Properties for Element Material

There is a pattern to how these entities at the bottom of the grouping are defined in the EXPRESS schema that facilitates understanding the structure. This pattern introduces a new concept in the EXPRESS schema, the 'SELECT' type. A 'SELECT' type allows a type to be any of a list of possible types or entities. Using the fea_linear_elasticity as an example is shown in Figure 39.

```

ENTITY fea_linear_elasticity;
  ENTITY representation_item;
    name                                     : LABEL;
  ENTITY fea_material_property_representation_item;
  ENTITY fea_linear_elasticity;
    fea_constants                           : SYMMETRIC_TENSOR4_3D;
END_ENTITY;

TYPE Symmetric_Tensor4_3d = SELECT
( Anisotropic_Symmetric_Tensor4_3d,
  Fea_Isotropic_Symmetric_Tensor4_3d,
  Fea_Iso_Orthotropic_Symmetric_Tensor4_3d,
  Fea_Transverse_Isotropic_Symmetric_Tensor4_3d,
  Fea_Column_Normalised_Orthotropic_Symmetric_Tensor4_3d,
  Fea_Column_Normalised_Monoclinic_Symmetric_Tensor4_3d );
END_TYPE;

TYPE Fea_Isotropic_Symmetric_Tensor4_3d = ARRAY [1 : 2] OF Context_Dependent_Measure;
END_TYPE;

```

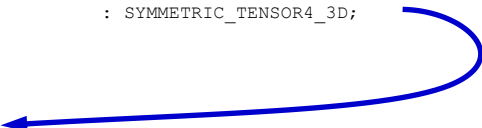


Figure 39 Entity -> SELECT Type -> Type Pattern for Material Properties

The tensor type for this material property is a symmetric_tensor4_3d which dictates which mathematical operations are required to transform information in this tensor to a different geometric frame of reference. However, there are many simplifications of the full tensor expression that can be made based on the type of material being modeled. For this pilot model, an isotropic linear material reduces to 2 independent constants. Therefore, the fea_isotropic_symmetric_tensor4_3d type was selected. This type is a simple array of 2 context_dependent_measures (for Young's modulus (E) and Poisson's ratio (nu)).

The other properties are specified with similar patterns when tensor quantities are required. For example, the coefficient of linear expansion property is defined by the schema shown in Figure 40.

```

ENTITY fea_tangential_coefficient_of_linear_thermal_expansion;
  ENTITY representation_item;
    name                                     : LABEL;
  ENTITY fea_material_property_representation_item;
  ENTITY fea_tangential_coefficient_of_linear_thermal_expansion;
    fea_constants                           : SYMMETRIC_TENSOR2_3D;
END_ENTITY;

TYPE Symmetric_Tensor2_3d = SELECT
( Isotropic_Symmetric_Tensor2_3d,
  Orthotropic_Symmetric_Tensor2_3d,
  Anisotropic_Symmetric_Tensor2_3d );
END_TYPE;

TYPE Isotropic_Symmetric_Tensor2_3d = Context_Dependent_Measure;
END_TYPE;

```

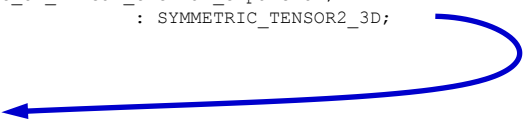


Figure 40 EXPRESS Schema for Coefficient of Linear Thermal Expansion

The mass density property is different in that it is not a tensor quantity and is represented by a simple scalar data type which is a single context_dependent_measure (see Figure 41).

```

ENTITY fea_mass_density;
  ENTITY representation_item;
    name : LABEL;
  ENTITY fea_material_property_representation_item;
  ENTITY fea_mass_density;
    fea_constant : SCALAR;
END_ENTITY;

TYPE Scalar = Context_Dependent_Measure;
END_TYPE;

```

Figure 41 EXPRESS Schema for Mass Density

Following the EXPRESS schema methodology for typing and sub-typing is not straight forward and probably beyond what this handbook is intended to convey. Readers should study the recommended practices and SMRL full EXPRESS listing to investigate further how these material properties are constructed. The most important aspect of this section is the way the tensor quantities are packaged into simple arrays in the AP209 ed2 data model. This topic is discussed in further detail in the AP209 ed2 recommended practices document and Part 104 Section 7.

Lastly, the data_environment for the element_material property items is diagrammed in Figure 42.

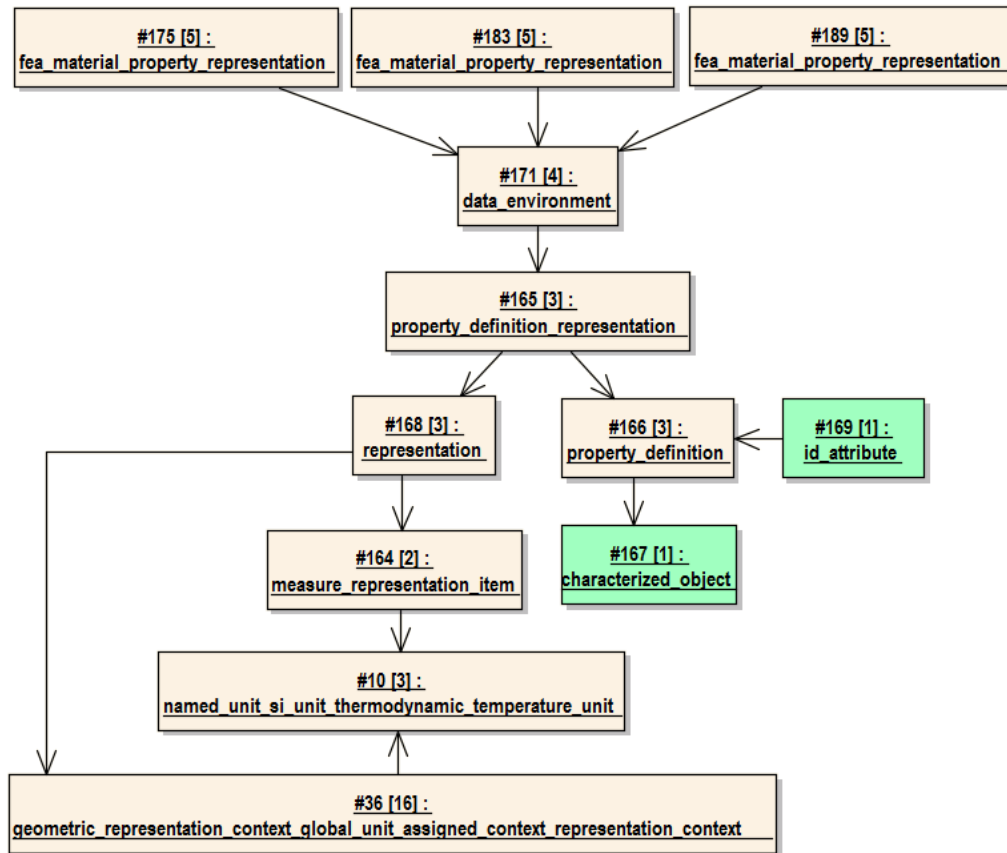


Figure 42 STEP Data Environment Instance Diagram

Figure 42 starts with the three fea_material_property_representations that were discussed above. It uses a slightly different property specification methodology that does not involve the SELECT typing and tensor packaging discussed in Section 5.7.3. Instances of property_definition_representation(s) are listed in the items list for the data_environment entity. However, for this pilot model, temperature is the only environmental property specified so there is only one property_definition_representation listed. The property_definition_representation uses a representation instance to specify a measure_representation_item in the items list. The measure_representation_item is where the property value is captured as a measure and also provides a direct link to a unit as appropriate for the property.

The listing shown in Figure 43 illustrates the data_environment used for this pilot model. Both representational and definitional aspects of the properties are supported. *Note (as of this writing, the temperature measure is correct but the specified unit .DEGREE_CELSIUS. is incorrect. Future releases of this handbook will correct this error)*

```
#171= DATA_ENVIRONMENT('DATA_ENV','Property_conditions',(#165));

#165= PROPERTY_DEFINITION_REPRESENTATION(#166,#168);
#168= REPRESENTATION('representation_id_1',(#164),#36);
#164= MEASURE_REPRESENTATION_ITEM('representation_item_name_1',THERMODYNAMIC_TEMPERATURE_MEASURE(70.),#10);

#166= PROPERTY_DEFINITION('Material Property Definition',$,#167);
#167= CHARACTERIZED_OBJECT('property',$);
#169= ID_ATTRIBUTE('MAT1.1',#166);

#10= /* SI_UNIT+THERMODYNAMIC_TEMPERATURE_UNIT */
(NAMED_UNIT(*)SI_UNIT($,.DEGREE_CELSIUS.)THERMODYNAMIC_TEMPERATURE_UNIT());
```

Figure 43 STEP File Fragment of Data Environment

The property_definition (from the data_environment) and the material_property (from the fea_material_property_representations) provide a reference to additional information about the property if needed. Currently, the characterized_object is a placeholder for the additional information. This link could be used to establish traceability to very detailed information provided by companion standards such as AP235 (10303-235) or to individual material products. An example of how Figure 34 would look if a reference to an isotropic material product instance was used is shown in Figure 44. Material products are required if laminate tables for composite materials are used.

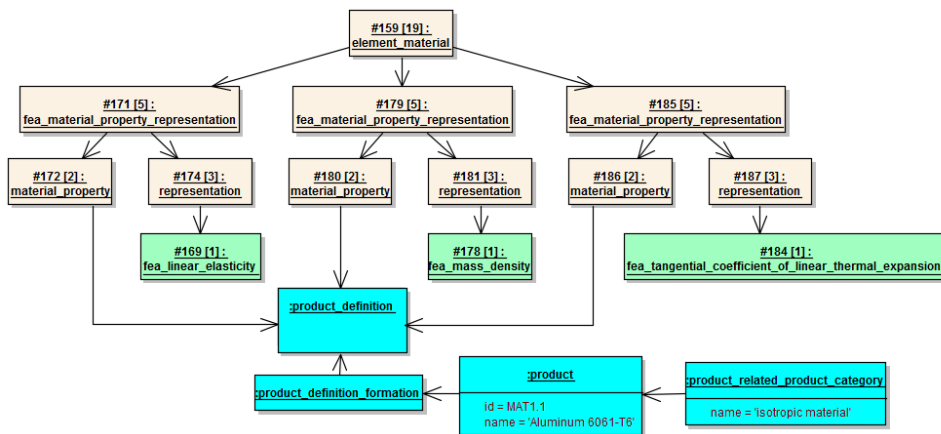


Figure 44 Use of Material Product and Product_definition in place of Characterized_object

The EXPRESS schema shown in Figure 45 for the data_environment, finalizes the material property discussion. The last EXPRESS entity definition for measure_representation_item introduces the EXPRESS construct of multiple inheritance. This construct defines an entity that is a union of both the listed super-types. This creates an instance that can fill the role of both super-types in the STEP data model.

```

ENTITY data_environment;
    name                : LABEL;
    description          : TEXT;
    elements             : SET [1:?] OF property_definition_representation;
END_ENTITY;

ENTITY property_definition_representation;
    definition           : REPRESENTED_DEFINITION;
    used_representation : representation;
    DERIVE
    description         : TEXT;
    name                : LABEL;
END_ENTITY;

TYPE REPRESENTED_DEFINITION = SELECT
    (general_property,
    property_definition,
    property_definition_relationship,
    shape_aspect,
    shape_aspect_relationship);
END_TYPE;

ENTITY property_definition;
    name                : LABEL;
    description         : OPTIONAL TEXT;
    definition           : CHARACTERIZED_DEFINITION;
    DERIVE
    id                  : IDENTIFIER;
END_ENTITY;

ENTITY Measure_Representation_Item
    SUBTYPE OF ( Representation_Item, Measure_With_Unit );
END_ENTITY;

```

Figure 45 EXPRESS Schema for Data Environment

A measure_representation_item is both a representation_item and measure_with_unit where a numerical measure value and its unit is defined. The definition of measure_with_unit is a super-type that list the 33 physical quantity types found in the SI Coherent system of units (see Part 41 and ISO 31). In this case, a thermodynamic_temperature_measure_with_unit has a unit_component of thermodynamic_temperature_unit and value_component that is a thermodynamic_measure type with a real value.

6 Pilot Model ATS2 – 1D Bar Element

The ATS2 pilot model composition is illustrated in the Figure 46. It is a variation of the ATS1 pilot model in that a different solver element type is used to represent more complex behaviors by using additional degrees of freedom.

- Bar with axial and bending stiffness (no torsional stiffness)

- FE model composition

■ Elements:	16	CBAR
■ Nodes:	17	GRID
■ Loads:	8	FORCE
	2	LOAD
■ Boundary:	1	SPC1
	1	SPCADD
■ Property:	1	PBAR
■ Material:	1	MAT1 (aluminum)
■ System:	1	CORD2R (at origin)

- Subcase and output requests

■ Subcases:	3	SUBCASE
■ Boundary:	3	SPC
■ Loads:	3	LOAD
■ Output:	12	GPFORCE (global)
		DISPLACEMENT
		SPCFORCES
		STRESS

*See listing for output parameters

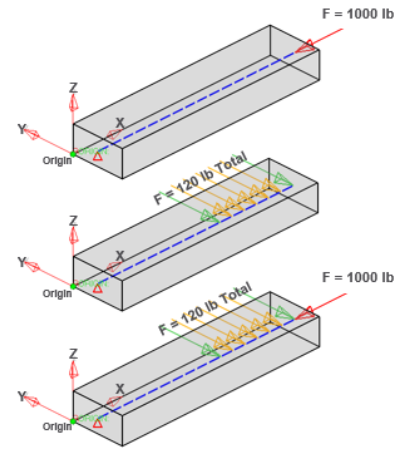


Figure 46 Pilot Model Content Summary for ATS2

Additional details of the model are:

- Introduction of boundary condition combinations
- A lateral bending load case as well as a scaled linear combination load case
- Exercise the double field NASTRAN card format in the input file
- All grid points are defined in a single local Cartesian coordinate system id=1

6.1 Product Definition Shape

Since this pilot model uses the same local coordinate system as ATS1, the diagram shown in Figure 12 for the ATS1 pilot model is valid with the exception that the instance IDs may have changed. The discussion of section 5.1 applies in its entirety to this pilot model.

6.2 FEA Model

The discussion in Section 5.2 applies to the ATS2 model. As shown in Figure 47, the fea_model_3d instance is identical to the ATS1 model.

```
#77= FEA_MODEL_3D('Identification', (#35), #36,
'NASTRAN BDF Converter v0.0.0', ('NASTRAN'), 'AnalysisModelType');
```

Figure 47 STEP File Fragment for FEA Model 3D

6.3 Coordinate System

The coordinate system discussion in Section 5.3 applies.

6.3.1 STEP Diagram

The instance diagram in Section 5.3.1 is identical for this model.

6.3.2 FE Model Input

The FEA model input for coordinate systems in model ATS2 is identical to Section 5.3.1.

6.3.3 STEP Entities

The STEP instances for coordinate systems are identical to Section 5.3.3 and are listed in Figure 48.

```
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,.CARTESIAN.,'FEA_BASIC_COORD_SYSTEM.0');

#36= /* GEOMETRIC_REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT('FEA_BASIC_COORD_SYSTEM.0','3d'));

#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));

#45= FEA_AXIS2_PLACEMENT_3D('1',#43,#41,#39,.CARTESIAN.,'CORD2R.1');

#46= /* GEOMETRIC_REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT('CORD2R.1','3d'));

#39= DIRECTION('RefX',(1.,0.,0.));
#41= DIRECTION('AxisZ',(0.,0.,1.));
#43= CARTESIAN_POINT('',(0.,0.,0.));

#92= POINT_REPRESENTATION('point_representation_name_1',(#93,#45),#46);
#93= NODE_SET('node_set_name_1',(#90,#99,#103,#107,#111,#115,#119,#123,
#127,#131,#135,#139,#143,#147,#151,#155,#159));

#161= ITEM_DEFINED_TRANSFORMATION('','',#35,#45);;
#162= REPRESENTATION_RELATIONSHIP_WITH_TRANSFORMATION('','',#77,#92,#161);;
```

Figure 48 STEP File Fragment for Basic and Local Coordinate Systems

6.4 Node Definition

The grid point discussion in Section 5.4 applies.

6.4.1 STEP Diagram

The diagram shown in Section 5.4.1 applies; however, some instance IDs may be different.

6.4.2 FE Model Input

The input from the FEA model is identical to Section 5.4.2.

6.4.3 STEP Entities

The node instances are identical to Section 5.4.3; however, the node_group has a different ID. Figure 49 shows the STEP entities for the first 3 nodes and the node_group instance.

```

#90= NODE('1', (#88), #46, #77);
#88= CARTESIAN_POINT('1', (0., -2., 1.));

#99= NODE('2', (#97), #46, #77);
#97= CARTESIAN_POINT('2', (1., -2., 1.));

#103= NODE('3', (#101), #46, #77);
#101= CARTESIAN_POINT('3', (2., -2., 1.));

#625= NODE_GROUP('', 'ALL', #77, (#90, #99, #103, #107, #111, #115, #119, #123,
#127, #131, #135, #139, #143, #147, #151, #155, #159));
#626= ID_ATTRIBUTE('ALL', #625);

```

Figure 49 STEP File Fragment for Nodes and Node_Group

6.5 Element Definition

A linear bar element is defined between each grid point to supply stiffness to the grid points. Bar elements are capable of supplying stiffness to the full 6 degrees of freedom at each grid point. Again, this discussion is related to the definition of the FEA solver element and not the AP209 ed2 entity of the same name. The same `curve_3d_element_representation` entity is used as for the pilot model ATS1 but the property definitions are populated differently as is the element descriptor to reflect the additional capabilities provided by this solver element type.

6.5.1 STEP Diagram

The structure for a single element is identical to Section 5.5.1, but the related instances that can be shared from one element to another, such as element property, are different. Figure 50 illustrates that difference.

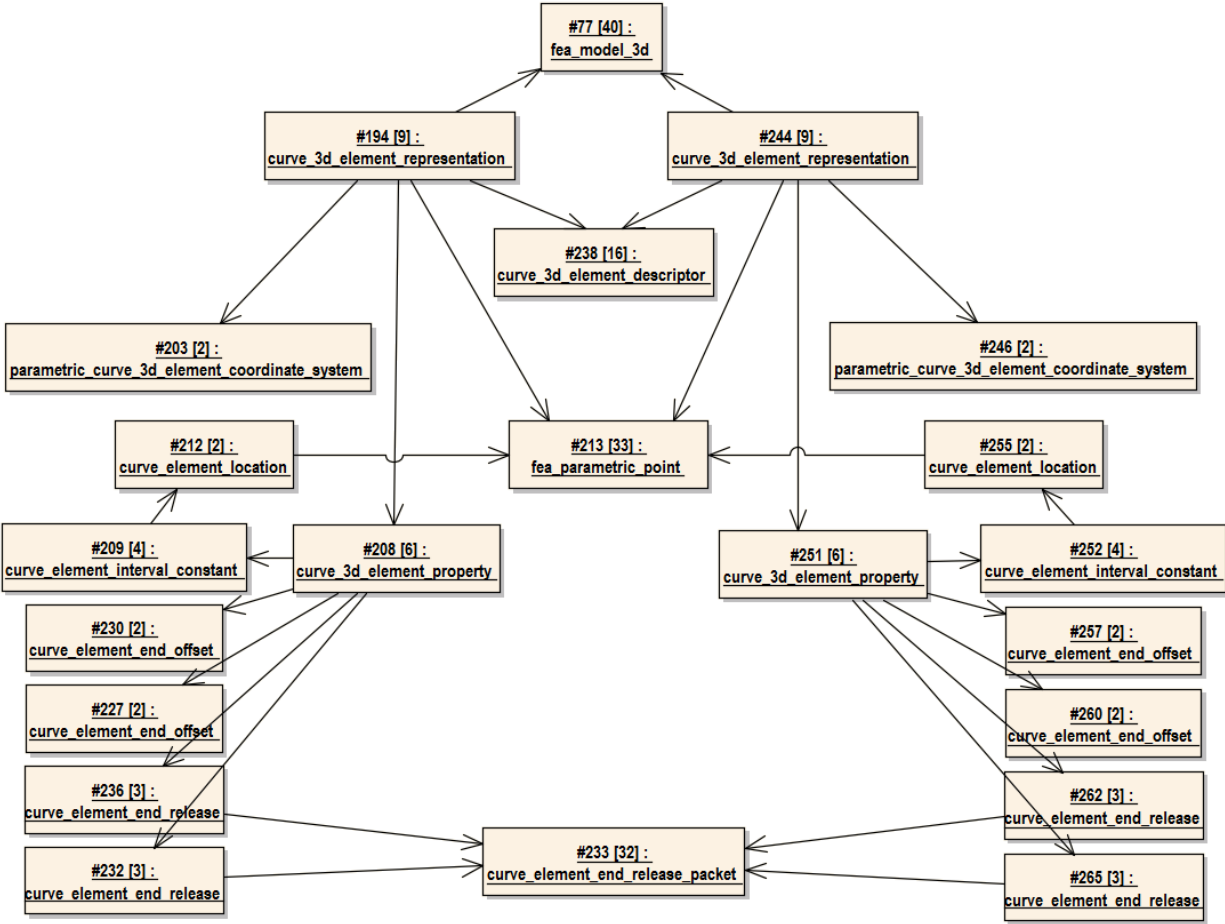


Figure 50 Structure of Curve_3d_element_representation for ATSS2

Many of the common instances have been hidden in this diagram. The main difference of note is that because NASTRAN CBAR elements support individual offsets and end releases defined on each element, there could exist a unique curve_3d_element_property for each element. Those properties must then reference unique curve_element_interval_constants and individual end releases and offsets. A single fea_parametric_point can be used since there are no multi section bars in this model. A single instance of the curve_element_end_release_packet is also used. This is possible because all end releases on all elements are blank and the single instance of curve_element_end_release_packet is populated with a freedom enumeration equal to '.NONE.'. This is discussed further in Section 6.

Additional optimization of the STEP output could be performed on the curve_3d_element_property instances to reuse more instances for common element property IDs. To take advantage of this optimization, key or hashing schemes should be employed to determine equality of the combined interval definition, property id, end release and end offset information as found in the parsed solver input. Optimization of output is a complex topic that is only introduced in this document and is an active area of discussion and development in the STEP community.

6.5.2 FE Model Input

There are 16 NASTRAN elements defined using the CBAR input card shown in Figure 51. The bar elements used in this pilot model supply stiffness for all 6 degrees of freedom at each grid point. CBAR elements can reference property cards that either define the beam section constants directly (PBAR) or define a geometric cross section shape (PBARL). The PBAR property is used for the initial pilot models.

	1	2	3	4	5	6	7	8	9	10
CBAR	EID	PID	GA	GB	X1	X2	X3	OFFT		
	PA	PB	W1A	W2A	W3A	W1B	W2B	W3B		
CBAR*	1		1		1		2			
*	0.		7.54979-8		1.					
CBAR*	2		1		2		3			
*	0.		7.54979-8		1.					

Figure 51 NASTRAN Input Specification for 1D CBAR Element

Another variation introduced with this element type is the use of double-field input where each logical field is physically 16 characters long. Therefore, two lines of input are required to express each line of input in the card diagrams shown.

Additionally, an orientation vector (X1, X2, X3) is introduced that necessitates individual parametric_curve_3d_element_coordinate_systems. This orientation vector clocks the local element coordinate system to locate the reference directions for complex section properties such as those shown in Figure 52. The orientation vector data also contains a very small, near zero, real value. This value was included to test small value handling during the translation process.

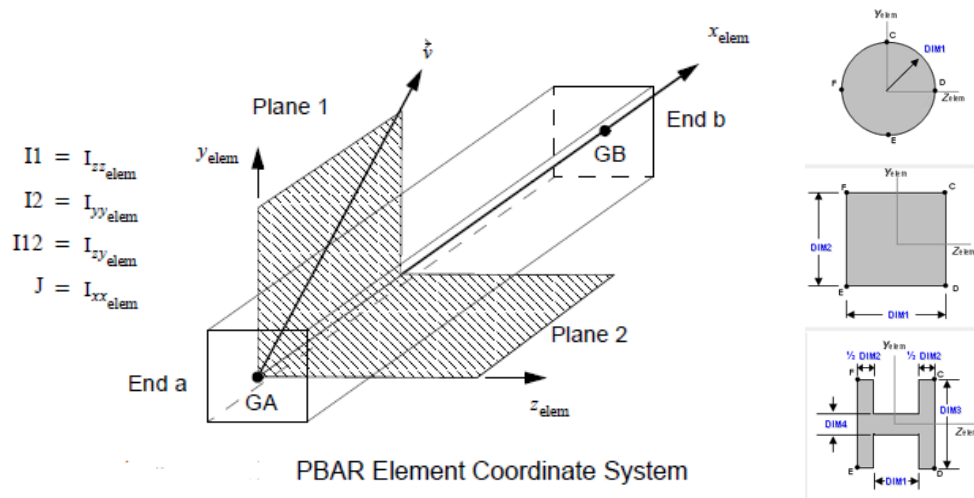


Figure 52 Element Coordinate System for NASTRAN CBAR Property Reference

6.5.3 STEP Entities

The 1-dimensional bar element maps to the same curve_3d_element_representation entity as the ATS1 rod element model. The behavioral aspects are specified differently than in Section 5.5.3 through use of

a `curve_3d_element_descriptor` with additional enumerated purposes defined. The additional behaviors account for the bending and shear capabilities of the NASTRAN CBAR element. Again, the descriptor text has been formatted for readability and generally will not appear as shown by the STEP files in Figure 53.

```
#194= CURVE_3D_ELEMENT_REPRESENTATION('1', (#203,#213),#195, (#90,#99),#77,#238,#208,#163);
#244= CURVE_3D_ELEMENT_REPRESENTATION('2', (#246,#213),#195, (#99,#103),#77,#238,#251,#163);

"#238= CURVE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER., 'LINEAR_CURVE.CBAR*', (
(ENUMERATED_CURVE_ELEMENT_PURPOSE(.AXIAL.)),
(ENUMERATED_CURVE_ELEMENT_PURPOSE(.Y_Y_BENDING.)),
ENUMERATED_CURVE_ELEMENT_PURPOSE(.Z_Z_BENDING.)),
(ENUMERATED_CURVE_ELEMENT_PURPOSE(.TORSION.)),
(ENUMERATED_CURVE_ELEMENT_PURPOSE(.X_Y_SHEAR.)),
ENUMERATED_CURVE_ELEMENT_PURPOSE(.X_Z_SHEAR.))
);"
```

Figure 53 STEP Entities for CBAR Element and Element Descriptor

The local element coordinate system instances referenced by the two element representations above are shown in Figure 54. Again, there are opportunities for optimization of the STEP output using the orientation values to determine equality of the direction instances.

```
#203= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#204);
#204= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#205);
#205= DIRECTION('dxy', (0.,7.549790000000000E-8,1.));

#246= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#247);
#247= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#248);
#248= DIRECTION('dxy', (0.,7.549790000000000E-8,1.));

#213= FEA_PARAMETRIC_POINT('', (1.,0.,0.));

#195= /* GEOMETRIC_REPRESENTATION_CONTEXT+PARAMETRIC_REPRESENTATION_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)PARAMETRIC_REPRESENTATION_CONTEXT()
REPRESENTATION_CONTEXT('REP_CONTEXT_FEA','3D'));
```

Figure 54 CBAR Parametric Element Coordinate System and Context

6.6 Property Definition

The property definition for the ATS2 pilot model follows a similar structure as for the ATS1 model with the exception of the possibility of unique property instances to account for information that may be specified on individual element. This topic was touched upon in Section 6.5.1 and is not repeated here. The indexing and retrieval schemes that are employed to take advantage of instance reuse are implementation dependent and beyond the intent of this pilot model discussion. However, every effort should be taken to capture the modeling intent of the source FEA model construction when possible to assist with solver input reconstruction.

In situations that require multiple property entities to be created in the AP209 ed2 data model where only a single property was read from the source data, the property metadata such as name and description fields should be used to indicate the source association of the multiple properties. Typically, these types of weak relationship expressions are not to be relied upon for computer processing but are of great value to the end consumer of the FEA information and should be retained.

6.6.1 STEP Diagram

The diagram for a single property is identical to that shown in Section 5.6.1. However, there are multiple instances of curve_3d_element_property and many more terms in the section definition are non-zero to reflect the additional bending properties of the CBAR element.

6.6.2 FE Model Input

The NASTRAN input model shown in Figure 55 has only one PBAR defined which means that all the elements share the same section properties.

	1	2	3	4	5	6	7	8	9	10
PBAR	PID	MID	A	I1	I2	J	NSM			
	C1	C2	D1	D2	E1	E2	F1	F2		
	K1	K2	I12							
PBAR	1	1	8.	2.667	10.667	0.	0.			
	1.	2.	1.	-2.	0.	0.	0.	0.		
			0.							

Figure 55 NASTRAN Input Specification for 1D PBAR

Similar to the ATS1 pilot model, the 'J' torsional term is specified as zero. The C and D non-zero fields are stress recovery locations in the plane of the cross section and are not used in this model.

6.6.3 STEP Entities

The STEP AP209 ed2 property listing for the two properties shown in the diagram are shown in Figure 56. The order displayed is different in that the common instances are listed at the end.

```
#208= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.1','',( #209), (#227,#230), (#232,#236));

#209= CURVE_ELEMENT_INTERVAL_CONSTANT(#212,#210,#220);
#212= CURVE_ELEMENT_LOCATION(#213);
#210= EULER_ANGLES((0.,0.,0.));
#227= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#230= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#232= CURVE_ELEMENT_END_RELEASE(#35, (#233));
#236= CURVE_ELEMENT_END_RELEASE(#35, (#233));

#251= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.2','',( #252), (#257,#260), (#262,#265));

#252= CURVE_ELEMENT_INTERVAL_CONSTANT(#255,#253,#220);
#255= CURVE_ELEMENT_LOCATION(#213);
#253= EULER_ANGLES((0.,0.,0.));
#257= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#260= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#262= CURVE_ELEMENT_END_RELEASE(#35, (#233));
#265= CURVE_ELEMENT_END_RELEASE(#35, (#233));

#233= CURVE_ELEMENT_END_RELEASE_PACKET(ENUMERATED_CURVE_ELEMENT_FREEDOM(.NONE.),0.);
#213= FEA_PARAMETRIC_POINT('',(1.,0.,0.));

#220= CURVE_ELEMENT_SECTION_DERIVED_DEFINITIONS('PBAR.1_0',
0.,
8.,
(CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
(2.667,10.667,0.),
0.,
CONTEXT_DEPENDENT_MEASURE(0.),
(CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
(CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
(CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),
CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
```

Figure 56 STEP File Fragment for Curve 3D Element Property Structure (PBAR)

Again the topics of instance reuse and output optimization are mentioned due to the obvious repetition of identical instances in this property listing.

6.7 Material Definition

The material definition and discussion is identical to that presented in Section 5.7.

6.7.1 STEP Diagram

Identical to Section 5.7.1.

6.7.2 FE Model Input

Identical to Section 5.7.2

6.7.3 STEP Entities

The instances for the material definition shown in Figure 57 are identical to Section 5.7.3.

```
#163= ELEMENT_MATERIAL('MAT1.1','Fea Material',(#175,#183,#189));

#175= FEA_MATERIAL_PROPERTY_REPRESENTATION(#176,#178,#171);
#179= DESCRIPTION_ATTRIBUTE('Elasticity',#175);
#176= MATERIAL_PROPERTY('MAT1.1.0',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#178= REPRESENTATION('representation_id_2',(#173),#36);
#173= FEA_LINEAR_ELASTICITY('',FEA_ISOTROPIC_SYMMETRIC_TENSOR4_3D((10000000.,0.33)));

#183= FEA_MATERIAL_PROPERTY_REPRESENTATION(#184,#185,#171);
#186= DESCRIPTION_ATTRIBUTE('MassDensity',#183);
#184= MATERIAL_PROPERTY('MAT1.1.1',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#185= REPRESENTATION('representation_id_3',(#182),#36);
#182= FEA_MASS_DENSITY('',0.000254);

#189= FEA_MATERIAL_PROPERTY_REPRESENTATION(#190,#191,#171);
#192= DESCRIPTION_ATTRIBUTE('TangentCTE',#189);
#190= MATERIAL_PROPERTY('MAT1.1.2',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#191= REPRESENTATION('representation_id_4',(#188),#36);
#188= FEA_TANGENTIAL_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION('',ISOTROPIC_SYMMETRIC_TENSOR2_3D(1.30E-5));
```

Figure 57 STEP Fragment for Isotropic Material Properties

7 Pilot Model ATS3 – 2D Shell Element

The ATS3pilot model composition is illustrated in Figure 58.

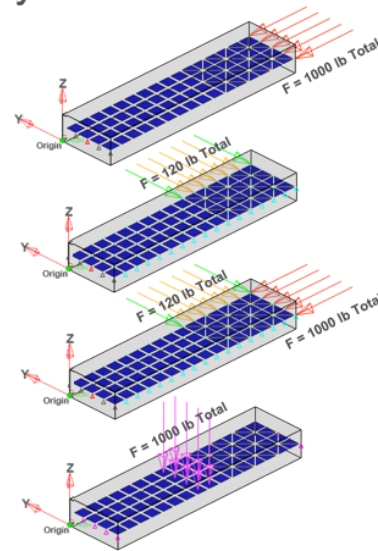
- Shell model with wider variety of boundary condition and load combinations

- FE model composition

■ Elements:	40	CQUAD4
	48	CTRAI3
■ Nodes:	85	GRID
■ Loads:	12	FORCE
	8	PLOAD2 (normal pressure)
	3	LOAD
■ Boundary:	104	SPC1
	2	SPCADD
■ Property:	1	PSHELL
■ Material:	1	MAT1 (aluminum)

- Subcase and output requests

■ Subcases:	4	SUBCASE
■ Boundary:	4	SPC
■ Loads:	4	LOAD
■ Output:	16	GPFORCE (global)
		DISPLACEMENT
		SPCFORCES
		STRESS



*See listing for output parameters

Figure 58 Pilot Model Content Summary ATS3

Additional details of the model are:

- All nodes defined in basic coordinate system, no local systems defined
- Shell element normal pressure load case (-z) direction
- Uses inclusive continuous node range definition in boundary condition specification
- Rich combinations of boundary conditions and load cases to model beam behaviors

7.1 Product Definition Shape

The structure of the product definition entity graph is shown in Figure 59 for the 2D shell element ATS3 pilot model. It is very similar to the previous pilot models except that there are no local coordinate systems.

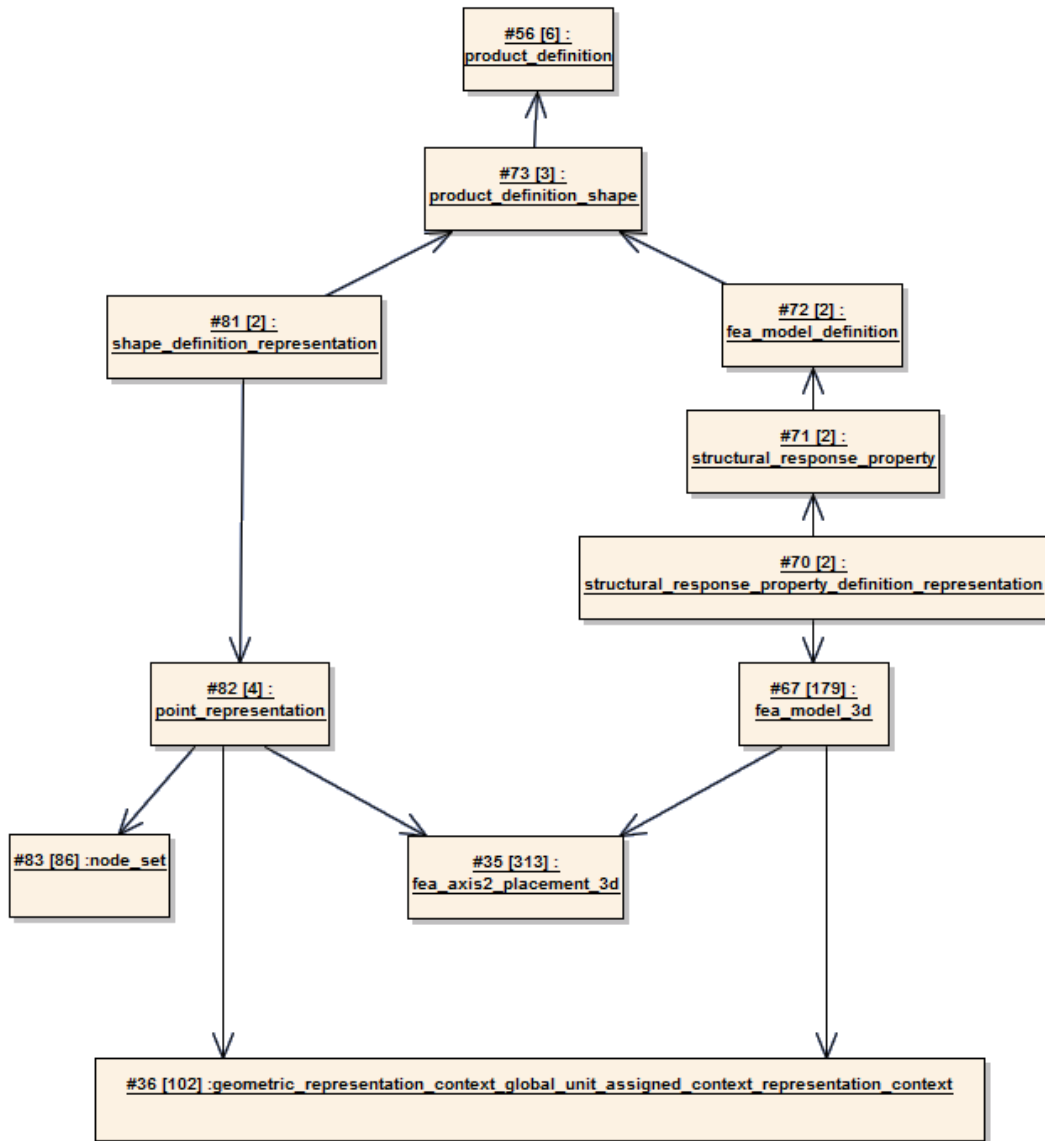


Figure 59 Basic coordinate system used for finite element model geometric entities

7.2 FEA Model

The fea_model_3d entity is unchanged from the prior examples. However, as noted above, a single fea_axis2_placement3d is shared between the fea_model_3D and the point representation. This indicates that all geometric entities related to the FEM are founded with respect to the implied basic NASTRAN coordinate system. No transformation operators are required.

7.3 Coordinate System

No local coordinate systems are defined for the ATS3 model. Only the basic coordinate system is used as shown in Figure 59. According to the recommended practice document, the `point_representation` and associated `node_set` are optional in this case since all nodes are founded with respect to the `fea_model_3d` and associated `fea_axis2_placement_3d`. However, for consistency, the `point_representation` and associated `node_set` are instantiated and associated as shown above. In this instance, the `node_set` will have a list of references to all the nodes.

7.3.1 STEP Diagram

No additional diagram needed for coordinate systems.

7.3.2 FE Model Input

The NASTRAN basic coordinate system is an implied system and no user input is required.

7.3.3 STEP Entities

The STEP entities used to define the basic coordinate system are shown in Figure 60 for reference. Note the use of the complex context entity. In this type of EXPRESS construct, multiple entities can be aggregated into a single instance to indicate an inseparable relationship and to provide a single reference to be used throughout the STEP model.

```
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,.CARTESIAN.,'FEA_BASIC_COORD_SYSTEM.0');

#36= /* GEOMETRIC_REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)
 GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,#12,#17,#7,#8,#11,#26,#20,#10,#9))
 REPRESENTATION_CONTEXT('FEA_BASIC_COORD_SYSTEM.0','3d'));

#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));

#82= POINT_REPRESENTATION('point_representation_name_1',(#83,#35),#36);
```

Figure 60 STEP File Fragment for Basic Coordinate System

7.4 Node Definition

The nodes defined for the ATS3 model represent the same 16 inch prismatic shape as the prior models; however, the use of shell elements requires a 2-dimensional geometric layout of nodes. There are 85 geometric nodes defined in the model (17 rows of 5 nodes). All the nodes are located in a plane located at the mid-surface of the shape ($Z=1.0$).

7.4.1 STEP Diagram

The node instance diagram provided by Figure 61 can be compared with the one presented in Figure 19. Note the differences in these diagrams that reflect the different geometric founding. The nodes are related to the FEA model which in turn is related to the single instance of `fea_axis2_placement_3d` that represents the basic coordinate system. The `node_set` and `point_representation` provide a redundant path from all the nodes to the single instance of `fea_axis2_placement_3d` for geometric founding. This redundancy is why the `point_representation` and `node_set` are optional when only one coordinate system is used.

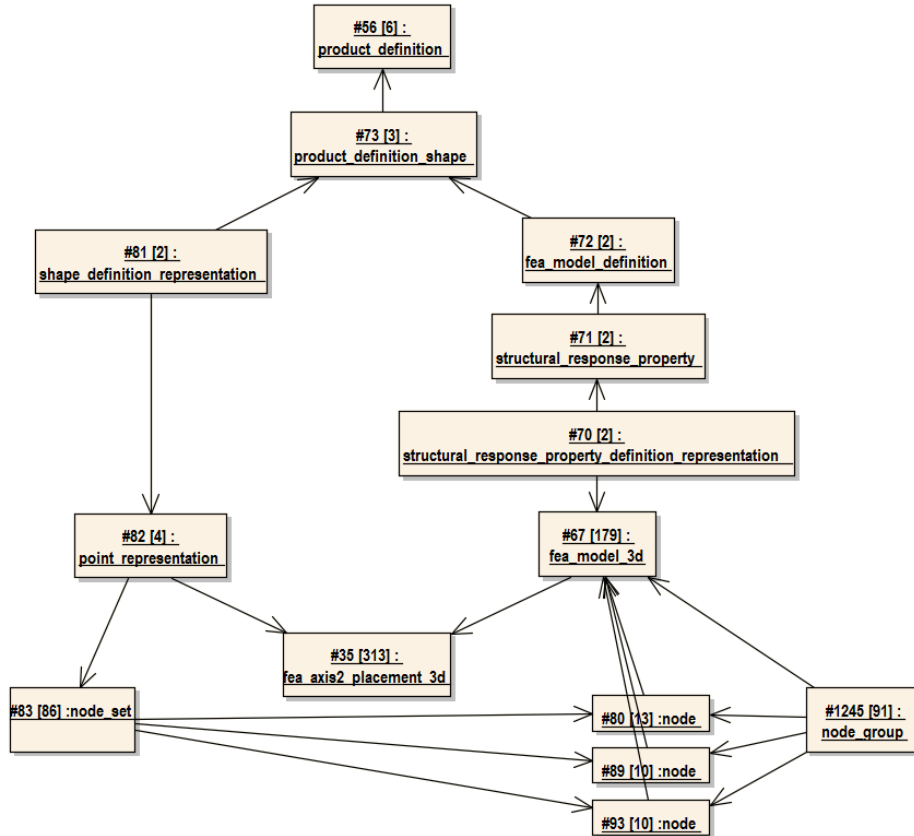


Figure 61 STEP Node Entity Relationships to other FEA Instances

7.4.2 FE Model Input

The nodes shown in Figure 61 are created as a result of the NASTRAN input shown in Figure 62. Note that both the 'CP' and 'CD' attributes are blank which implies use of the basic NASTRAN coordinate system.

	1	2	3	4	5	6	7	8	9	10
	GRID	ID	CP	X1	X2	X3	CD	PS	SEID	
GRID*	1					-6.24022-8		-4.		
*	1.									
GRID	2			1.	-4.	1.				
GRID	3			2.	-4.	1.				

Figure 62 NASTRAN Card Image for Grid Points

This input also illustrates the use of mixed format input in the NASTRAN source file. The first grid uses the 16-character wide data fields which results in a second line of input to define the grid point. The use of double field input is necessary to minimize numeric errors that arise when larger values differ by a small value. This scenario is common in vehicle modeling when coordinates are used for large vehicles with small detailed model features. In these cases, the use of the NASTRAN short field (8-character) format may cause numeric errors due to collapsed element definitions.

7.4.3 STEP Entities

The translated NASTRAN nodes are listed in Figure 63. The three references for each node instance represent the associated cartesian_point (#78 for node number 1), the 3-dimensional geometric_representation_context (#36), and the fea_model_3d (#67).

```
#80= NODE('1', (#78), #36, #67);
#78= CARTESIAN_POINT('1', (-6.240220000000000E-8, -4., 1.));

#89= NODE('2', (#87), #36, #67);
#87= CARTESIAN_POINT('2', (1., -4., 1.));

#93= NODE('3', (#91), #36, #67);
#91= CARTESIAN_POINT('3', (2., -4., 1.));

#83= NODE_SET('node_set_name_1', (#80, #89, #93, #97, #101, #105, #109, #113,
#117, #121, #125, #129, #133, #137, #141, #145, #149, #153, #157, #161, #165, #169,
#173, #177, #181, #185, #189, #193, #197, #201, #205, #209, #213, #217, #221, #225,
#229, #233, #237, #241, #245, #249, #253, #257, #261, #265, #269, #273, #277, #281,
#285, #289, #293, #297, #301, #305, #309, #313, #317, #321, #325, #329, #333, #337,
#341, #345, #349, #353, #357, #361, #365, #369, #373, #377, #381, #385, #389, #393,
#397, #401, #405, #409, #413, #417, #421));
```

Figure 63 STEP File Fragment for ATS3 Nodes

7.5 Element Definition

The element definition for ATS3 introduces 4-sided quadrilateral and 3-sided triangular shell elements. These elements can support 6 degrees of freedom at each node used in the definition of the element connectivity. This model uses a linear formulation for these shell elements which requires that only corner nodes be defined for each element. Higher-order element types are possible when additional nodes are used on element edges or faces. These types of elements support quadratic and cubic interpolation functions in the element formulation but are not used in this pilot study. Both the element shape and order are defined in the associated element descriptor instance.

7.5.1 STEP Diagram

The element diagram for the first two quadrilateral elements is shown in Figure 64. The relationship to the nodes for these two elements indicates that they are adjacent and share the edge defined by nodes 2 and 13 (STEP instance IDs #89 and #133). In the solver model, these elements use a common physical property and material property as indicated by the relationships to the surface_element_property and element_material instances.

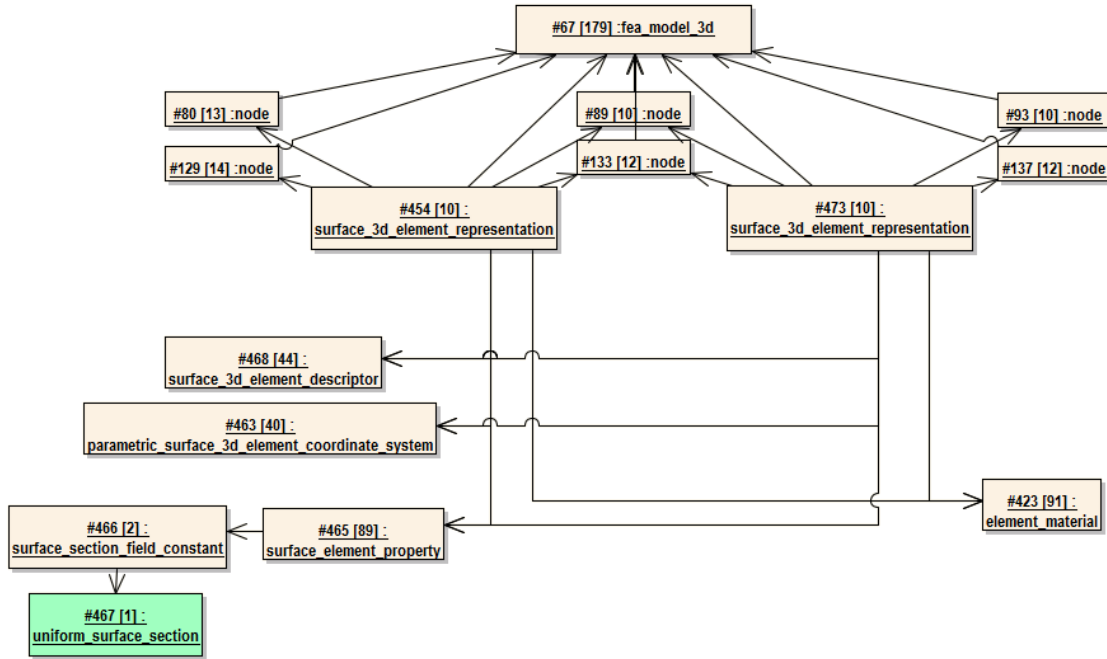


Figure 64 STEP Surface 2D Element Definition and Related Data Model Structures

A detail that may not be immediately apparent is the different number of associations indicated by the node label in brackets [] shown on this diagram (eg. node #89 has [10] associations and node #129 has [14]). This indicates that node #129 is referenced by additional entities such as loads or boundary conditions. It could also be due to differences in mesh topology such as an external corner node or interior node shared by many elements. There are many possibilities to explain different association counts. Figure 65 illustrates this point and shows the additional references on node #129 are in fact boundary conditions defined by single_point_constraint_elements.

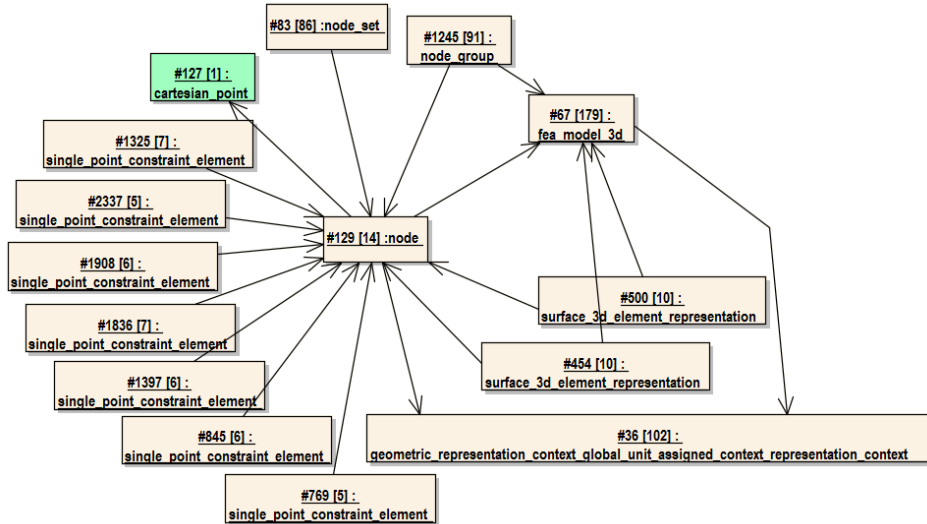


Figure 65 STEP Instances Associated to NODE #129

Similar figures could be constructed for the triangular element definitions with the primary difference being that only 3 nodes will be in the item_list for the surface_3d_element_representation.

7.5.2 FE Model Input

The NASTRAN input for shell elements is shown in Figure 66. Both quadrilateral and triangular element input and STEP listings are presented.

1	2	3	4	5	6	7	8	9	10
CQUAD4	EID	PID	G1	G2	G3	G4	THETA or MCID	ZOFFS	
		TFLAG	T1	T2	T3	T4			

1	2	3	4	5	6	7	8	9	10
CTRIA3	EID	PID	G1	G2	G3	ZOFFS	THETA or MCID		
		TFLAG	T1	T2	T3				

CQUAD4	1	1	1	2	13	12			
CQUAD4	2	1	2	3	14	13			
CTRIA3	41	1	64	22	11				

Figure 66 NASTRAN Card Image for Quadrilateral and Triangular Linear Elements

The solver attributes up to the THETA field are familiar (element ID, property ID, Grid ID connectivity list). The THETA field defines orientation of an element material direction, ZOFFS defines an offset of the plane of the element along the element normal direction, TFLAG and T(i) are used to define membrane thicknesses at the grid points for tapered elements. None of these additional fields are used in the pilot study but the material orientation is commonly used and therefore discussed below.

The THETA field can contain either an angle or a coordinate system ID that orients the element material coordinate system. If an angle is defined, the material coordinate system is rotated by this angle from the element coordinate system about the element normal. If a coordinate system ID is specified, the X-axis of that system is projected onto the plane of the element which defines a vector direction relative to the element coordinate system x-axis. If blank, the element material coordinate system is the element coordinate system. This is especially important when composite properties or any orthotropic or anisotropic materials are used. The AP209 ed2 data model supports specification of these types of element material coordinate systems; however, the ATS3 pilot model does not define a separate material coordinate direction. Therefore, a parametric_surface_3d_element_coordinate_system instance as shown in Figure 67 is shared for each element type.

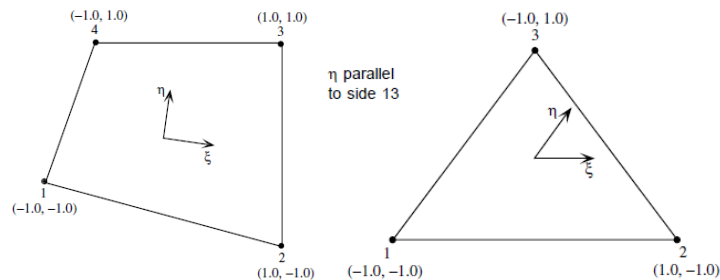


Figure 67 Parametric Element Coordinate Systems for Quadrilateral and Triangular Elements

The fundamental concept is that the coordinate systems are parametric and can be computed using the geometric properties of the element instance. The details of element coordinate system development are described in the NASTRAN quick reference manual or theoretical manuals but is beyond the scope of this document. The Part 104 document discusses the selection of element coordinate systems in great detail in Section 5.8 Element topologies and in Section 5.9 Element coordinate systems. A thorough review of these sections is recommended.

7.5.3 STEP Entities

The STEP file listing of the elements and related entities for the ATS3 model are shown in Figure 68, and the EXPRESS schema definitions for these entities are shown in Figure 69 and Figure 70.

```
#454= SURFACE_3D_ELEMENT_REPRESENTATION('1', (#463), #455, (#80, #89, #133, #129), #67, #468, #465, #423);
#473= SURFACE_3D_ELEMENT_REPRESENTATION('2', (#463), #455, (#89, #93, #137, #133), #67, #468, #465, #423);
#590= SURFACE_3D_ELEMENT_REPRESENTATION('41', (#592), #455, (#329, #169, #125), #67, #594, #465, #423);

#468= SURFACE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER., 'LINEAR_QUADRILATERAL.CQUAD4', (
  (ENUMERATED_SURFACE_ELEMENT_PURPOSE(.MEMBRANE_DIRECT.),
  ENUMERATED_SURFACE_ELEMENT_PURPOSE(.MEMBRANE_SHEAR.)),
  (ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_DIRECT.),
  ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_TORSION.)),
  (ENUMERATED_SURFACE_ELEMENT_PURPOSE(.NORMAL_TO_PLANE_SHEAR.))
), .QUADRILATERAL.);
#594= SURFACE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER., 'LINEAR_TRIANGLE.CTRIA3', (
  (ENUMERATED_SURFACE_ELEMENT_PURPOSE(.MEMBRANE_DIRECT.),
  ENUMERATED_SURFACE_ELEMENT_PURPOSE(.MEMBRANE_SHEAR.)),
  (ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_DIRECT.),
  ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_TORSION.)),
  (ENUMERATED_SURFACE_ELEMENT_PURPOSE(.NORMAL_TO_PLANE_SHEAR.))
), .TRIANGLE.);

#463= PARAMETRIC_SURFACE_3D_ELEMENT_COORDINATE_SYSTEM('', 1, 0.);
#592= PARAMETRIC_SURFACE_3D_ELEMENT_COORDINATE_SYSTEM('', 1, 0.);

#455= /* GEOMETRIC_REPRESENTATION_CONTEXT+PARAMETRIC_REPRESENTATION_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3) PARAMETRIC_REPRESENTATION_CONTEXT()
REPRESENTATION_CONTEXT('REP_CONTEXT_FEA', '3D'));
```

Figure 68 STEP File Fragment for Surface 3D Elements and Related Entities

```
ENTITY Element_Descriptor
  SUPERTYPE OF (
    ONEOF (
      Volume_3d_Element_Descriptor,
      Axisymmetric_Volume_2d_Element_Descriptor,
      Plane_Volume_2d_Element_Descriptor,
      Surface_3d_Element_Descriptor,
      Axisymmetric_Surface_2d_Element_Descriptor,
      Plane_Surface_2d_Element_Descriptor,
      Curve_3d_Element_Descriptor,
      Axisymmetric_Curve_2d_Element_Descriptor,
      Plane_Curve_2d_Element_Descriptor ) );
  topology_order : Element_Order;
  description : Text;
END ENTITY;

ENTITY Surface_3d_Element_Descriptor
  SUBTYPE OF ( Element_Descriptor );
  purpose : SET [1 : ?] OF SET [1 : ?] OF Surface_Element_Purpose;
  shape : Element_2d_Shape;
END ENTITY;
```

Figure 69 EXPRESS Schema for Surface 3D Element Descriptor

The schema listing in Figure 69 has not been flattened and the supertype-subtype relationships are explicitly defined in separate entity definitions that must be navigated to understand the full definition of a specialized class such as `surface_3d_element_descriptor`. Both styles of schema have been presented in this document to familiarize the reader with the alternate formats. The SMRL uses the supertype-subtype format.

Additional type information related to the element descriptors is used to populate the attributes. This information defines many behavior aspects of the elements as appropriate for the particular solver used as the data source or the intended target solver format.

```
TYPE Element_Order = ENUMERATION OF
( Linear_Order,
  Quadratic_Order,
  Cubic_Order );
END_TYPE;

TYPE Surface_Element_Purpose = SELECT
( Enumerated_Surface_Element_Purpose,
  Application_Defined_Element_Purpose );
END_TYPE;

TYPE Enumerated_Surface_Element_Purpose = ENUMERATION OF
( Membrane_Direct,
  Membrane_Shear,
  Bending_Direct,
  Bending_Torsion,
  Normal_To_Plane_Shear );
END_TYPE;

TYPE Element_2d_Shape = ENUMERATION OF
( Quadrilateral,
  Triangle );
END_TYPE;
```

Figure 70 EXPRESS Schema Definition for Surface Element 3D Element Descriptor Attributes

Use of element descriptors for describing element behavior in STEP is a mechanism to provide enumerated terms that can be used to recreate some (but not all) of the mathematics used in the element formulation (not the actual mathematical formulations). As an example, the NASTRAN CQUAD4 and TRIA3 elements have fundamental differences in element formulations that effect the variation of strain over the surface of the element. However, the descriptors for each enumerate similar capabilities and behaviors.

To capture these mathematical differences, a lower level construct in AP209 ed2 can be used to describe the element matrix integration schemes involved in the element formulation. Section 5.10 Element matrix integration of Part 104 details these aspects of element formulation and is the starting point for further investigation of this topic. However, this is an advanced topic that is not covered in any more detail for the pilot study.

The full EXPRESS schema definition of the surface_3d_element_representation entity is complex and makes extensive use of WHERE rules in the schema definition to ensure referential integrity of the AP209 ed2 element data model. Figure 71 lists the specialized surface_3d_element_representation and its immediate supertype, element_representation.

```

ENTITY Element_Representation
  SUPERTYPE OF (
    ONEOF (
      Volume_3d_Element_Representation,
      Axisymmetric_Volume_2d_Element_Representation,
      Plane_Volume_2d_Element_Representation,
      Surface_3d_Element_Representation,
      Axisymmetric_Surface_2d_Element_Representation,
      Plane_Surface_2d_Element_Representation,
      Curve_3d_Element_Representation,
      Axisymmetric_Curve_2d_Element_Representation,
      Plane_Curve_2d_Element_Representation,
      Point_Element_Representation,
      Directionally_Explicit_Element_Representation,
      Explicit_Element_Representation,
      Substructure_Element_Representation ) )
  SUBTYPE OF ( Representation );
  node_list : LIST [1 : ?] OF Node_Representation;
  WHERE
    wr1:( SIZEOF( QUERY ( item <* node_list | ( ( 'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'GEOMETRIC_NODE' )
      IN TYPEOF( item ) ) ) ) = 0 );
END_ENTITY;

ENTITY Surface_3d_Element_Representation
  SUBTYPE OF ( Element_Representation );
  model_ref : Fea_Model_3d;
  element_descriptor : Surface_3d_Element_Descriptor;
  property : Surface_Element_Property;
  material : Element_Material;
  UNIQUE
    url : model_ref, SELF\Representation.name;
  WHERE
    wr1: ( ( SIZEOF( QUERY ( item <* SELF\Representation.items | ( ( 'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' +
      'PARAMETRIC_SURFACE_3D_ELEMENT_COORDINATE_SYSTEM' ) IN TYPEOF( item ) ) ) ) + SIZEOF( QUERY ( item <* SELF\
      Representation.items | ( ( 'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' +
      'CONSTANT_SURFACE_3D_ELEMENT_COORDINATE_SYSTEM' ) IN TYPEOF( item ) ) ) ) + SIZEOF( QUERY ( item <* SELF\
      Representation.items | ( ( 'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' +
      'ALIGNED_SURFACE_3D_ELEMENT_COORDINATE_SYSTEM' ) IN TYPEOF( item ) ) ) ) ) = 1 );
    wr2: ( SIZEOF( QUERY ( item1 <* material.properties | ( SIZEOF( QUERY ( item2 <*
      item1\Property_Definition_Representation.
      used_representation.items | ( SIZEOF( [
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_LINEAR_ELASTICITY' ,
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_MASS_DENSITY',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_AREA_DENSITY',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_TANGENTIAL_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_SECANT_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_MOISTURE_ABSORPTION',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_SHELL_MEMBRANE_STIFFNESS',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_SHELL_BENDING_STIFFNESS',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_SHELL_MEMBRANE_BENDING_COUPLING_STIFFNESS',
        'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.' + 'FEA_SHELL_SHEAR_STIFFNESS'] * TYPEOF( item2 ) ) = 1 ) ) )
      = 1 ) ) ) >= 1 );
    wr3: ( 'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF.PARAMETRIC_REPRESENTATION_CONTEXT' IN TYPEOF( SELF\
      Representation.context_of_items ) );
    fu1: Required_2d_Nodes( SELF\Element_Representation.node_list, Element_Descriptor.shape, Element_Descriptor\
      Element_Descriptor.topology_order );
END_ENTITY;

```

Figure 71 EXPRESS Schema Definition for Surface_3D_Element_Representation

7.6 Property Definition

The property definitions for surface 3D elements are not as complex as the 1D elements but require some explanation. For the AT3 pilot model, a single NASTRAN property is used that specifies a uniform thickness value normal to the 2-dimensional plane of each element. This thickness provides the missing 3rd dimension for surface based shell element models of 3 dimensional volumes.

This is an approximation to a full 3D volume model, but it provides an efficient mechanism to reduce the size of the analysis models by eliminating the redundant thickness dimension from the geometrical definition of the FEM. The accuracy of a FEM solution using this approximation is dependent upon many factors, one of which is that the length and width of the element should be much greater than the thickness. This ‘thin shell’ assumption is not strictly followed in this pilot model, however, the effect is on the values produced by the solution process, not the representation of the model and solution in a AP209 ed2 data model. In other words, the reader is cautioned that bad solution data can be represented in the STEP data model as easily as any other data format.

7.6.1 STEP Diagram

The instance diagram for the `surface_element_property` is no more complex than the instances shown in Figure 64. All element instances are included in Figure 72 to illustrate the shared property usage.

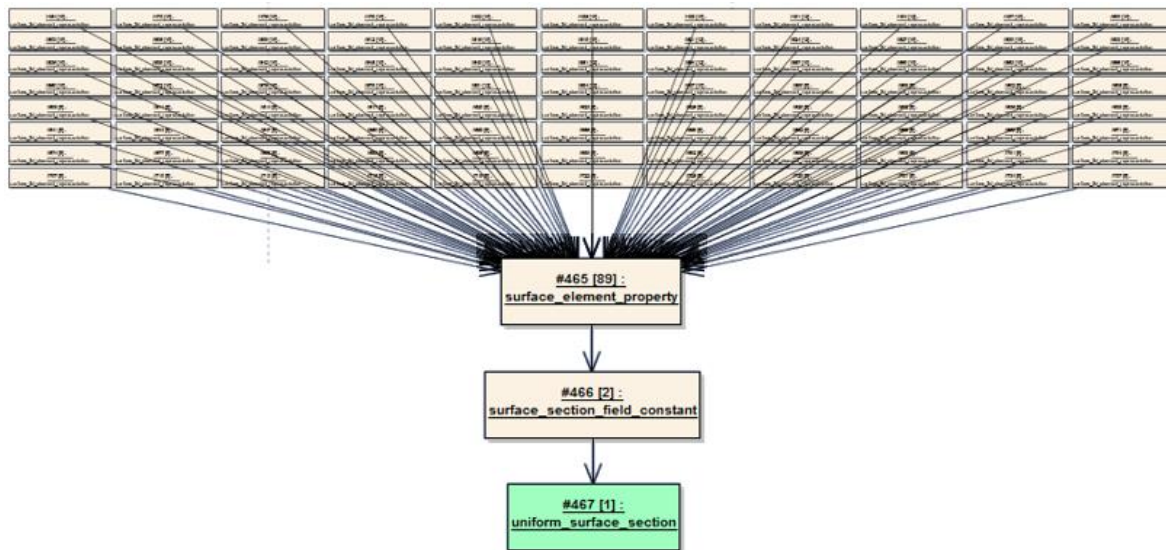


Figure 72 STEP Instance Diagram Showing Single Shared `Surface_Element_Property`

The `uniform_surface_section` and `surface_section_field_constant` entities found in this diagram represent a constant thickness value over the surface of the element. Non-uniform section information (such as tapered thickness over the element) can be represented by specifying a list of `uniform_surface_section` entities in a `surface_section_field_varying` entity. The reader is referred to the recommended practice document and the schema definitions in the SMRL. Additionally, other properties related to the behavior of the through-the-thickness section are provided and can be used to represent further the behavior of the element. If any of these additional properties is supplied by an individual element (such as element offset), unique field and section definitions must be created and related to a unique `surface_element_property`.

7.6.2 FE Model Input

The single NASTRAN property card for the ATS3 model is shown in Figure 73. Only the material and thickness attributes are used in the pilot study models.

1	2	3	4	5	6	7	8	9	10
PSHELL	PID	MID1	T	MID2	12I/T**3	MID3	TS/T	NSM	
	Z1	Z2	MID4						
PSHELL	1	1	2.	1		1			

Figure 73 NASTRAN Card Input for PSHELL Property

7.6.3 STEP Entities

The STEP instances shown in Figure 74 represent the shell property for the ATS3 model. The uniform_surface_section listing has been reformatted for easy comparison with the EXPRESS schema figure for these entities.

```
#465= SURFACE_ELEMENT_PROPERTY('PSHELL.1','',#466);
#466= SURFACE_SECTION_FIELD_CONSTANT(#467);
#467= UNIFORM_SURFACE_SECTION(
    UNSPECIFIED_VALUE(.UNSPECIFIED.),
    UNSPECIFIED_VALUE(.UNSPECIFIED.),
    UNSPECIFIED_VALUE(.UNSPECIFIED.),
    2.,
    UNSPECIFIED_VALUE(.UNSPECIFIED.),
    UNSPECIFIED_VALUE(.UNSPECIFIED.));
```

Figure 74 STEP File Fragment for Surface_Element_Property and Related Entities

The EXPRESS schema definitions for these entities and the supertypes are shown in Figure 75.

```
ENTITY Surface_Element_Property;
    property_id : Identifier;
    description  : Text;
    section     : Surface_Section_Field;
END_ENTITY;

ENTITY Surface_Section_Field
    SUPERTYPE OF (
        ONEOF (
            Surface_Section_Field_Constant,
            Surface_Section_Field_Varying ) );
END_ENTITY;

ENTITY Surface_Section_Field_Constant
    SUBTYPE OF ( Surface_Section_Field );
    definition : Surface_Section;
END_ENTITY;

ENTITY Surface_Section
    SUPERTYPE OF (
        ONEOF (
            Uniform_Surface_Section,
            Uniform_Surface_Section_Layered ) );
    offset           : Measure_Or_Unspecified_Value;
    non_structural_mass : Measure_Or_Unspecified_Value;
    non_structural_mass_offset : Measure_Or_Unspecified_Value;
END_ENTITY;

ENTITY Uniform_Surface_Section
    SUBTYPE OF ( Surface_Section );
    thickness        : Context_Dependent_Measure;
    bending_thickness : Measure_Or_Unspecified_Value;
    shear_thickness  : Measure_Or_Unspecified_Value;
END_ENTITY;
```

Figure 75 EXPRESS Schema for Surface_Element_Property and Related Entities

7.7 Material Definition

The material definition and discussion are identical to that in Section 5.7.

7.7.1 STEP Diagram

Identical to Section 5.7.1.

7.7.2 FE Model Input

Identical to Section 5.7.2.

7.7.3 STEP Entities

Identical to Section 5.7.3.

8 Pilot Model ATS4 – 3D Solid Element

The ATS4pilot model composition is illustrated in Figure 76.

- Solid model with 3 linear element types

- FE model composition

■ Elements:	32	CHEXA
	240	CTETRA
	96	CPENTA
■ Nodes:	255	GRID
■ Loads:	36	FORCE
	3	LOAD
■ Boundary:	30	SPC1
	2	SPCADD
■ Property:	1	PSOLID
■ Material:	1	MAT1 (aluminum)

- Subcase and output requests

■ Subcases:	3	SUBCASE
■ Boundary:	3	SPC
■ Loads:	3	LOAD
■ Output:	12	GPFORCE (global)
		DISPLACEMENT
		SPCFORCES
		STRESS

*See listing for output parameters

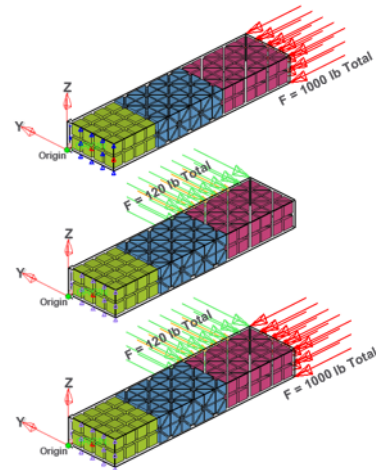


Figure 76 Pilot Model Content Summary ATS4

8.1 Product Definition Shape

The structure of the product definition entity graph is similar to the 2D shell element ATS3 pilot model; however, the instance identifiers and association counts shown in Figure 77 are different.

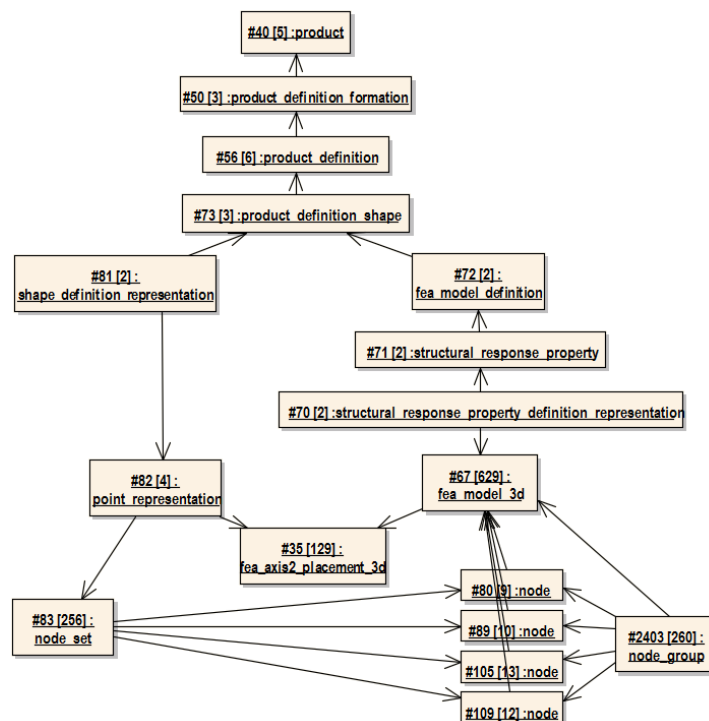


Figure 77 ATS4 FEM High Level Product Definition Shape Structure

8.2 FEA Model

The FEA model for the ATS4 pilot model is similar to the ATS3 pilot model. No local coordinate systems are present. All geometric founding is with respect to the basic coordinate system.

8.3 Coordinate System

No local coordinate systems are defined for the ATS4 model. Only the basic coordinate system is used.

8.3.1 STEP Diagram

No additional diagram is needed for coordinate systems.

8.3.2 FE Model Input

The NASTRAN basic coordinate system is an implied system; no user input is required.

8.3.3 STEP Entities

No entities beyond the fea_model_3d, point_representation and fea_axis2_placement_3d shown in Figure 77 are required to describe the basic coordinate system and the geometric founding of this model.

8.4 Node Definition

The ATS4 pilot study model uses 3-dimensional solid elements which require a 3-dimensional grid of node locations to define the discretized analysis space. The nodes are arranged in 3 layers at z=0, 1 and 2 inches. Each of these node layers is laid out as a 5 x 17 array of equally spaces nodes for a total of 255 nodes.

8.4.1 STEP Diagram

The details of the node definitions for ththe ATS4 model are similar to the prior 2D shell ATS3 model. Refer to Section 7.4.1 for details.

8.4.2 FE Model Input

Refer to Section 7.4.2 for input formats. The complete listing of the NASTRAN grid point inputs is included in the Appendix of this document.

8.4.3 STEP Entities

The instances for the first 5 node entities is shown in Figure 78.

```
#80= NODE('1', (#78), #36, #67);
#78= CARTESIAN_POINT('1', (0., -4., -3.4315200000000000E-8));
#89= NODE('2', (#87), #36, #67);
#87= CARTESIAN_POINT('2', (0., -3., -3.4315200000000000E-8));
#93= NODE('3', (#91), #36, #67);
#91= CARTESIAN_POINT('3', (0., -2., -3.4315200000000000E-8));
#97= NODE('4', (#95), #36, #67);
#95= CARTESIAN_POINT('4', (0., -1., -3.4315200000000000E-8));
#101= NODE('5', (#99), #36, #67);
#99= CARTESIAN_POINT('5', (0., -6.0137600000000000E-9, -3.4315200000000000E-8));

#83= NODE_SET('node_set_name_1', (#80, #89, #93, #97, #101, #105, #109, #113,
#117, #121, #125, #129, #133, #137, #141, #145, #149, #153, #157, #161, #165, #169,
...removed for clarity...
, #1013, #1017, #1021, #1025, #1029, #1033, #1037, #1041, #1045, #1049, #1053, #1057
, #1061, #1065, #1069, #1073, #1077, #1081, #1085, #1089, #1093, #1097, #1101));
```

Figure 78 STEP File Fragment for AT43 Nodes

8.5 Element Definition

The ATS4 pilot model introduces the solid volumetric element type to the study. These elements fully define the analysis domain of the element and require a 3-dimensional grid of node coordinates to specify the connectivity of the elements. The elements are 4-noded tetrahedron, 6-noded wedge and 8-noded hexahedron elements.

Special care must be given to proper mapping of the connectivity node list. The solver specification for connectivity (NASTRAN) may use a different node order than the STEP AP209 ed2 standard, depending on the mathematical order of the element (linear, quadratic, cubic, etc.). For this pilot study, linear elements were selected and the node order for the element vertices is consistent. However, this is an exception and not a rule. Figure 79 shows the node order definitions for a quadratic hexahedron element. Note the different mid-side node IDs and the lack of a centroid and face center nodes in the NASTRAN definitions. Refer to the Part 104 document for complete topology (edge and face) definitions for all supported elements shapes and orders. However, as stated earlier, the linear element uses the circled vertex nodes that are numbered similarly.

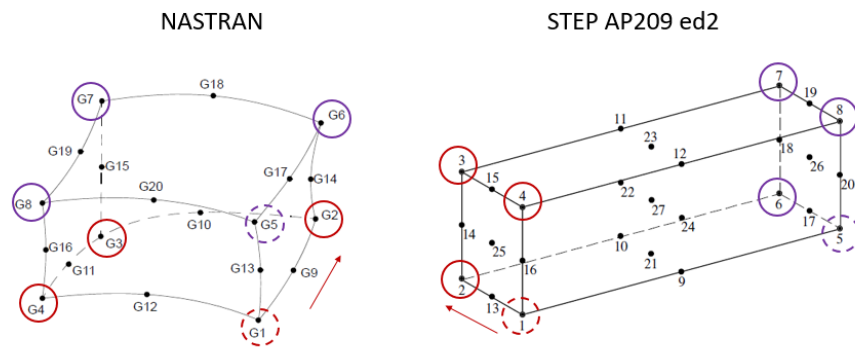


Figure 79 Node Order Mapping for Quadratic Hexahedron Element Shape

The solver format for volumetric elements also supports additional input that specifies the internal formulations of the element in the solver. These options are not included in this initial pilot study.

8.5.1 STEP Diagram

The STEP instance diagram illustrating the element connectivity and associated entities is shown in Figure 80. In the ATS4 model, very few entities besides the element instance are required to define the FEM element. The additional entities are discussed in the following sections.

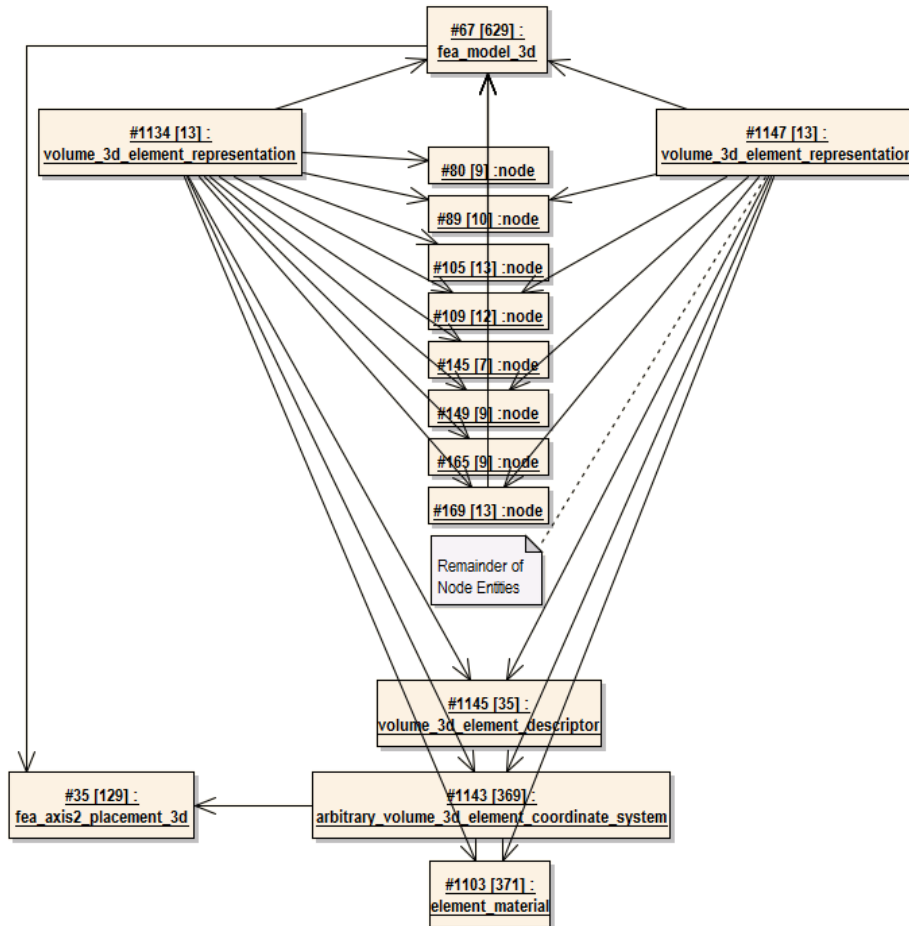


Figure 80 STEP Volume 3D Element Definition and Related Data Model Structures

All the nodes for the first volume_3d_element_representation are shown in the diagram. The second element shares 4 nodes that typically indicates adjacent solid elements that share a common face. Similar structures are found in the STEP data model for each volume_3d_element_descriptor instance. In other hybrid models (volume, surface and curve based elements in the same model), there will be combinations of all the structures discussed in all of the ATS models.

Additionally, the particular NASTRAN definition for the solid element property leads to the selection of the arbitrary_volume_3d_element_coordinate_system. This will be discussed in Section 8.6.

Lastly, the entire ATS4 model uses the same isotropic material definition discussed in Section 5.7.

8.5.2 FE Model Input

The solver format for specifying the linear hexahedron volumetric element in NASTRAN is shown in Figure 81.

	1	2	3	4	5	6	7	8	9	10
CHEXA	EID	PID	G1	G2	G3	G4	G5	G6		
	G7	G8	G9	G10	G11	G12	G13	G14		
	G15	G16	G17	G18	G19	G20				
CHEXA	1	1	1	2	7	6	16	17		
	22	21								
CHEXA	2	1	2	3	8	7	17	18		
	23	22								
CHEXA	3	1	3	4	9	8	18	19		
	24	23								

Figure 81 NASTRAN Card Image for Linear Hexahedron Elements

The formats for the tetraheadon and wedge solid elements are described in the NASTRAN reference manual.

8.5.3 STEP Entities

A brief listing of the Part 21 text is shown in Figure 82. Only hexahedron elements are listed but all the element descriptor are presented.

```
#1135=/* GEOMETRIC_REPRESENTATION_CONTEXT+PARAMETRIC_REPRESENTATION_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)PARAMETRIC_REPRESENTATION_CONTEXT()
REPRESENTATION_CONTEXT('REP_CONTEXT_FEA','3D'));

#1134= VOLUME_3D_ELEMENT_REPRESENTATION('1',(#1143),#1135, (#80,#89,#109,
#105,#145,#149,#169,#165),#67,#1145,#1103);
#1147= VOLUME_3D_ELEMENT_REPRESENTATION('2',(#1143),#1135, (#89,#93,#113,
#109,#149,#153,#173,#169),#67,#1145,#1103);
#1150= VOLUME_3D_ELEMENT_REPRESENTATION('3',(#1143),#1135, (#93,#97,#117,
#113,#153,#157,#177,#173),#67,#1145,#1103);

#1145= VOLUME_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER., 'LINEAR_HEXAHEDRON.CHEXA',
(ENUMERATED_VOLUME_ELEMENT_PURPOSE(.STRESS_DISPLACEMENT.)), .HEXAHEDRON.);
#1243= VOLUME_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER., 'LINEAR_TETRAHEDRON.CTETRA',
(ENUMERATED_VOLUME_ELEMENT_PURPOSE(.STRESS_DISPLACEMENT.)), .TETRAHEDRON.);
#1965= VOLUME_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER., 'LINEAR_WEDGE.CPENTA',
(ENUMERATED_VOLUME_ELEMENT_PURPOSE(.STRESS_DISPLACEMENT.)), .WEDGE.);
```

Figure 82 STEP File Fragment for Volume 3D Element Information

8.6 Property Definition

The property definition for a solid element is minimal; however its associations to an element material and a local element coordinate system are required.

8.6.1 STEP Diagram

The diagram in Figure 80 shows the relationship of volumetric elements to the element material and local element coordinate system.

8.6.2 FE Model Input

The NASTRAN PSOLID card shown in Figure 83 is used to associate both the element material and a coordinate system to the related element; it is shared between all element types in this instance.

1	2	3	4	5	6	7	8	9	10
PSOLID	PID	MID	CORDM	IN	STRESS	ISOP	FCTN	COROT	
PSOLID	1	1	0						

Figure 83 NASTRAN Volume Element Property Card

The specification in NASTRAN of the CORDM=0 is an explicit reference to a material coordinate system for the element. This maps to the `arbitrary_volume_3d_element_coordinate_system` entity shown in Figure 80 which in-turn refers to the basic coordinate system. The other options on the PSOLID card are not used in this pilot model.

8.6.3 STEP Entities

No additional STEP entities are associated with the volumetric property. Figure 80 in Section 8.5.1 fully defines the required AP209 ed2 instances.

8.7 Material Definition

The material definition and discussion is identical to that presented in Section 5.7.

8.7.1 STEP Diagram

Identical to Section 5.7.1.

8.7.2 FE Model Input

Identical to Section 5.7.2.

8.7.3 STEP Entities

Identical to Section 5.7.3.

9 References and Links

The following are a list of useful links which the reader can use to learn more about the STEP standard, the US and European organizations that administer, develop and support these standards, and the LOTAR Engineering and Simulation work group, which authored this handbook.

The reader is encouraged to visit all the links for an introduction and overview of the activities of these organizations. However, the LOTAR EAS WG link and the CAx-IF and CAE-IF links contain reference material that is directly applicable to the topics discussed in the handbook.

LOTAR International	http://www.lotar-international.org
LOTAR EAS WG	http://www.lotar-international.org/lotar-workgroups/engineering-analysis-simulation.html
NAFEMS	http://www.nafems.org
AFNeT	http://www.afnet.fr
PDES, Inc.	https://www.pdesinc.org
prostep ivip	http://www.prostep.org/en.html
AIA	http://www.aia-aerospace.org
ASD-STAN	http://www.asd-stan.org
ISO STEP AP209 ed2	http://www.ap209.org
CAx-IF	https://www.cax-if.org
CAE-IF	http://afnet.fr/dotank/sps/cae-if

Table 1 Useful Links for Further Reading on ISO 10303 (STEP)

10 Appendix A – NASTRAN Input File Full Listing

The NASTRAN input files for the 4 pilot models, as described in the following 4 subsections, were used for this pilot study. They are not expected to be changed or updated unless a significant issue is identified that materially affects the generation of the STEP files. The first load case is defined consistently for all models with appropriate loads and boundary conditions to enable comparable solution data. However, the results may not be numerically identical due to differences in the model abstractions and element selection.

10.1 ATS1m4.bdf

```
$ Linear Static Analysis
SOL 101
TIME 600
CEND
$
SEALL = ALL
SUPER = ALL
TITLE = Nastran job EAS test case ATS1m4
ECHO = NONE
MAXLINES = 999999999
GPFORCE(PUNCH) = ALL
$
SUBCASE 1
  SUBTITLE=subcase1
  SPC = 100
  LOAD = 200
  DISPLACEMENT(PUNCH, SORT1, REAL)=ALL
  SPCFORCES(PUNCH, SORT1, REAL)=ALL
  STRESS(PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
$
BEGIN BULK
PARAM   POST      -1
PARAM   AUTOSPC   YES
PARAM   NOCOMPS  -1
PARAM   PRTMAXIM  YES
$
PROD    1          1          8.          0.
$
CROD   1          1          1           2
CROD   2          1          2           3
CROD   3          1          3           4
CROD   4          1          4           5
CROD   5          1          5           6
CROD   6          1          6           7
CROD   7          1          7           8
CROD   8          1          8           9
CROD   9          1          9          10
CROD  10          1          10          11
CROD  11          1          11          12
CROD  12          1          12          13
CROD  13          1          13          14
CROD  14          1          14          15
CROD  15          1          15          16
CROD  16          1          16          17
$
MAT1   1          1.+7          .33          2.54-4  1.3-5  70.
$
GRID   1          1          0.          -2.          1.
GRID   2          1          1.          -2.          1.
GRID   3          1          2.          -2.          1.
GRID   4          1          3.          -2.          1.
GRID   5          1          4.          -2.          1.
GRID   6          1          5.          -2.          1.
GRID   7          1          6.          -2.          1.
GRID   8          1          7.          -2.          1.
GRID   9          1          8.          -2.          1.
GRID  10          1          9.          -2.          1.
```

GRID	11	1	10.	-2.	1.			
GRID	12	1	11.	-2.	1.			
GRID	13	1	12.	-2.	1.			
GRID	14	1	13.	-2.	1.			
GRID	15	1	14.	-2.	1.			
GRID	16	1	15.	-2.	1.			
GRID	17	1	16.	-2.	1.			
\$								
SPC1	100	123	1					
\$								
FORCE	200	17	0	1000.	-1.	0.	0.	
\$								
CORD2R	1		0.	0.	0.	0.	0.	1.
	1.	0.	0.					
\$								
ENDDATA								

10.2 ATS2m4.bdf

```

$ Linear Static Analysis
SOL 101
TIME 600
CEND
$
SEALL = ALL
SUPER = ALL
TITLE = Nastran EAS test case ATS2m4
ECHO = NONE
MAXLINES = 999999999
GPFORCE(PUNCH) = ALL
$
SUBCASE 1
  SUBTITLE=subcase1
  SPC = 100
  LOAD = 200
  DISPLACEMENT(PUNCH, SORT1, REAL)=ALL
  SPCFORCES(PUNCH, SORT1, REAL)=ALL
  STRESS(PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
SUBCASE 2
  SUBTITLE=subcase2
  SPC = 10
  LOAD = 22
  DISPLACEMENT(PUNCH, SORT1, REAL)=ALL
  SPCFORCES(PUNCH, SORT1, REAL)=ALL
  STRESS(PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
SUBCASE 3
  SUBTITLE=subcase3
  SPC = 10
  LOAD = 23
  DISPLACEMENT(PUNCH, SORT1, REAL)=ALL
  SPCFORCES(PUNCH, SORT1, REAL)=ALL
  STRESS(PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
$
BEGIN BULK
PARAM   POST      -1
PARAM   AUTOSPC   YES
PARAM   NOCOMPS  -1
PARAM   PRTMAXIM  YES
$
PBAR    1          1          8.          2.667   10.667   0.          0.
        1.          2.          1.          -2.          0.          0.          0.          0.
        0.
$
CBAR*   1          1          1          1          2
*       0.          7.54979-8  1.
CBAR*   2          1          2          3
*       0.          7.54979-8  1.
CBAR*   3          1          3          4
*       0.          7.54979-8  1.
CBAR*   4          1          4          5
*       0.          7.54979-8  1.
CBAR*   5          1          5          6
*       0.          7.54979-8  1.
CBAR*   6          1          6          7
*       0.          7.54979-8  1.
CBAR*   7          1          7          8
*       0.          7.54979-8  1.
CBAR*   8          1          8          9
*       0.          7.54979-8  1.
CBAR*   9          1          9          10
*      0.          7.54979-8  1.
CBAR*  10          1          10         11
*      0.          7.54979-8  1.
CBAR*  11          1          11         12
*      0.          7.54979-8  1.
CBAR*  12          1          12         13
*      0.          7.54979-8  1.
CBAR*  13          1          13         14

```


*	0.		7.54979-8	1.				
CBAR*	14		1	14			15	
*	0.		7.54979-8	1.				
CBAR*	15		1	15			16	
*	0.		7.54979-8	1.				
CBAR*	16		1	16			17	
*	0.		7.54979-8	1.				
\$								
MAT1	1	1.+7	.33	2.54-4	1.3-5	70.		
\$								
GRID	1	1	0.	-2.	1.			
GRID	2	1	1.	-2.	1.			
GRID	3	1	2.	-2.	1.			
GRID	4	1	3.	-2.	1.			
GRID	5	1	4.	-2.	1.			
GRID	6	1	5.	-2.	1.			
GRID	7	1	6.	-2.	1.			
GRID	8	1	7.	-2.	1.			
GRID	9	1	8.	-2.	1.			
GRID	10	1	9.	-2.	1.			
GRID	11	1	10.	-2.	1.			
GRID	12	1	11.	-2.	1.			
GRID	13	1	12.	-2.	1.			
GRID	14	1	13.	-2.	1.			
GRID	15	1	14.	-2.	1.			
GRID	16	1	15.	-2.	1.			
GRID	17	1	16.	-2.	1.			
\$								
SPCADD	10	100						
\$								
LOAD	22	1.	1.	300	1.	400		
LOAD	23	1.	1.	200	1.	300	1.	400
\$								
SPC1	100	123456	1					
\$								
FORCE	200	17	0	1000.	-1.	0.	0.	
FORCE	300	11	0	10.	0.	-1.	0.	
FORCE	300	17	0	10.	0.	-1.	0.	
FORCE	400	12	0	20.	0.	-1.	0.	
FORCE	400	13	0	20.	0.	-1.	0.	
FORCE	400	14	0	20.	0.	-1.	0.	
FORCE	400	15	0	20.	0.	-1.	0.	
FORCE	400	16	0	20.	0.	-1.	0.	
\$								
CORD2R	1		0.	0.	0.	0.	0.	1.
	1.	0.	0.					
\$								
ENDDATA								

10.3 ATS3m4.bdf

```

$ Linear Static Analysis
SOL 101
TIME 600
CEND
$
SEALL = ALL
SUPER = ALL
TITLE = Nastran job EAS test case ATS3m4
ECHO = NONE
MAXLINES = 999999999
GPFORCE(PUNCH) = ALL
$
SUBCASE 1
  SUBTITLE=subcase1
  SPC = 11
  LOAD = 21
  DISPLACEMENT (PUNCH, SORT1, REAL)=ALL
  SPCFORCES (PUNCH, SORT1, REAL)=ALL
  STRESS (PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
SUBCASE 2
  SUBTITLE=subcase2
  SPC = 12
  LOAD = 22
  DISPLACEMENT (PUNCH, SORT1, REAL)=ALL
  SPCFORCES (PUNCH, SORT1, REAL)=ALL
  STRESS (PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
SUBCASE 3
  SUBTITLE=subcase3
  SPC = 12
  LOAD = 23
  DISPLACEMENT (PUNCH, SORT1, REAL)=ALL
  SPCFORCES (PUNCH, SORT1, REAL)=ALL
  STRESS (PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
SUBCASE 4
  SUBTITLE=subcase4
  SPC = 103
  LOAD = 500
  DISPLACEMENT (PUNCH, SORT1, REAL)=ALL
  SPCFORCES (PUNCH, SORT1, REAL)=ALL
  STRESS (PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
$
BEGIN BULK
PARAM   POST      -1
PARAM   AUTOSPC   YES
PARAM   NOCOMPS   -1
PARAM   PRTMAXIM  YES
$
PSHELL  1         1         2.         1         1
$
CQUAD4  1         1         1         2         13         12
CQUAD4  2         1         2         3         14         13
CQUAD4  3         1         3         4         15         14
CQUAD4  4         1         4         5         16         15
CQUAD4  5         1         5         6         17         16
CQUAD4  6         1         6         7         18         17
CQUAD4  7         1         7         8         19         18
CQUAD4  8         1         8         9         20         19
CQUAD4  9         1         9         10        21         20
CQUAD4  10        1         10        11        22         21
CQUAD4  11        1         12        13        24         23
CQUAD4  12        1         13        14        25         24
CQUAD4  13        1         14        15        26         25
CQUAD4  14        1         15        16        27         26
CQUAD4  15        1         16        17        28         27
CQUAD4  16        1         17        18        29         28
CQUAD4  17        1         18        19        30         29
CQUAD4  18        1         19        20        31         30
CQUAD4  19        1         20        21        32         31
CQUAD4  20        1         21        22        33         32

```

CQUAD4	21	1	23	24	35	34
CQUAD4	22	1	24	25	36	35
CQUAD4	23	1	25	26	37	36
CQUAD4	24	1	26	27	38	37
CQUAD4	25	1	27	28	39	38
CQUAD4	26	1	28	29	40	39
CQUAD4	27	1	29	30	41	40
CQUAD4	28	1	30	31	42	41
CQUAD4	29	1	31	32	43	42
CQUAD4	30	1	32	33	44	43
CQUAD4	31	1	34	35	46	45
CQUAD4	32	1	35	36	47	46
CQUAD4	33	1	36	37	48	47
CQUAD4	34	1	37	38	49	48
CQUAD4	35	1	38	39	50	49
CQUAD4	36	1	39	40	51	50
CQUAD4	37	1	40	41	52	51
CQUAD4	38	1	41	42	53	52
CQUAD4	39	1	42	43	54	53
CQUAD4	40	1	43	44	55	54
CTRIA3	41	1	64	22	11	
CTRIA3	42	1	11	57	64	
CTRIA3	43	1	57	58	64	
CTRIA3	44	1	65	64	58	
CTRIA3	45	1	66	65	58	
CTRIA3	46	1	58	59	66	
CTRIA3	47	1	59	60	66	
CTRIA3	48	1	67	66	60	
CTRIA3	49	1	68	67	60	
CTRIA3	50	1	60	61	68	
CTRIA3	51	1	61	62	68	
CTRIA3	52	1	69	68	62	
CTRIA3	53	1	22	64	33	
CTRIA3	54	1	71	33	64	
CTRIA3	55	1	72	71	64	
CTRIA3	56	1	64	65	72	
CTRIA3	57	1	65	66	72	
CTRIA3	58	1	73	72	66	
CTRIA3	59	1	74	73	66	
CTRIA3	60	1	66	67	74	
CTRIA3	61	1	67	68	74	
CTRIA3	62	1	75	74	68	
CTRIA3	63	1	76	75	68	
CTRIA3	64	1	68	69	76	
CTRIA3	65	1	78	44	33	
CTRIA3	66	1	33	71	78	
CTRIA3	67	1	71	72	78	
CTRIA3	68	1	79	78	72	
CTRIA3	69	1	80	79	72	
CTRIA3	70	1	72	73	80	
CTRIA3	71	1	73	74	80	
CTRIA3	72	1	81	80	74	
CTRIA3	73	1	82	81	74	
CTRIA3	74	1	74	75	82	
CTRIA3	75	1	75	76	82	
CTRIA3	76	1	83	82	76	
CTRIA3	77	1	44	78	55	
CTRIA3	78	1	85	55	78	
CTRIA3	79	1	86	85	78	
CTRIA3	80	1	78	79	86	
CTRIA3	81	1	79	80	86	
CTRIA3	82	1	87	86	80	
CTRIA3	83	1	88	87	80	
CTRIA3	84	1	80	81	88	
CTRIA3	85	1	81	82	88	
CTRIA3	86	1	89	88	82	
CTRIA3	87	1	90	89	82	
CTRIA3	88	1	82	83	90	
\$						
MAT1	1	1.+7		.33	2.54-4	1.3-5 70.
\$						

GRID*	1			-6.24022-8	-4.
*	1.				
GRID	2	1.	-4.	1.	
GRID	3	2.	-4.	1.	
GRID	4	3.	-4.	1.	
GRID	5	4.	-4.	1.	
GRID	6	5.	-4.	1.	
GRID	7	6.	-4.	1.	
GRID	8	7.	-4.	1.	
GRID	9	8.	-4.	1.	
GRID	10	9.	-4.	1.	
GRID	11	10.	-4.	1.	
GRID*	12			-6.24022-8	-3.
*	1.				
GRID	13	1.	-3.	1.	
GRID	14	2.	-3.	1.	
GRID	15	3.	-3.	1.	
GRID	16	4.	-3.	1.	
GRID	17	5.	-3.	1.	
GRID	18	6.	-3.	1.	
GRID	19	7.	-3.	1.	
GRID	20	8.	-3.	1.	
GRID	21	9.	-3.	1.	
GRID	22	10.	-3.	1.	
GRID*	23			-6.24022-8	-2.
*	1.				
GRID	24	1.	-2.	1.	
GRID	25	2.	-2.	1.	
GRID	26	3.	-2.	1.	
GRID	27	4.	-2.	1.	
GRID	28	5.	-2.	1.	
GRID	29	6.	-2.	1.	
GRID	30	7.	-2.	1.	
GRID	31	8.	-2.	1.	
GRID	32	9.	-2.	1.	
GRID	33	10.	-2.	1.	
GRID*	34			-6.24022-8	-1.
*	1.				
GRID	35	1.	-1.	1.	
GRID	36	2.	-1.	1.	
GRID	37	3.	-1.	1.	
GRID	38	4.	-1.	1.	
GRID	39	5.	-1.	1.	
GRID	40	6.	-1.	1.	
GRID	41	7.	-1.	1.	
GRID	42	8.	-1.	1.	
GRID	43	9.	-1.	1.	
GRID	44	10.	-1.	1.	
GRID*	45			-6.24022-8	-5.27577-8
*	1.				
GRID*	46			1.	-5.27577-8
*	1.				
GRID*	47			2.	-5.27577-8
*	1.				
GRID*	48			3.	-5.27577-8
*	1.				
GRID*	49			4.	-5.27577-8
*	1.				
GRID*	50			5.	-5.27577-8
*	1.				
GRID*	51			6.	-5.27577-8
*	1.				
GRID*	52			7.	-5.27577-8
*	1.				
GRID*	53			8.	-5.27577-8
*	1.				
GRID*	54			9.	-5.27577-8
*	1.				
GRID*	55			10.	-5.27577-8
*	1.				
GRID	57	11.	-4.	1.	

GRID	58		12.	-4.	1.			
GRID	59		13.	-4.	1.			
GRID	60		14.	-4.	1.			
GRID	61		15.	-4.	1.			
GRID	62		16.	-4.	1.			
GRID	64		11.	-3.	1.			
GRID	65		12.	-3.	1.			
GRID	66		13.	-3.	1.			
GRID	67		14.	-3.	1.			
GRID	68		15.	-3.	1.			
GRID	69		16.	-3.	1.			
GRID	71		11.	-2.	1.			
GRID	72		12.	-2.	1.			
GRID	73		13.	-2.	1.			
GRID	74		14.	-2.	1.			
GRID	75		15.	-2.	1.			
GRID	76		16.	-2.	1.			
GRID	78		11.	-1.	1.			
GRID	79		12.	-1.	1.			
GRID	80		13.	-1.	1.			
GRID	81		14.	-1.	1.			
GRID	82		15.	-1.	1.			
GRID	83		16.	-1.	1.			
GRID*	85				11.			-5.27577-8
*	1.							
GRID*	86				12.			-5.27577-8
*	1.							
GRID*	87				13.			-5.27577-8
*	1.							
GRID*	88				14.			-5.27577-8
*	1.							
GRID*	89				15.			-5.27577-8
*	1.							
GRID*	90				16.			-5.27577-8
*	1.							
\$								
SPCADD	11	100	101	110				
SPCADD	12	100	102	110				
\$								
LOAD	21	1.	1.	200				
LOAD	22	1.	1.	300	1.	400		
LOAD	23	1.	1.	200	1.	300	1.	400
\$								
SPC1	100	123	23					
SPC1	101	1	1	12	34	45		
SPC1	102	123	1	12	34	45		
SPC1	103	123	23					
SPC1	103	23	76					
SPC1	103	3	1	12	34	45		
SPC1	103	3	62	69	83	90		
SPC1	110	45	1	THRU	55			
SPC1	110	45	57	58	59	60	61	62
	64	65	66	67	68	69	71	72
	73	74	75	76	78	79	80	81
	82	83	85	86	87	88	89	90
\$								
FORCE	200	62	0	125.	-1.	0.	0.	
FORCE	200	69	0	250.	-1.	0.	0.	
FORCE	200	76	0	250.	-1.	0.	0.	
FORCE	200	83	0	250.	-1.	0.	0.	
FORCE	200	90	0	125.	-1.	0.	0.	
FORCE	300	55	0	10.	0.	-1.	0.	
FORCE	300	90	0	10.	0.	-1.	0.	
FORCE	400	85	0	20.	0.	-1.	0.	
FORCE	400	86	0	20.	0.	-1.	0.	
FORCE	400	87	0	20.	0.	-1.	0.	
FORCE	400	88	0	20.	0.	-1.	0.	
FORCE	400	89	0	20.	0.	-1.	0.	
\$								
PLOAD2		500-125.0		8				
PLOAD2		500-125.0		9				

PLOAD2	500-125.0	18
PLOAD2	500-125.0	19
PLOAD2	500-125.0	28
PLOAD2	500-125.0	29
PLOAD2	500-125.0	38
PLOAD2	500-125.0	39
\$		
ENDDATA		

10.4 ATS4m4.bdf

```

$ Linear Static Analysis
SOL 101
TIME 600
CEND
$
SEALL = ALL
SUPER = ALL
TITLE = Nastran job EAS test case ATS4m4
ECHO = NONE
MAXLINES = 999999999
GPFORCE(PUNCH) = ALL
$
SUBCASE 1
  SUBTITLE=subcase1
  SPC = 11
  LOAD = 21
  DISPLACEMENT(PUNCH, SORT1, REAL)=ALL
  SPCFORCES(PUNCH, SORT1, REAL)=ALL
  STRESS(PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
SUBCASE 2
  SUBTITLE=subcase2
  SPC = 12
  LOAD = 22
  DISPLACEMENT(PUNCH, SORT1, REAL)=ALL
  SPCFORCES(PUNCH, SORT1, REAL)=ALL
  STRESS(PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
SUBCASE 3
  SUBTITLE=subcase3
  SPC = 12
  LOAD = 23
  DISPLACEMENT(PUNCH, SORT1, REAL)=ALL
  SPCFORCES(PUNCH, SORT1, REAL)=ALL
  STRESS(PUNCH, SORT1, REAL, VONMISES, BILIN)=ALL
$
BEGIN BULK
PARAM   POST      -1
PARAM   AUTOSPC   YES
PARAM   PRTMAXIM  YES
$
PSOLID  1          1          0
$
CHEXA   1          1          1          2          7          6          16         17
        22         21
CHEXA   2          1          2          3          8          7          17         18
        23         22
CHEXA   3          1          3          4          9          8          18         19
        24         23
CHEXA   4          1          4          5          10         9          19         20
        25         24
CHEXA   5          1          6          7          12         11         21         22
        27         26
CHEXA   6          1          7          8          13         12         22         23
        28         27
CHEXA   7          1          8          9          14         13         23         24
        29         28
CHEXA   8          1          9          10         15         14         24         25
        30         29
CHEXA   9          1          16         17         22         21         31         32
        37         36
CHEXA  10          1          17         18         23         22         32         33
        38         37
CHEXA  11          1          18         19         24         23         33         34
        39         38
CHEXA  12          1          19         20         25         24         34         35
        40         39
CHEXA  13          1          21         22         27         26         36         37
        42         41
CHEXA  14          1          22         23         28         27         37         38
        43         42

```

CHEXA	15	1	23	24	29	28	38	39
	44	43						
CHEXA	16	1	24	25	30	29	39	40
	45	44						
CHEXA	17	1	31	32	37	36	46	47
	52	51						
CHEXA	18	1	32	33	38	37	47	48
	53	52						
CHEXA	19	1	33	34	39	38	48	49
	54	53						
CHEXA	20	1	34	35	40	39	49	50
	55	54						
CHEXA	21	1	36	37	42	41	51	52
	57	56						
CHEXA	22	1	37	38	43	42	52	53
	58	57						
CHEXA	23	1	38	39	44	43	53	54
	59	58						
CHEXA	24	1	39	40	45	44	54	55
	60	59						
CHEXA	25	1	46	47	52	51	61	62
	67	66						
CHEXA	26	1	47	48	53	52	62	63
	68	67						
CHEXA	27	1	48	49	54	53	63	64
	69	68						
CHEXA	28	1	49	50	55	54	64	65
	70	69						
CHEXA	29	1	51	52	57	56	66	67
	72	71						
CHEXA	30	1	52	53	58	57	67	68
	73	72						
CHEXA	31	1	53	54	59	58	68	69
	74	73						
CHEXA	32	1	54	55	60	59	69	70
	75	74						
\$								
CTETRA	33	1	76	83	111	77		
CTETRA	34	1	118	111	83	119		
CTETRA	35	1	84	77	119	83		
CTETRA	36	1	112	119	77	111		
CTETRA	37	1	77	83	111	119		
CTETRA	38	1	84	119	77	85		
CTETRA	39	1	112	77	119	113		
CTETRA	40	1	78	113	85	77		
CTETRA	41	1	120	85	113	119		
CTETRA	42	1	77	85	119	113		
CTETRA	43	1	78	85	113	79		
CTETRA	44	1	120	113	85	121		
CTETRA	45	1	86	79	121	85		
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GRID	100	7.	-3.	0.	
GRID	101	6.	-3.	0.	
GRID	102	5.	-3.	0.	
GRID	104	10.	-4.	0.	
GRID	105	9.	-4.	0.	
GRID	106	8.	-4.	0.	
GRID	107	7.	-4.	0.	
GRID	108	6.	-4.	0.	
GRID	109	5.	-4.	0.	
GRID*	111			10.	-5.27577-8
*	1.				
GRID*	112			9.	-5.27577-8
*	1.				
GRID*	113			8.	-5.27577-8
*	1.				
GRID*	114			7.	-5.27577-8
*	1.				
GRID*	115			6.	-5.27577-8
*	1.				
GRID*	116			5.	-5.27577-8
*	1.				
GRID	118	10.	-1.	1.	
GRID	119	9.	-1.	1.	
GRID	120	8.	-1.	1.	
GRID	121	7.	-1.	1.	
GRID	122	6.	-1.	1.	
GRID	123	5.	-1.	1.	
GRID	125	10.	-2.	1.	
GRID	126	9.	-2.	1.	
GRID	127	8.	-2.	1.	
GRID	128	7.	-2.	1.	
GRID	129	6.	-2.	1.	
GRID	130	5.	-2.	1.	
GRID	132	10.	-3.	1.	
GRID	133	9.	-3.	1.	
GRID	134	8.	-3.	1.	
GRID	135	7.	-3.	1.	
GRID	136	6.	-3.	1.	
GRID	137	5.	-3.	1.	
GRID	139	10.	-4.	1.	
GRID	140	9.	-4.	1.	
GRID	141	8.	-4.	1.	
GRID	142	7.	-4.	1.	
GRID	143	6.	-4.	1.	
GRID	144	5.	-4.	1.	
GRID*	146			10.	-5.27577-8
*	2.				
GRID*	147			9.	-5.27577-8
*	2.				
GRID*	148			8.	-5.27577-8
*	2.				
GRID*	149			7.	-5.27577-8
*	2.				
GRID*	150			6.	-5.27577-8

*	2.				
GRID*	151			5.	-5.27577-8
*	2.				
GRID	153	10.	-1.	2.	
GRID	154	9.	-1.	2.	
GRID	155	8.	-1.	2.	
GRID	156	7.	-1.	2.	
GRID	157	6.	-1.	2.	
GRID	158	5.	-1.	2.	
GRID	160	10.	-2.	2.	
GRID	161	9.	-2.	2.	
GRID	162	8.	-2.	2.	
GRID	163	7.	-2.	2.	
GRID	164	6.	-2.	2.	
GRID	165	5.	-2.	2.	
GRID	167	10.	-3.	2.	
GRID	168	9.	-3.	2.	
GRID	169	8.	-3.	2.	
GRID	170	7.	-3.	2.	
GRID	171	6.	-3.	2.	
GRID	172	5.	-3.	2.	
GRID	174	10.	-4.	2.	
GRID	175	9.	-4.	2.	
GRID	176	8.	-4.	2.	
GRID	177	7.	-4.	2.	
GRID	178	6.	-4.	2.	
GRID	179	5.	-4.	2.	
GRID*	181			16.	-5.27577-8
*	0.				
GRID*	182			15.	-5.27577-8
*	0.				
GRID*	183			14.	-5.27577-8
*	0.				
GRID*	184			13.	-5.27577-8
*	0.				
GRID*	185			12.	-5.27577-8
*	0.				
GRID*	186			11.	-5.27577-8
*	0.				
GRID	188	16.	-1.	0.	
GRID	189	15.	-1.	0.	
GRID	190	14.	-1.	0.	
GRID	191	13.	-1.	0.	
GRID	192	12.	-1.	0.	
GRID	193	11.	-1.	0.	
GRID	195	16.	-2.	0.	
GRID	196	15.	-2.	0.	
GRID	197	14.	-2.	0.	
GRID	198	13.	-2.	0.	
GRID	199	12.	-2.	0.	
GRID	200	11.	-2.	0.	
GRID	202	16.	-3.	0.	
GRID	203	15.	-3.	0.	
GRID	204	14.	-3.	0.	
GRID	205	13.	-3.	0.	
GRID	206	12.	-3.	0.	
GRID	207	11.	-3.	0.	
GRID	209	16.	-4.	0.	
GRID	210	15.	-4.	0.	
GRID	211	14.	-4.	0.	
GRID	212	13.	-4.	0.	
GRID	213	12.	-4.	0.	
GRID	214	11.	-4.	0.	
GRID*	216			16.	-5.27577-8
*	1.				
GRID*	217			15.	-5.27577-8
*	1.				
GRID*	218			14.	-5.27577-8
*	1.				
GRID*	219			13.	-5.27577-8
*	1.				

GRID*	220			12.				-5.27577-8
*	1.							
GRID*	221			11.				-5.27577-8
*	1.							
GRID	223	16.	-1.	1.				
GRID	224	15.	-1.	1.				
GRID	225	14.	-1.	1.				
GRID	226	13.	-1.	1.				
GRID	227	12.	-1.	1.				
GRID	228	11.	-1.	1.				
GRID	230	16.	-2.	1.				
GRID	231	15.	-2.	1.				
GRID	232	14.	-2.	1.				
GRID	233	13.	-2.	1.				
GRID	234	12.	-2.	1.				
GRID	235	11.	-2.	1.				
GRID	237	16.	-3.	1.				
GRID	238	15.	-3.	1.				
GRID	239	14.	-3.	1.				
GRID	240	13.	-3.	1.				
GRID	241	12.	-3.	1.				
GRID	242	11.	-3.	1.				
GRID	244	16.	-4.	1.				
GRID	245	15.	-4.	1.				
GRID	246	14.	-4.	1.				
GRID	247	13.	-4.	1.				
GRID	248	12.	-4.	1.				
GRID	249	11.	-4.	1.				
GRID*	251			16.				-5.27577-8
*	2.							
GRID*	252			15.				-5.27577-8
*	2.							
GRID*	253			14.				-5.27577-8
*	2.							
GRID*	254			13.				-5.27577-8
*	2.							
GRID*	255			12.				-5.27577-8
*	2.							
GRID*	256			11.				-5.27577-8
*	2.							
GRID	258	16.	-1.	2.				
GRID	259	15.	-1.	2.				
GRID	260	14.	-1.	2.				
GRID	261	13.	-1.	2.				
GRID	262	12.	-1.	2.				
GRID	263	11.	-1.	2.				
GRID	265	16.	-2.	2.				
GRID	266	15.	-2.	2.				
GRID	267	14.	-2.	2.				
GRID	268	13.	-2.	2.				
GRID	269	12.	-2.	2.				
GRID	270	11.	-2.	2.				
GRID	272	16.	-3.	2.				
GRID	273	15.	-3.	2.				
GRID	274	14.	-3.	2.				
GRID	275	13.	-3.	2.				
GRID	276	12.	-3.	2.				
GRID	277	11.	-3.	2.				
GRID	279	16.	-4.	2.				
GRID	280	15.	-4.	2.				
GRID	281	14.	-4.	2.				
GRID	282	13.	-4.	2.				
GRID	283	12.	-4.	2.				
GRID	284	11.	-4.	2.				
\$								
SPCADD	11	100	101					
SPCADD	12	100	102					
\$								
LOAD	21	1.	1.	200				
LOAD	22	1.	1.	300	1.	400		
LOAD	23	1.	1.	200	1.	300	1.	400

\$							
SPC1	100	123	8				
SPC1	100	3	6				
SPC1	101	1	1	THRU	7		
SPC1	101	1	9	THRU	15		
SPC1	102	123	1	THRU	7		
SPC1	102	123	9	THRU	15		
\$							
FORCE	200	181	0	31.25	-1.	0.	0.
FORCE	200	209	0	31.25	-1.	0.	0.
FORCE	200	251	0	31.25	-1.	0.	0.
FORCE	200	279	0	31.25	-1.	0.	0.
FORCE	200	188	0	62.50	-1.	0.	0.
FORCE	200	195	0	62.50	-1.	0.	0.
FORCE	200	202	0	62.50	-1.	0.	0.
FORCE	200	216	0	62.50	-1.	0.	0.
FORCE	200	244	0	62.50	-1.	0.	0.
FORCE	200	258	0	62.50	-1.	0.	0.
FORCE	200	265	0	62.50	-1.	0.	0.
FORCE	200	272	0	62.50	-1.	0.	0.
FORCE	200	223	0	125.0	-1.	0.	0.
FORCE	200	230	0	125.0	-1.	0.	0.
FORCE	200	237	0	125.0	-1.	0.	0.
FORCE	300	76	01.0	0.0	-2.5	0.0	0.0
FORCE	300	146	01.0	0.0	-2.5	0.0	0.0
FORCE	300	181	01.0	0.0	-2.5	0.0	0.0
FORCE	300	251	01.0	0.0	-2.5	0.0	0.0
FORCE	300	111	01.0	0.0	-5.0	0.0	0.0
FORCE	300	186	01.0	0.0	-5.0	0.0	0.0
FORCE	300	183	01.0	0.0	-5.0	0.0	0.0
FORCE	300	184	01.0	0.0	-5.0	0.0	0.0
FORCE	300	185	01.0	0.0	-5.0	0.0	0.0
FORCE	300	182	01.0	0.0	-5.0	0.0	0.0
FORCE	300	216	01.0	0.0	-5.0	0.0	0.0
FORCE	300	252	01.0	0.0	-5.0	0.0	0.0
FORCE	300	253	01.0	0.0	-5.0	0.0	0.0
FORCE	300	254	01.0	0.0	-5.0	0.0	0.0
FORCE	300	255	01.0	0.0	-5.0	0.0	0.0
FORCE	300	256	01.0	0.0	-5.0	0.0	0.0
FORCE	400	217	01.0	0.0	-10.0	0.0	0.0
FORCE	400	218	01.0	0.0	-10.0	0.0	0.0
FORCE	400	219	01.0	0.0	-10.0	0.0	0.0
FORCE	400	220	01.0	0.0	-10.0	0.0	0.0
FORCE	400	221	01.0	0.0	-10.0	0.0	0.0
\$							
ENDDATA							

11 Appendix B – STEP Part21 Output File Full Listing

The following pages list the full STEP Part21 file contents for the 4 pilot models. This section will be updated as the STEP converters mature and required corrections are incorporated into this document. As such, the actual instance identifiers in these files may not match the ones used in the figures and tables within the body of this document.

11.1 ATS1m4.stp

```
ISO-10303-21;
HEADER;

/*****
* Creation date:          Tue Feb 07 13:53:28 2017
* Schema:                AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF
*****/

FILE_DESCRIPTION(('','2;1');
FILE_NAME(
'O:\projects\Crystal\software_FEM\converters\examples\db\e.DataRepository.Fem_Model'
,
'2017-02-07T13:53:28',
('ANONYMOUS USER'),
('ANONYMOUS ORGANISATION'),
'EDMsix Version 2.0100.a14 Jan 31 2017',
'',
'');
FILE_SCHEMA(('AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF'));
ENDSEC;

DATA;
#1= APPLICATION_CONTEXT(
'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF');
#3= ID_ATTRIBUTE('to be decided',#1);
#4= DESCRIPTION_ATTRIBUTE('to be decided',#1);
#5= APPLICATION_PROTOCOL_DEFINITION('international standard',
'ap209_multidisciplinary_analysis_and_design',2011,#1);
#6= DIMENSIONAL_EXPONENTS(0.,0.,0.,0.,0.,0.,0.);
#7= /* LENGTH_UNIT+SI_UNIT */(LENGTH_UNIT()NAMED_UNIT(*)SI_UNIT($,
.METRE.));
#8= /* MASS_UNIT+SI_UNIT */(MASS_UNIT()NAMED_UNIT(*)SI_UNIT(.KILO.,
.GRAM.));
#9= /* SI_UNIT+TIME_UNIT */(NAMED_UNIT(*)SI_UNIT($,.SECOND.)TIME_UNIT()
);
#10= /* SI_UNIT+THERMODYNAMIC_TEMPERATURE_UNIT */(NAMED_UNIT(*)SI_UNIT($,
.DEGREE_CELSIUS.)THERMODYNAMIC_TEMPERATURE_UNIT());
#11= /* PLANE_ANGLE_UNIT+SI_UNIT */(NAMED_UNIT(*)PLANE_ANGLE_UNIT()
SI_UNIT($,.RADIAN.));
#12= SI_FORCE_UNIT((#13,#14,#15),*,$,.NEWTON.);
#13= DERIVED_UNIT_ELEMENT(#8,1.);
#14= DERIVED_UNIT_ELEMENT(#7,1.);
#15= DERIVED_UNIT_ELEMENT(#9,-2.);
#17= SI_FREQUENCY_UNIT((#18),*,$,.HERTZ.);
#18= DERIVED_UNIT_ELEMENT(#9,-1.);
#20= SI_PRESSURE_UNIT((#13,#21,#15),*,$,.PASCAL.);
#21= DERIVED_UNIT_ELEMENT(#7,-1.);
#23= SI_ENERGY_UNIT((#13,#24,#15),*,$,.JOULE.);
#24= DERIVED_UNIT_ELEMENT(#7,2.);
#26= SI_POWER_UNIT((#13,#24,#27),*,$,.WATT.);
#27= DERIVED_UNIT_ELEMENT(#9,-3.);
#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,.CARTESIAN.,
'FEA_BASIC_COORD_SYSTEM.0');
#36= /* GEOMETRIC REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT(
'FEA_BASIC_COORD_SYSTEM.0','3d'));
#39= DIRECTION('RefX',(1.,0.,0.));
#41= DIRECTION('AxisZ',(0.,0.,1.));
#43= CARTESIAN_POINT('',(0.,0.,0.));
#45= FEA_AXIS2_PLACEMENT_3D('1',#43,#41,#39,.CARTESIAN.,'CORD2R.1');
#46= /* GEOMETRIC REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT('CORD2R.1','3d'
));
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#49= ORGANIZATION($,'default-organization',$);
#50= PRODUCT('default-id.0','default-fea-part','',(#52));
#52= PRODUCT_CONTEXT('design_context',#1,'design_context');
#54= PRODUCT_RELATED_PRODUCT_CATEGORY('part',$,(#50));
#55= ID_ATTRIBUTE('',#54);
#57= APPLIED_IDENTIFICATION_ASSIGNMENT('default-id.0',#58,(#60,#66,#50)
);
#58= IDENTIFICATION_ROLE('default-role',$);
#59= PRODUCT_RELATED_PRODUCT_CATEGORY('product',$,(#50));
#60= PRODUCT_DEFINITION_FORMATION('default-id.0','',#50);
#61= GROUP('id',$);
#62= APPLIED_CLASSIFICATION_ASSIGNMENT(#61,#64,(#57));
#64= CLASSIFICATION_ROLE('',#64);
#66= PRODUCT_DEFINITION('default-id.0',$,#60,#67);
#67= PRODUCT_DEFINITION_CONTEXT('assembly definition',#1,
'life cycle stage');
#68= APPLIED_CLASSIFICATION_ASSIGNMENT(#69,#70,(#66));
#69= GROUP('default-gpvt-type',$);
#70= CLASSIFICATION_ROLE('view_type',$);
#73= ORGANIZATION_ROLE('id context');
#74= APPLIED_ORGANIZATION_ASSIGNMENT(#49,#73,(#57));
#76= NAME_ATTRIBUTE('',#66);
#77= FEA_MODEL_3D('Identification',(35),#36,
'NASTRAN BDF Converter v0.0.0','(NASTRAN)','AnalysisModelType');
#80= STRUCTURAL_RESPONSE_PROPERTY_DEFINITION_REPRESENTATION(#81,#77);
#81= STRUCTURAL_RESPONSE_PROPERTY('structural_response_property_id_1',$,
#82);
#82= FEA_MODEL_DEFINITION('fea_model_definition_id_1',$,#83,.U.);
#83= PRODUCT_DEFINITION_SHAPE('name',$,#66);
#84= CARTESIAN_POINT('0',(0.,0.,0.));
#86= DUMMY_NODE('0',(84),#36,#77);
#88= CARTESIAN_POINT('1',(0.,-2.,1.));
#90= NODE('1',(88),#46,#77);
#91= SHAPE_DEFINITION_REPRESENTATION(#83,#92);
#92= POINT_REPRESENTATION('point_representation_name_1',(93,#45),#46);
#93= NODE_SET('node_set_name_1',(90,#99,#103,#107,#111,#115,#119,#123,
#127,#131,#135,#139,#143,#147,#151,#155,#159));
#97= CARTESIAN_POINT('2',(1.,-2.,1.));
#99= NODE('2',(97),#46,#77);
#101= CARTESIAN_POINT('3',(2.,-2.,1.));
#103= NODE('3',(101),#46,#77);
#105= CARTESIAN_POINT('4',(3.,-2.,1.));
#107= NODE('4',(105),#46,#77);
#109= CARTESIAN_POINT('5',(4.,-2.,1.));
#111= NODE('5',(109),#46,#77);
#113= CARTESIAN_POINT('6',(5.,-2.,1.));
#115= NODE('6',(113),#46,#77);
#117= CARTESIAN_POINT('7',(6.,-2.,1.));
#119= NODE('7',(117),#46,#77);
#121= CARTESIAN_POINT('8',(7.,-2.,1.));
#123= NODE('8',(121),#46,#77);
#125= CARTESIAN_POINT('9',(8.,-2.,1.));
#127= NODE('9',(125),#46,#77);
#129= CARTESIAN_POINT('10',(9.,-2.,1.));
#131= NODE('10',(129),#46,#77);
#133= CARTESIAN_POINT('11',(10.,-2.,1.));
#135= NODE('11',(133),#46,#77);
#137= CARTESIAN_POINT('12',(11.,-2.,1.));
#139= NODE('12',(137),#46,#77);
#141= CARTESIAN_POINT('13',(12.,-2.,1.));
#143= NODE('13',(141),#46,#77);
#145= CARTESIAN_POINT('14',(13.,-2.,1.));
#147= NODE('14',(145),#46,#77);
#149= CARTESIAN_POINT('15',(14.,-2.,1.));
#151= NODE('15',(149),#46,#77);
#153= CARTESIAN_POINT('16',(15.,-2.,1.));
#155= NODE('16',(153),#46,#77);
#157= CARTESIAN_POINT('17',(16.,-2.,1.));
#159= NODE('17',(157),#46,#77);
#161= ITEM_DEFINED_TRANSFORMATION('',',',#35,#45);
#162= REPRESENTATION_RELATIONSHIP_WITH_TRANSFORMATION('',',',#77,#92,#161

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);
#163= ELEMENT_MATERIAL('MAT1.1','Fea Material',(#175,#183,#189));
#164= MEASURE_REPRESENTATION_ITEM('representation_item_name_1',
THERMODYNAMIC_TEMPERATURE_MEASURE(70.),#10);
#165= PROPERTY_DEFINITION_REPRESENTATION(#166,#168);
#166= PROPERTY_DEFINITION('Material Property Definition',$,#167);
#167= CHARACTERIZED_OBJECT('property',$);
#168= REPRESENTATION('representation_id_1',(#164),#36);
#169= ID_ATTRIBUTE('MAT1.1',#166);
#171= DATA_ENVIRONMENT('DATA_ENV','Property_conditions',(#165));
#173= FEA_LINEAR_ELASTICITY('',FEA_ISOTROPIC_SYMMETRIC_TENSOR4_3D((
10000000.,0.33)));
#175= FEA_MATERIAL_PROPERTY_REPRESENTATION(#176,#178,#171);
#176= MATERIAL_PROPERTY('MAT1.1.0',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#178= REPRESENTATION('representation_id_2',(#173),#36);
#179= DESCRIPTION_ATTRIBUTE('Elasticity',#175);
#182= FEA_MASS_DENSITY('',0.000254);
#183= FEA_MATERIAL_PROPERTY_REPRESENTATION(#184,#185,#171);
#184= MATERIAL_PROPERTY('MAT1.1.1',$,#177);
#185= REPRESENTATION('representation_id_3',(#182),#36);
#186= DESCRIPTION_ATTRIBUTE('MassDensity',#183);
#188= FEA_TANGENTIAL_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION('',
ISOTROPIC_SYMMETRIC_TENSOR2_3D(0.));
#189= FEA_MATERIAL_PROPERTY_REPRESENTATION(#190,#191,#171);
#190= MATERIAL_PROPERTY('MAT1.1.2',$,#177);
#191= REPRESENTATION('representation_id_4',(#188),#36);
#192= DESCRIPTION_ATTRIBUTE('TangentCTE',#189);
#194= CURVE_3D_ELEMENT_PROPERTY('PROD.1','',(#195),(#213,#216),(#218,
#222));
#195= CURVE_ELEMENT_INTERVAL_CONSTANT(#198,#196,#206);
#196= EULER_ANGLES((0.,0.,0.));
#198= CURVE_ELEMENT_LOCATION(#199);
#199= FEA_PARAMETRIC_POINT('',(1.,0.,0.));
#201= REPRESENTATION('dpr0',(#199),#202);
#202= PARAMETRIC_REPRESENTATION_CONTEXT('FEA parametric context',
'Parametric');
#206= CURVE_ELEMENT_SECTION_DERIVED_DEFINITIONS('',0.,8.,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),(0.,0.,0.),
0.,CONTEXT_DEPENDENT_MEASURE(0.),(CONTEXT_DEPENDENT_MEASURE(0.)),
CONTEXT_DEPENDENT_MEASURE(0.),(CONTEXT_DEPENDENT_MEASURE(0.)),
CONTEXT_DEPENDENT_MEASURE(0.),(CONTEXT_DEPENDENT_MEASURE(0.)),
CONTEXT_DEPENDENT_MEASURE(0.)),CONTEXT_DEPENDENT_MEASURE(0.));
#213= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#216= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#218= CURVE_ELEMENT_END_RELEASE(#35,#219);
#219= CURVE_ELEMENT_END_RELEASE_PACKET(ENUMERATED_CURVE_ELEMENT_FREEDOM(
.NONE.),0.);
#222= CURVE_ELEMENT_END_RELEASE(#35,#219);
#224= CURVE_3D_ELEMENT_REPRESENTATION('1',(#233,#199),#225,(#90,#99),#77,
#238,#194,#163);
#225=
/* GEOMETRIC_REPRESENTATION_CONTEXT+PARAMETRIC_REPRESENTATION_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)PARAMETRIC_REPRESENTATION_CONTEXT()
REPRESENTATION_CONTEXT('REP_CONTEXT_FEA','3D'));
#227= REPRESENTATION('Default SimDM Fea representation',(#229),#225);
#229= REPRESENTATION_ITEM('Default SimDM item');
#230= ID_ATTRIBUTE('Default SimDM Fea representation',#227);
#231= DESCRIPTION_ATTRIBUTE('Default SimDM Fea representation',#227);
#233= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#236);
#234= DIRECTION('undefined',(1.,0.,0.));
#236= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#234);
#238= CURVE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER.,'LINEAR_CURVE.CROD',((
ENUMERATED_CURVE_ELEMENT_PURPOSE(.AXIAL.)),(
ENUMERATED_CURVE_ELEMENT_PURPOSE(.TORSION.))));
#242= CURVE_3D_ELEMENT_REPRESENTATION('2',(#233,#199),#225,(#99,#103),
#77,#238,#194,#163);
#245= CURVE_3D_ELEMENT_REPRESENTATION('3',(#233,#199),#225,(#103,#107),
#77,#238,#194,#163);
#248= CURVE_3D_ELEMENT_REPRESENTATION('4',(#233,#199),#225,(#107,#111),

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#77,#238,#194,#163);
#251= CURVE_3D_ELEMENT_REPRESENTATION('5',(#233,#199),#225,(#111,#115),
#77,#238,#194,#163);
#254= CURVE_3D_ELEMENT_REPRESENTATION('6',(#233,#199),#225,(#115,#119),
#77,#238,#194,#163);
#257= CURVE_3D_ELEMENT_REPRESENTATION('7',(#233,#199),#225,(#119,#123),
#77,#238,#194,#163);
#260= CURVE_3D_ELEMENT_REPRESENTATION('8',(#233,#199),#225,(#123,#127),
#77,#238,#194,#163);
#263= CURVE_3D_ELEMENT_REPRESENTATION('9',(#233,#199),#225,(#127,#131),
#77,#238,#194,#163);
#266= CURVE_3D_ELEMENT_REPRESENTATION('10',(#233,#199),#225,(#131,#135),
#77,#238,#194,#163);
#269= CURVE_3D_ELEMENT_REPRESENTATION('11',(#233,#199),#225,(#135,#139),
#77,#238,#194,#163);
#272= CURVE_3D_ELEMENT_REPRESENTATION('12',(#233,#199),#225,(#139,#143),
#77,#238,#194,#163);
#275= CURVE_3D_ELEMENT_REPRESENTATION('13',(#233,#199),#225,(#143,#147),
#77,#238,#194,#163);
#278= CURVE_3D_ELEMENT_REPRESENTATION('14',(#233,#199),#225,(#147,#151),
#77,#238,#194,#163);
#281= CURVE_3D_ELEMENT_REPRESENTATION('15',(#233,#199),#225,(#151,#155),
#77,#238,#194,#163);
#284= CURVE_3D_ELEMENT_REPRESENTATION('16',(#233,#199),#225,(#155,#159),
#77,#238,#194,#163);
#287= CONTROL(#77,'Control.0','FemConvert',
'Nastran job EAS test case ATS1m4',('<SOL>101</SOL>','TIME 600','CEND',
'<GLOBALCASE>0</GLOBALCASE>','<SUBCASE>1</SUBCASE>','ENDDATA'),(
'NASTRAN'));
#290= SPECIFIED_STATE('STEP DEFAULT','default_initial_state');
#291= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#287,'STATIC STEP 1',1,#290,'
,#313);
#292= SPECIFIED_STATE('Step 1 Base Specified State',
'Relating Specified State');
#293= SPECIFIED_STATE('SPCCASE_100_200_1','Aggregator SPC 100 Step 1');
#294= SPECIFIED_STATE('SPCVALSTATE_100_200','');
#295= STATE_RELATIONSHIP(
'SPCVALSTATE_100_200 is related to SPCCASE_100_200_1','',#293,#294);
#296= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#294,#299,#297,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#297= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#299= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.0',(#291),#90,#35,(#301,
#304,#305),'');
#301= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.X_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#304= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Y_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#305= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Z_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#306= STATE_RELATIONSHIP(
'SPCCASE_100_200_1 is related to Step 1 Base Specified State','',#292,
#293);
#307= SPECIFIED_STATE('LOADSTATECORE_200','Core Loads Specified State');
#308= NODAL_FREEDOM_ACTION_DEFINITION(#307,#159,#35,#309,(
CONTEXT_DEPENDENT_MEASURE(-1000.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#309= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#312= STATE_RELATIONSHIP(
'LOADSTATECORE_200 is related to Step 1 Base Specified State','',#292,
#307);
#313= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 1','',
#292);
#314= OUTPUT_REQUEST_STATE('Step 1 Output Request State','',(#291));
#316= NODAL_FREEDOM_VALUES(#314,#320,#35,#317,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(

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.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.));
#317= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(
.Y_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(.Z_ROTATION.)));
#320= NODE_GROUP('', 'ALL', #77, (#90, #99, #103, #107, #111, #115, #119, #123,
#127, #131, #135, #139, #143, #147, #151, #155, #159));
#321= ID_ATTRIBUTE('ALL', #320);
#323= NODAL_FREEDOM_ACTION_DEFINITION(#307, #159, #35, #309, (
CONTEXT_DEPENDENT_MEASURE(-1000.), CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)), .APPLIED_LOADS.);
ENDSEC;

END-ISO-10303-21;
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11.2 ATS2m4.stp

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ISO-10303-21;
HEADER;

/*****
* Creation date:          Tue Feb 07 13:53:29 2017
* Schema:                AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF
*****/

FILE_DESCRIPTION(('','2;1');
FILE_NAME(
'O:\projects\Crystal\software_FEM\converters\examples\db\e.DataRepository.Fem_Model'
,
'2017-02-07T13:53:29',
('ANONYMOUS USER'),
('ANONYMOUS ORGANISATION'),
'EDMsix Version 2.0100.a14 Jan 31 2017',
'',
'');
FILE_SCHEMA(('AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF'));
ENDSEC;

DATA;
#1= APPLICATION_CONTEXT(
'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF');
#3= ID_ATTRIBUTE('to be decided',#1);
#4= DESCRIPTION_ATTRIBUTE('to be decided',#1);
#5= APPLICATION_PROTOCOL_DEFINITION('international standard',
'ap209_multidisciplinary_analysis_and_design',2011,#1);
#6= DIMENSIONAL_EXPONENTS(0.,0.,0.,0.,0.,0.,0.);
#7= /* LENGTH_UNIT+SI_UNIT */(LENGTH_UNIT()NAMED_UNIT(*)SI_UNIT($,
.METRE.));
#8= /* MASS_UNIT+SI_UNIT */(MASS_UNIT()NAMED_UNIT(*)SI_UNIT(.KILO.,
.GRAM.));
#9= /* SI_UNIT+TIME_UNIT */(NAMED_UNIT(*)SI_UNIT($,.SECOND.)TIME_UNIT(
));
#10= /* SI_UNIT+THERMODYNAMIC_TEMPERATURE_UNIT */(NAMED_UNIT(*)SI_UNIT($,
.DEGREE_CELSIUS.)THERMODYNAMIC_TEMPERATURE_UNIT());
#11= /* PLANE_ANGLE_UNIT+SI_UNIT */(NAMED_UNIT(*)PLANE_ANGLE_UNIT(
SI_UNIT($,.RADIAN.));
#12= SI_FORCE_UNIT((#13,#14,#15),*,$,.NEWTON.);
#13= DERIVED_UNIT_ELEMENT(#8,1.);
#14= DERIVED_UNIT_ELEMENT(#7,1.);
#15= DERIVED_UNIT_ELEMENT(#9,-2.);
#17= SI_FREQUENCY_UNIT((#18),*,$,.HERTZ.);
#18= DERIVED_UNIT_ELEMENT(#9,-1.);
#20= SI_PRESSURE_UNIT((#13,#21,#15),*,$,.PASCAL.);
#21= DERIVED_UNIT_ELEMENT(#7,-1.);
#23= SI_ENERGY_UNIT((#13,#24,#15),*,$,.JOULE.);
#24= DERIVED_UNIT_ELEMENT(#7,2.);
#26= SI_POWER_UNIT((#13,#24,#27),*,$,.WATT.);
#27= DERIVED_UNIT_ELEMENT(#9,-3.);
#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,.CARTESIAN.,
'FEA_BASIC_COORD_SYSTEM.0');
#36= /* GEOMETRIC REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT(
'FEA_BASIC_COORD_SYSTEM.0','3d'));
#39= DIRECTION('RefX',(1.,0.,0.));
#41= DIRECTION('AxisZ',(0.,0.,1.));
#43= CARTESIAN_POINT('',(0.,0.,0.));
#45= FEA_AXIS2_PLACEMENT_3D('1',#43,#41,#39,.CARTESIAN.,'CORD2R.1');
#46= /* GEOMETRIC REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT('CORD2R.1','3d'
));

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#49= ORGANIZATION($,'default-organization',$);
#50= PRODUCT('default-id.0','default-fea-part','',(#52));
#52= PRODUCT_CONTEXT('design_context',#1,'design_context');
#54= PRODUCT_RELATED_PRODUCT_CATEGORY('part',$,(#50));
#55= ID_ATTRIBUTE('',#54);
#57= APPLIED_IDENTIFICATION_ASSIGNMENT('default-id.0',#58,(#60,#66,#50)
);
#58= IDENTIFICATION_ROLE('default-role',$);
#59= PRODUCT_RELATED_PRODUCT_CATEGORY('product',$,(#50));
#60= PRODUCT_DEFINITION_FORMATION('default-id.0','',#50);
#61= GROUP('id',$);
#62= APPLIED_CLASSIFICATION_ASSIGNMENT(#61,#64,(#57));
#64= CLASSIFICATION_ROLE('',#64);
#66= PRODUCT_DEFINITION('default-id.0',$,#60,#67);
#67= PRODUCT_DEFINITION_CONTEXT('assembly definition',#1,
'life cycle stage');
#68= APPLIED_CLASSIFICATION_ASSIGNMENT(#69,#70,(#66));
#69= GROUP('default-gpvt-type',$);
#70= CLASSIFICATION_ROLE('view_type',$);
#73= ORGANIZATION_ROLE('id context');
#74= APPLIED_ORGANIZATION_ASSIGNMENT(#49,#73,(#57));
#76= NAME_ATTRIBUTE('',#66);
#77= FEA_MODEL_3D('Identification',(#35),#36,
'NASTRAN BDF Converter v0.0.0',('NASTRAN'),'AnalysisModelType');
#80= STRUCTURAL_RESPONSE_PROPERTY_DEFINITION_REPRESENTATION(#81,#77);
#81= STRUCTURAL_RESPONSE_PROPERTY('structural_response_property_id_1',$,
#82);
#82= FEA_MODEL_DEFINITION('fea_model_definition_id_1',$,#83,.U.);
#83= PRODUCT_DEFINITION_SHAPE('name',$,#66);
#84= CARTESIAN_POINT('0',(0.,0.,0.));
#86= DUMMY_NODE('0',(#84),#36,#77);
#88= CARTESIAN_POINT('1',(0.,-2.,1.));
#90= NODE('1',(#88),#46,#77);
#91= SHAPE_DEFINITION_REPRESENTATION(#83,#92);
#92= POINT_REPRESENTATION('point_representation_name_1',(#93,#45),#46);
#93= NODE_SET('node_set_name_1',(#90,#99,#103,#107,#111,#115,#119,#123,
#127,#131,#135,#139,#143,#147,#151,#155,#159));
#97= CARTESIAN_POINT('2',(1.,-2.,1.));
#99= NODE('2',(#97),#46,#77);
#101= CARTESIAN_POINT('3',(2.,-2.,1.));
#103= NODE('3',(#101),#46,#77);
#105= CARTESIAN_POINT('4',(3.,-2.,1.));
#107= NODE('4',(#105),#46,#77);
#109= CARTESIAN_POINT('5',(4.,-2.,1.));
#111= NODE('5',(#109),#46,#77);
#113= CARTESIAN_POINT('6',(5.,-2.,1.));
#115= NODE('6',(#113),#46,#77);
#117= CARTESIAN_POINT('7',(6.,-2.,1.));
#119= NODE('7',(#117),#46,#77);
#121= CARTESIAN_POINT('8',(7.,-2.,1.));
#123= NODE('8',(#121),#46,#77);
#125= CARTESIAN_POINT('9',(8.,-2.,1.));
#127= NODE('9',(#125),#46,#77);
#129= CARTESIAN_POINT('10',(9.,-2.,1.));
#131= NODE('10',(#129),#46,#77);
#133= CARTESIAN_POINT('11',(10.,-2.,1.));
#135= NODE('11',(#133),#46,#77);
#137= CARTESIAN_POINT('12',(11.,-2.,1.));
#139= NODE('12',(#137),#46,#77);
#141= CARTESIAN_POINT('13',(12.,-2.,1.));
#143= NODE('13',(#141),#46,#77);
#145= CARTESIAN_POINT('14',(13.,-2.,1.));
#147= NODE('14',(#145),#46,#77);
#149= CARTESIAN_POINT('15',(14.,-2.,1.));
#151= NODE('15',(#149),#46,#77);
#153= CARTESIAN_POINT('16',(15.,-2.,1.));
#155= NODE('16',(#153),#46,#77);
#157= CARTESIAN_POINT('17',(16.,-2.,1.));
#159= NODE('17',(#157),#46,#77);
#161= ITEM_DEFINED_TRANSFORMATION('',',',#35,#45);
#162= REPRESENTATION_RELATIONSHIP_WITH_TRANSFORMATION('',',',#77,#92,#161

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);
#163= ELEMENT_MATERIAL('MAT1.1','Fea Material',(#175,#183,#189));
#164= MEASURE_REPRESENTATION_ITEM('representation_item_name_1',
THERMODYNAMIC_TEMPERATURE_MEASURE(70.),#10);
#165= PROPERTY_DEFINITION_REPRESENTATION(#166,#168);
#166= PROPERTY_DEFINITION('Material Property Definition',$,#167);
#167= CHARACTERIZED_OBJECT('property',$);
#168= REPRESENTATION('representation_id_1',(#164),#36);
#169= ID_ATTRIBUTE('MAT1.1',#166);
#171= DATA_ENVIRONMENT('DATA ENV','Property_conditions',(#165));
#173= FEA_LINEAR_ELASTICITY('',FEA_ISOTROPIC_SYMMETRIC_TENSOR4_3D((
10000000.,0.33)));
#175= FEA_MATERIAL_PROPERTY_REPRESENTATION(#176,#178,#171);
#176= MATERIAL_PROPERTY('MAT1.1.0',$,#177);
#177= CHARACTERIZED_OBJECT('material_property',$);
#178= REPRESENTATION('representation_id_2',(#173),#36);
#179= DESCRIPTION_ATTRIBUTE('Elasticity',#175);
#182= FEA_MASS_DENSITY('',0.000254);
#183= FEA_MATERIAL_PROPERTY_REPRESENTATION(#184,#185,#171);
#184= MATERIAL_PROPERTY('MAT1.1.1',$,#177);
#185= REPRESENTATION('representation_id_3',(#182),#36);
#186= DESCRIPTION_ATTRIBUTE('MassDensity',#183);
#188= FEA_TANGENTIAL_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION('',
ISOTROPIC_SYMMETRIC_TENSOR2_3D(0.));
#189= FEA_MATERIAL_PROPERTY_REPRESENTATION(#190,#191,#171);
#190= MATERIAL_PROPERTY('MAT1.1.2',$,#177);
#191= REPRESENTATION('representation_id_4',(#188),#36);
#192= DESCRIPTION_ATTRIBUTE('TangentCTE',#189);
#194= CURVE_3D_ELEMENT_REPRESENTATION('1',(#203,#213),#195, (#90,#99),#77
,#238,#208,#163);
#195=
/* GEOMETRIC REPRESENTATION CONTEXT+PARAMETRIC REPRESENTATION CONTEXT */
(GEOMETRIC REPRESENTATION CONTEXT(3)PARAMETRIC REPRESENTATION CONTEXT()
REPRESENTATION CONTEXT('REP_CONTEXT_FEA','3D'));
#197= REPRESENTATION('Default SimDM Fea representation',(#199),#195);
#199= REPRESENTATION_ITEM('Default SimDM item');
#200= ID_ATTRIBUTE('Default SimDM Fea representation',#197);
#201= DESCRIPTION_ATTRIBUTE('Default SimDM Fea representation',#197);
#203= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#204);
#204= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#205);
#205= DIRECTION('dxy',(0.,7.549790000000000000E-8,1.));
#208= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.1','',(#209),(#227,#230),(#232,
#236));
#209= CURVE_ELEMENT_INTERVAL_CONSTANT(#212,#210,#220);
#210= EULER_ANGLES((0.,0.,0.));
#212= CURVE_ELEMENT_LOCATION(#213);
#213= FEA_PARAMETRIC_POINT('',(1.,0.,0.));
#215= REPRESENTATION('dpr0',(#213),#216);
#216= PARAMETRIC_REPRESENTATION_CONTEXT('FEA parametric context',
'Parametric');
#220= CURVE_ELEMENT_SECTION_DERIVED_DEFINITIONS('PBAR.1_0',0.,8.,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),(2.667,
10.667,0.),0.,CONTEXT_DEPENDENT_MEASURE(0.),(CONTEXT_DEPENDENT_MEASURE(
0.),CONTEXT_DEPENDENT_MEASURE(0.)),(CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),(CONTEXT_DEPENDENT_MEASURE(0.)),
CONTEXT_DEPENDENT_MEASURE(0.)),CONTEXT_DEPENDENT_MEASURE(0.));
#227= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#230= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#232= CURVE_ELEMENT_END_RELEASE(#35, (#233));
#233= CURVE_ELEMENT_END_RELEASE_PACKET(ENUMERATED_CURVE_ELEMENT_FREEDOM(
.NONE.),0.);
#236= CURVE_ELEMENT_END_RELEASE(#35, (#233));
#238= CURVE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER.,'LINEAR_CURVE.CBAR*',((
ENUMERATED_CURVE_ELEMENT_PURPOSE(.AXIAL.)),(
ENUMERATED_CURVE_ELEMENT_PURPOSE(.Y_Y_BENDING.)),
ENUMERATED_CURVE_ELEMENT_PURPOSE(.Z_Z_BENDING.)),(
ENUMERATED_CURVE_ELEMENT_PURPOSE(.TORSION.)),(
ENUMERATED_CURVE_ELEMENT_PURPOSE(.X_Y_SHEAR.)),
ENUMERATED_CURVE_ELEMENT_PURPOSE(.X_Z_SHEAR.)));
#244= CURVE_3D_ELEMENT_REPRESENTATION('2',(#246,#213),#195, (#99,#103),

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#77,#238,#251,#163);
#246= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#247);
#247= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#248);
#248= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#251= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.2','',(#252),(#257,#260),(#262,
#265));
#252= CURVE_ELEMENT_INTERVAL_CONSTANT(#255,#253,#220);
#253= EULER_ANGLES((0.,0.,0.));
#255= CURVE_ELEMENT_LOCATION(#213);
#257= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#260= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#262= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#265= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#267= CURVE_3D_ELEMENT_REPRESENTATION('3',(#269,#213),#195,(#103,#107),
#77,#238,#274,#163);
#269= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#270);
#270= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#271);
#271= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#274= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.3','',(#275),(#280,#283),(#285,
#288));
#275= CURVE_ELEMENT_INTERVAL_CONSTANT(#278,#276,#220);
#276= EULER_ANGLES((0.,0.,0.));
#278= CURVE_ELEMENT_LOCATION(#213);
#280= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#283= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#285= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#288= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#290= CURVE_3D_ELEMENT_REPRESENTATION('4',(#292,#213),#195,(#107,#111),
#77,#238,#297,#163);
#292= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#293);
#293= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#294);
#294= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#297= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.4','',(#298),(#303,#306),(#308,
#311));
#298= CURVE_ELEMENT_INTERVAL_CONSTANT(#301,#299,#220);
#299= EULER_ANGLES((0.,0.,0.));
#301= CURVE_ELEMENT_LOCATION(#213);
#303= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#306= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#308= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#311= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#313= CURVE_3D_ELEMENT_REPRESENTATION('5',(#315,#213),#195,(#111,#115),
#77,#238,#320,#163);
#315= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#316);
#316= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#317);
#317= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#320= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.5','',(#321),(#326,#329),(#331,
#334));
#321= CURVE_ELEMENT_INTERVAL_CONSTANT(#324,#322,#220);
#322= EULER_ANGLES((0.,0.,0.));
#324= CURVE_ELEMENT_LOCATION(#213);
#326= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#329= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#331= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#334= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#336= CURVE_3D_ELEMENT_REPRESENTATION('6',(#338,#213),#195,(#115,#119),
#77,#238,#343,#163);
#338= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#339);
#339= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#340);
#340= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#343= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.6','',(#344),(#349,#352),(#354,
#357));
#344= CURVE_ELEMENT_INTERVAL_CONSTANT(#347,#345,#220);
#345= EULER_ANGLES((0.,0.,0.));
#347= CURVE_ELEMENT_LOCATION(#213);
#349= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#352= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#354= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#357= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#359= CURVE_3D_ELEMENT_REPRESENTATION('7',(#361,#213),#195,(#119,#123),
#77,#238,#366,#163);

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#361= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#362);
#362= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#363);
#363= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#366= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.7','',(#367),(#372,#375),(#377,
#380));
#367= CURVE_ELEMENT_INTERVAL_CONSTANT(#370,#368,#220);
#368= EULER_ANGLES((0.,0.,0.));
#370= CURVE_ELEMENT_LOCATION(#213);
#372= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#375= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#377= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#380= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#382= CURVE_3D_ELEMENT_REPRESENTATION('8',(#384,#213),#195,(#123,#127),
#77,#238,#389,#163);
#384= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#385);
#385= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#386);
#386= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#389= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.8','',(#390),(#395,#398),(#400,
#403));
#390= CURVE_ELEMENT_INTERVAL_CONSTANT(#393,#391,#220);
#391= EULER_ANGLES((0.,0.,0.));
#393= CURVE_ELEMENT_LOCATION(#213);
#395= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#398= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#400= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#403= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#405= CURVE_3D_ELEMENT_REPRESENTATION('9',(#407,#213),#195,(#127,#131),
#77,#238,#412,#163);
#407= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#408);
#408= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#409);
#409= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#412= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.9','',(#413),(#418,#421),(#423,
#426));
#413= CURVE_ELEMENT_INTERVAL_CONSTANT(#416,#414,#220);
#414= EULER_ANGLES((0.,0.,0.));
#416= CURVE_ELEMENT_LOCATION(#213);
#418= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#421= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#423= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#426= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#428= CURVE_3D_ELEMENT_REPRESENTATION('10',(#430,#213),#195,(#131,#135),
#77,#238,#435,#163);
#430= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#431);
#431= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#432);
#432= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#435= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.10','',(#436),(#441,#444),(#446,
#449));
#436= CURVE_ELEMENT_INTERVAL_CONSTANT(#439,#437,#220);
#437= EULER_ANGLES((0.,0.,0.));
#439= CURVE_ELEMENT_LOCATION(#213);
#441= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#444= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#446= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#449= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#451= CURVE_3D_ELEMENT_REPRESENTATION('11',(#453,#213),#195,(#135,#139),
#77,#238,#458,#163);
#453= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#454);
#454= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#455);
#455= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#458= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.11','',(#459),(#464,#467),(#469,
#472));
#459= CURVE_ELEMENT_INTERVAL_CONSTANT(#462,#460,#220);
#460= EULER_ANGLES((0.,0.,0.));
#462= CURVE_ELEMENT_LOCATION(#213);
#464= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#467= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#469= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#472= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#474= CURVE_3D_ELEMENT_REPRESENTATION('12',(#476,#213),#195,(#139,#143),
#77,#238,#481,#163);
#476= PARAMETRIC CURVE 3D ELEMENT COORDINATE SYSTEM('',#477);

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#477= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#478);
#478= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#481= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.12','',(#482),(#487,#490),(#492,
#495));
#482= CURVE_ELEMENT_INTERVAL_CONSTANT(#485,#483,#220);
#483= EULER_ANGLES((0.,0.,0.));
#485= CURVE_ELEMENT_LOCATION(#213);
#487= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#490= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#492= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#495= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#497= CURVE_3D_ELEMENT_REPRESENTATION('13',(#499,#213),#195,(#143,#147),
#77,#238,#504,#163);
#499= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#500);
#500= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#501);
#501= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#504= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.13','',(#505),(#510,#513),(#515,
#518));
#505= CURVE_ELEMENT_INTERVAL_CONSTANT(#508,#506,#220);
#506= EULER_ANGLES((0.,0.,0.));
#508= CURVE_ELEMENT_LOCATION(#213);
#510= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#513= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#515= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#518= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#520= CURVE_3D_ELEMENT_REPRESENTATION('14',(#522,#213),#195,(#147,#151),
#77,#238,#527,#163);
#522= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#523);
#523= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#524);
#524= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#527= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.14','',(#528),(#533,#536),(#538,
#541));
#528= CURVE_ELEMENT_INTERVAL_CONSTANT(#531,#529,#220);
#529= EULER_ANGLES((0.,0.,0.));
#531= CURVE_ELEMENT_LOCATION(#213);
#533= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#536= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#538= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#541= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#543= CURVE_3D_ELEMENT_REPRESENTATION('15',(#545,#213),#195,(#151,#155),
#77,#238,#550,#163);
#545= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#546);
#546= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#547);
#547= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#550= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.15','',(#551),(#556,#559),(#561,
#564));
#551= CURVE_ELEMENT_INTERVAL_CONSTANT(#554,#552,#220);
#552= EULER_ANGLES((0.,0.,0.));
#554= CURVE_ELEMENT_LOCATION(#213);
#556= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#559= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#561= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#564= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#566= CURVE_3D_ELEMENT_REPRESENTATION('16',(#568,#213),#195,(#155,#159),
#77,#238,#573,#163);
#568= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_SYSTEM('',#569);
#569= PARAMETRIC_CURVE_3D_ELEMENT_COORDINATE_DIRECTION('',#570);
#570= DIRECTION('dxy',(0.,7.549790000000000E-8,1.));
#573= CURVE_3D_ELEMENT_PROPERTY('PBAR.1.16','',(#574),(#579,#582),(#584,
#587));
#574= CURVE_ELEMENT_INTERVAL_CONSTANT(#577,#575,#220);
#575= EULER_ANGLES((0.,0.,0.));
#577= CURVE_ELEMENT_LOCATION(#213);
#579= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#582= CURVE_ELEMENT_END_OFFSET(#35,(0.,0.,0.));
#584= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#587= CURVE_ELEMENT_END_RELEASE(#35,(#233));
#589= CONTROL(#77,'Control.0','FemConvert',
'Nastran EAS test case ATS2m4',('<SOL>101</SOL>','TIME 600','CEND',
'<GLOBALCASE>0</GLOBALCASE>','<SUBCASE>1</SUBCASE>',
'<SUBCASE>2</SUBCASE>', '<SUBCASE>3</SUBCASE>', 'ENDDATA'), ('NASTRAN'));

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#592= SPECIFIED_STATE('STEP DEFAULT','default_initial_state');
#593= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#589,'STATIC STEP 1',1,#592,'
,#618);
#594= SPECIFIED_STATE('Step 1 Base Specified State',
'Relating Specified State');
#595= SPECIFIED_STATE('SPCCASE_100_200_1','Aggregator SPC 100 Step 1');
#596= SPECIFIED_STATE('SPCVALSTATE_100_200','');
#597= STATE_RELATIONSHIP(
'SPCVALSTATE_100_200 is related to SPCCASE_100_200_1','',#595,#596);
#598= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#596,#601,#599,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#599= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(
.Y_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(.Z_ROTATION.));
#601= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.0',(#593),#90,#35,(#603,
#606,#607,#608,#609,#610),'');
#603= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.X_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#606= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Y_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#607= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Z_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#608= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.)
,CONTEXT_DEPENDENT_MEASURE(1.));
#609= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(.Y_ROTATION.)
,CONTEXT_DEPENDENT_MEASURE(1.));
#610= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(.Z_ROTATION.)
,CONTEXT_DEPENDENT_MEASURE(1.));
#611= STATE_RELATIONSHIP(
'SPCCASE_100_200_1 is related to Step 1 Base Specified State','',#594,
#595);
#612= SPECIFIED_STATE('LOADSTATECORE_200','Core Loads Specified State');
#613= NODAL_FREEDOM_ACTION_DEFINITION(#612,#159,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(-1000.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#614= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.));
#617= STATE_RELATIONSHIP(
'LOADSTATECORE_200 is related to Step 1 Base Specified State','',#594,
#612);
#618= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 1','
,#594);
#619= OUTPUT_REQUEST_STATE('Step 1 Output Request State','',(#593));
#621= NODAL_FREEDOM_VALUES(#619,#625,#35,#622,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.)),UNSPECIFIED_VALUE(.UNSPECIFIED.));
#622= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(
.Y_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(.Z_ROTATION.));
#625= NODE_GROUP('','ALL',#77,(#90,#99,#103,#107,#111,#115,#119,#123,
#127,#131,#135,#139,#143,#147,#151,#155,#159));
#626= ID_ATTRIBUTE('ALL',#625);
#628= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#589,'STATIC STEP 2',2,#592,'
,#670);
#629= SPECIFIED_STATE('Step 2 Base Specified State',
'Relating Specified State');
#630= SPECIFIED_STATE('SPCCASE_10_22_2','Aggregator SPC 10 Step 2');
#631= SPECIFIED_STATE('SPCVALSTATE_100_22','');
#632= STATE_RELATIONSHIP(
'SPCVALSTATE_100_22 is related to SPCCASE_10_22_2','',#630,#631);
#633= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#631,#634,#599,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)),

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CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#634= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.1',(#628),#90,#35,(#603,
#606,#607,#608,#609,#610),'');
#638= STATE_RELATIONSHIP(
'SPCCASE_10_22_2 is related to Step 2 Base Specified State','',#629,#630
);
#639= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_22',
'Overall Factor Combined State');
#641= STATE_COMPONENT('OverallComp','',#639,1.);
#643= SPECIFIED_STATE('LOADSTATECORE_300','Core Loads Specified State');
#644= NODAL_FREEDOM_ACTION_DEFINITION(#643,#135,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#646= NODAL_FREEDOM_ACTION_DEFINITION(#643,#159,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#648= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_300',
'Item Factor State');
#649= STATE_RELATIONSHIP('LOADSTATEITEM_300 is related to OverallComp',
'',#641,#648);
#650= STATE_COMPONENT('ItemComp_22_300','',#648,1.);
#652= STATE_RELATIONSHIP(
'LOADSTATECORE_300 is related to ItemComp_22_300','',#650,#643);
#653= SPECIFIED_STATE('LOADSTATECORE_400','Core Loads Specified State');
#654= NODAL_FREEDOM_ACTION_DEFINITION(#653,#139,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#656= NODAL_FREEDOM_ACTION_DEFINITION(#653,#143,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#658= NODAL_FREEDOM_ACTION_DEFINITION(#653,#147,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#660= NODAL_FREEDOM_ACTION_DEFINITION(#653,#151,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#662= NODAL_FREEDOM_ACTION_DEFINITION(#653,#155,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#664= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_400',
'Item Factor State');
#665= STATE_RELATIONSHIP('LOADSTATEITEM_400 is related to OverallComp',
'',#641,#664);
#666= STATE_COMPONENT('ItemComp_22_400','',#664,1.);
#668= STATE_RELATIONSHIP(
'LOADSTATECORE_400 is related to ItemComp_22_400','',#666,#653);
#669= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_22 is related to Step 2 Base Specified State','',
#629,#639);
#670= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 2','',
#629);
#671= OUTPUT_REQUEST_STATE('Step 2 Output Request State','',(#628));
#673= NODAL_FREEDOM_VALUES(#671,#625,#35,#622,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.)));
#675= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#589,'STATIC STEP 3',3,#592,'',
#701);
#676= SPECIFIED_STATE('Step 3 Base Specified State',
'Relating Specified State');
#677= SPECIFIED_STATE('SPCCASE_10_23_3','Aggregator SPC 10 Step 3');
#678= SPECIFIED_STATE('SPCVALSTATE_100_23','');
#679= STATE_RELATIONSHIP(
'SPCVALSTATE_100_23 is related to SPCCASE_10_23_3','',#677,#678);
#680= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#678,#681,#599,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#681= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.2',(#675),#90,#35,(#603,
#606,#607,#608,#609,#610),'');
#685= STATE_RELATIONSHIP(

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'SPPCASE_10_23_3 is related to Step 3 Base Specified State','',#676,#677
);
#686= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_23',
'Overall Factor Combined State');
#687= STATE_COMPONENT('OverallComp','',#686,1.);
#689= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_200',
'Item Factor State');
#690= STATE_RELATIONSHIP('LOADSTATEITEM_200 is related to OverallComp',
'',#687,#689);
#691= STATE_COMPONENT('ItemComp_23_200','',#689,1.);
#693= STATE_RELATIONSHIP(
'LOADSTATECORE_200 is related to ItemComp_23_200','',#691,#612);
#694= STATE_RELATIONSHIP('LOADSTATEITEM_300 is related to OverallComp',
'',#687,#648);
#695= STATE_COMPONENT('ItemComp_23_300','',#648,1.);
#696= STATE_RELATIONSHIP(
'LOADSTATECORE_300 is related to ItemComp_23_300','',#695,#643);
#697= STATE_RELATIONSHIP('LOADSTATEITEM_400 is related to OverallComp',
'',#687,#664);
#698= STATE_COMPONENT('ItemComp_23_400','',#664,1.);
#699= STATE_RELATIONSHIP(
'LOADSTATECORE_400 is related to ItemComp_23_400','',#698,#653);
#700= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_23 is related to Step 3 Base Specified State','',
#676,#686);
#701= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 3','',
#676);
#702= OUTPUT_REQUEST_STATE('Step 3 Output Request State','',(#675));
#704= NODAL_FREEDOM_VALUES(#702,#625,#35,#622,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.)));
#706= NODAL_FREEDOM_ACTION_DEFINITION(#612,#159,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(-1000.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#708= NODAL_FREEDOM_ACTION_DEFINITION(#643,#135,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#710= NODAL_FREEDOM_ACTION_DEFINITION(#643,#159,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#712= NODAL_FREEDOM_ACTION_DEFINITION(#653,#139,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#714= NODAL_FREEDOM_ACTION_DEFINITION(#653,#143,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#716= NODAL_FREEDOM_ACTION_DEFINITION(#653,#147,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#718= NODAL_FREEDOM_ACTION_DEFINITION(#653,#151,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#720= NODAL_FREEDOM_ACTION_DEFINITION(#653,#155,#35,#614,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
ENDSEC;

END-ISO-10303-21;

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11.3 ATS3m4.stp

```
ISO-10303-21;
HEADER;

/*****
* Creation date:           Tue Feb 07 13:53:31 2017
* Schema:                 AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF
*****/

FILE_DESCRIPTION(('','2;1');
FILE_NAME(
'O:\projects\Crystal\software_FEM\converters\examples\db\le.DataRepository.Fem_Model'
,
'2017-02-07T13:53:31',
('ANONYMOUS USER'),
('ANONYMOUS ORGANISATION'),
'EDMsix Version 2.0100.a14 Jan 31 2017',
'',
'');
FILE_SCHEMA(('AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF'));
ENDSEC;

DATA;
#1= APPLICATION_CONTEXT(
'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF');
#3= ID_ATTRIBUTE('to be decided',#1);
#4= DESCRIPTION_ATTRIBUTE('to be decided',#1);
#5= APPLICATION_PROTOCOL_DEFINITION('international standard',
'ap209_multidisciplinary_analysis_and_design',2011,#1);
#6= DIMENSIONAL_EXPONENTS(0.,0.,0.,0.,0.,0.,0.);
#7= /* LENGTH_UNIT+SI_UNIT */(LENGTH_UNIT()NAMED_UNIT(*)SI_UNIT($,
.METRE.));
#8= /* MASS_UNIT+SI_UNIT */(MASS_UNIT()NAMED_UNIT(*)SI_UNIT(.KILO.,
.GRAM.));
#9= /* SI_UNIT+TIME_UNIT */(NAMED_UNIT(*)SI_UNIT($,.SECOND.)TIME_UNIT()
);
#10= /* SI_UNIT+THERMODYNAMIC_TEMPERATURE_UNIT */(NAMED_UNIT(*)SI_UNIT($
,.DEGREE_CELSIUS.)THERMODYNAMIC_TEMPERATURE_UNIT());
#11= /* PLANE_ANGLE_UNIT+SI_UNIT */(NAMED_UNIT(*)PLANE_ANGLE_UNIT()
SI_UNIT($,.RADIAN.));
#12= SI_FORCE_UNIT((#13,#14,#15),*,$,.NEWTON.);
#13= DERIVED_UNIT_ELEMENT(#8,1.);
#14= DERIVED_UNIT_ELEMENT(#7,1.);
#15= DERIVED_UNIT_ELEMENT(#9,-2.);
#17= SI_FREQUENCY_UNIT((#18),*,$,.HERTZ.);
#18= DERIVED_UNIT_ELEMENT(#9,-1.);
#20= SI_PRESSURE_UNIT((#13,#21,#15),*,$,.PASCAL.);
#21= DERIVED_UNIT_ELEMENT(#7,-1.);
#23= SI_ENERGY_UNIT((#13,#24,#15),*,$,.JOULE.);
#24= DERIVED_UNIT_ELEMENT(#7,2.);
#26= SI_POWER_UNIT((#13,#24,#27),*,$,.WATT.);
#27= DERIVED_UNIT_ELEMENT(#9,-3.);
#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,.CARTESIAN.,
'FEA_BASIC_COORD_SYSTEM.0');
#36= /* GEOMETRIC REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT(
'FEA_BASIC_COORD_SYSTEM.0','3d'));
#39= ORGANIZATION($,'default-organization',$);
#40= PRODUCT('default-id.0','default-fea-part','',(#42));
#42= PRODUCT_CONTEXT('design_context',#1,'design_context');
#44= PRODUCT_RELATED_PRODUCT_CATEGORY('part',$,(#40));
#45= ID_ATTRIBUTE('',#44);
#47= APPLIED_IDENTIFICATION_ASSIGNMENT('default-id.0',#48,(#50,#56,#40)
);
#48= IDENTIFICATION_ROLE('default-role',$);
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#49= PRODUCT_RELATED_PRODUCT_CATEGORY('product',$, (#40));
#50= PRODUCT_DEFINITION_FORMATION('default-id.0',',', #40);
#51= GROUP('id', $);
#52= APPLIED_CLASSIFICATION_ASSIGNMENT(#51, #54, (#47));
#54= CLASSIFICATION_ROLE('', $);
#56= PRODUCT_DEFINITION('default-id.0', $, #50, #57);
#57= PRODUCT_DEFINITION_CONTEXT('assembly definition', #1,
'life cycle stage');
#58= APPLIED_CLASSIFICATION_ASSIGNMENT(#59, #60, (#56));
#59= GROUP('default-gpvt-type', $);
#60= CLASSIFICATION_ROLE('view_type', $);
#63= ORGANIZATION_ROLE('id context');
#64= APPLIED_ORGANIZATION_ASSIGNMENT(#39, #63, (#47));
#66= NAME_ATTRIBUTE('', #56);
#67= FEA_MODEL_3D('Identification', (#35), #36,
'NASTRAN BDF Converter v0.0.0', ('NASTRAN'), 'AnalysisModelType');
#70= STRUCTURAL_RESPONSE_PROPERTY_DEFINITION_REPRESENTATION(#71, #67);
#71= STRUCTURAL_RESPONSE_PROPERTY('structural_response_property_id_1', $,
#72);
#72= FEA_MODEL_DEFINITION('fea_model_definition_id_1', $, #73, .U.);
#73= PRODUCT_DEFINITION_SHAPE('name', $, #56);
#74= CARTESIAN_POINT('0', (0., 0., 0.));
#76= DUMMY_NODE('0', (#74), #36, #67);
#78= CARTESIAN_POINT('1', (-6.2402200000000000E-8, -4., 1.));
#80= NODE('1', (#78), #36, #67);
#81= SHAPE_DEFINITION_REPRESENTATION(#73, #82);
#82= POINT_REPRESENTATION('point_representation_name_1', (#83, #35), #36);
#83= NODE_SET('node_set_name_1', (#80, #89, #93, #97, #101, #105, #109, #113,
#117, #121, #125, #129, #133, #137, #141, #145, #149, #153, #157, #161, #165, #169,
#173, #177, #181, #185, #189, #193, #197, #201, #205, #209, #213, #217, #221, #225,
#229, #233, #237, #241, #245, #249, #253, #257, #261, #265, #269, #273, #277, #281,
#285, #289, #293, #297, #301, #305, #309, #313, #317, #321, #325, #329, #333, #337,
#341, #345, #349, #353, #357, #361, #365, #369, #373, #377, #381, #385, #389, #393,
#397, #401, #405, #409, #413, #417, #421));
#87= CARTESIAN_POINT('2', (1., -4., 1.));
#89= NODE('2', (#87), #36, #67);
#91= CARTESIAN_POINT('3', (2., -4., 1.));
#93= NODE('3', (#91), #36, #67);
#95= CARTESIAN_POINT('4', (3., -4., 1.));
#97= NODE('4', (#95), #36, #67);
#99= CARTESIAN_POINT('5', (4., -4., 1.));
#101= NODE('5', (#99), #36, #67);
#103= CARTESIAN_POINT('6', (5., -4., 1.));
#105= NODE('6', (#103), #36, #67);
#107= CARTESIAN_POINT('7', (6., -4., 1.));
#109= NODE('7', (#107), #36, #67);
#111= CARTESIAN_POINT('8', (7., -4., 1.));
#113= NODE('8', (#111), #36, #67);
#115= CARTESIAN_POINT('9', (8., -4., 1.));
#117= NODE('9', (#115), #36, #67);
#119= CARTESIAN_POINT('10', (9., -4., 1.));
#121= NODE('10', (#119), #36, #67);
#123= CARTESIAN_POINT('11', (10., -4., 1.));
#125= NODE('11', (#123), #36, #67);
#127= CARTESIAN_POINT('12', (-6.2402200000000000E-8, -3., 1.));
#129= NODE('12', (#127), #36, #67);
#131= CARTESIAN_POINT('13', (1., -3., 1.));
#133= NODE('13', (#131), #36, #67);
#135= CARTESIAN_POINT('14', (2., -3., 1.));
#137= NODE('14', (#135), #36, #67);
#139= CARTESIAN_POINT('15', (3., -3., 1.));
#141= NODE('15', (#139), #36, #67);
#143= CARTESIAN_POINT('16', (4., -3., 1.));
#145= NODE('16', (#143), #36, #67);
#147= CARTESIAN_POINT('17', (5., -3., 1.));
#149= NODE('17', (#147), #36, #67);
#151= CARTESIAN_POINT('18', (6., -3., 1.));
#153= NODE('18', (#151), #36, #67);
#155= CARTESIAN_POINT('19', (7., -3., 1.));
#157= NODE('19', (#155), #36, #67);
#159= CARTESIAN_POINT('20', (8., -3., 1.));

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#161= NODE('20', (#159), #36, #67);
#163= CARTESIAN_POINT('21', (9., -3., 1.));
#165= NODE('21', (#163), #36, #67);
#167= CARTESIAN_POINT('22', (10., -3., 1.));
#169= NODE('22', (#167), #36, #67);
#171= CARTESIAN_POINT('23', (-6.240220000000000E-8, -2., 1.));
#173= NODE('23', (#171), #36, #67);
#175= CARTESIAN_POINT('24', (1., -2., 1.));
#177= NODE('24', (#175), #36, #67);
#179= CARTESIAN_POINT('25', (2., -2., 1.));
#181= NODE('25', (#179), #36, #67);
#183= CARTESIAN_POINT('26', (3., -2., 1.));
#185= NODE('26', (#183), #36, #67);
#187= CARTESIAN_POINT('27', (4., -2., 1.));
#189= NODE('27', (#187), #36, #67);
#191= CARTESIAN_POINT('28', (5., -2., 1.));
#193= NODE('28', (#191), #36, #67);
#195= CARTESIAN_POINT('29', (6., -2., 1.));
#197= NODE('29', (#195), #36, #67);
#199= CARTESIAN_POINT('30', (7., -2., 1.));
#201= NODE('30', (#199), #36, #67);
#203= CARTESIAN_POINT('31', (8., -2., 1.));
#205= NODE('31', (#203), #36, #67);
#207= CARTESIAN_POINT('32', (9., -2., 1.));
#209= NODE('32', (#207), #36, #67);
#211= CARTESIAN_POINT('33', (10., -2., 1.));
#213= NODE('33', (#211), #36, #67);
#215= CARTESIAN_POINT('34', (-6.240220000000000E-8, -1., 1.));
#217= NODE('34', (#215), #36, #67);
#219= CARTESIAN_POINT('35', (1., -1., 1.));
#221= NODE('35', (#219), #36, #67);
#223= CARTESIAN_POINT('36', (2., -1., 1.));
#225= NODE('36', (#223), #36, #67);
#227= CARTESIAN_POINT('37', (3., -1., 1.));
#229= NODE('37', (#227), #36, #67);
#231= CARTESIAN_POINT('38', (4., -1., 1.));
#233= NODE('38', (#231), #36, #67);
#235= CARTESIAN_POINT('39', (5., -1., 1.));
#237= NODE('39', (#235), #36, #67);
#239= CARTESIAN_POINT('40', (6., -1., 1.));
#241= NODE('40', (#239), #36, #67);
#243= CARTESIAN_POINT('41', (7., -1., 1.));
#245= NODE('41', (#243), #36, #67);
#247= CARTESIAN_POINT('42', (8., -1., 1.));
#249= NODE('42', (#247), #36, #67);
#251= CARTESIAN_POINT('43', (9., -1., 1.));
#253= NODE('43', (#251), #36, #67);
#255= CARTESIAN_POINT('44', (10., -1., 1.));
#257= NODE('44', (#255), #36, #67);
#259= CARTESIAN_POINT('45', (-6.240220000000000E-8, -5.275770000000000E-8,
1.));
#261= NODE('45', (#259), #36, #67);
#263= CARTESIAN_POINT('46', (1., -5.275770000000000E-8, 1.));
#265= NODE('46', (#263), #36, #67);
#267= CARTESIAN_POINT('47', (2., -5.275770000000000E-8, 1.));
#269= NODE('47', (#267), #36, #67);
#271= CARTESIAN_POINT('48', (3., -5.275770000000000E-8, 1.));
#273= NODE('48', (#271), #36, #67);
#275= CARTESIAN_POINT('49', (4., -5.275770000000000E-8, 1.));
#277= NODE('49', (#275), #36, #67);
#279= CARTESIAN_POINT('50', (5., -5.275770000000000E-8, 1.));
#281= NODE('50', (#279), #36, #67);
#283= CARTESIAN_POINT('51', (6., -5.275770000000000E-8, 1.));
#285= NODE('51', (#283), #36, #67);
#287= CARTESIAN_POINT('52', (7., -5.275770000000000E-8, 1.));
#289= NODE('52', (#287), #36, #67);
#291= CARTESIAN_POINT('53', (8., -5.275770000000000E-8, 1.));
#293= NODE('53', (#291), #36, #67);
#295= CARTESIAN_POINT('54', (9., -5.275770000000000E-8, 1.));
#297= NODE('54', (#295), #36, #67);
#299= CARTESIAN_POINT('55', (10., -5.275770000000000E-8, 1.));

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#301= NODE('55', (#299), #36, #67);
#303= CARTESIAN_POINT('57', (11., -4., 1.));
#305= NODE('57', (#303), #36, #67);
#307= CARTESIAN_POINT('58', (12., -4., 1.));
#309= NODE('58', (#307), #36, #67);
#311= CARTESIAN_POINT('59', (13., -4., 1.));
#313= NODE('59', (#311), #36, #67);
#315= CARTESIAN_POINT('60', (14., -4., 1.));
#317= NODE('60', (#315), #36, #67);
#319= CARTESIAN_POINT('61', (15., -4., 1.));
#321= NODE('61', (#319), #36, #67);
#323= CARTESIAN_POINT('62', (16., -4., 1.));
#325= NODE('62', (#323), #36, #67);
#327= CARTESIAN_POINT('64', (11., -3., 1.));
#329= NODE('64', (#327), #36, #67);
#331= CARTESIAN_POINT('65', (12., -3., 1.));
#333= NODE('65', (#331), #36, #67);
#335= CARTESIAN_POINT('66', (13., -3., 1.));
#337= NODE('66', (#335), #36, #67);
#339= CARTESIAN_POINT('67', (14., -3., 1.));
#341= NODE('67', (#339), #36, #67);
#343= CARTESIAN_POINT('68', (15., -3., 1.));
#345= NODE('68', (#343), #36, #67);
#347= CARTESIAN_POINT('69', (16., -3., 1.));
#349= NODE('69', (#347), #36, #67);
#351= CARTESIAN_POINT('71', (11., -2., 1.));
#353= NODE('71', (#351), #36, #67);
#355= CARTESIAN_POINT('72', (12., -2., 1.));
#357= NODE('72', (#355), #36, #67);
#359= CARTESIAN_POINT('73', (13., -2., 1.));
#361= NODE('73', (#359), #36, #67);
#363= CARTESIAN_POINT('74', (14., -2., 1.));
#365= NODE('74', (#363), #36, #67);
#367= CARTESIAN_POINT('75', (15., -2., 1.));
#369= NODE('75', (#367), #36, #67);
#371= CARTESIAN_POINT('76', (16., -2., 1.));
#373= NODE('76', (#371), #36, #67);
#375= CARTESIAN_POINT('78', (11., -1., 1.));
#377= NODE('78', (#375), #36, #67);
#379= CARTESIAN_POINT('79', (12., -1., 1.));
#381= NODE('79', (#379), #36, #67);
#383= CARTESIAN_POINT('80', (13., -1., 1.));
#385= NODE('80', (#383), #36, #67);
#387= CARTESIAN_POINT('81', (14., -1., 1.));
#389= NODE('81', (#387), #36, #67);
#391= CARTESIAN_POINT('82', (15., -1., 1.));
#393= NODE('82', (#391), #36, #67);
#395= CARTESIAN_POINT('83', (16., -1., 1.));
#397= NODE('83', (#395), #36, #67);
#399= CARTESIAN_POINT('85', (11., -5.275770000000000E-8, 1.));
#401= NODE('85', (#399), #36, #67);
#403= CARTESIAN_POINT('86', (12., -5.275770000000000E-8, 1.));
#405= NODE('86', (#403), #36, #67);
#407= CARTESIAN_POINT('87', (13., -5.275770000000000E-8, 1.));
#409= NODE('87', (#407), #36, #67);
#411= CARTESIAN_POINT('88', (14., -5.275770000000000E-8, 1.));
#413= NODE('88', (#411), #36, #67);
#415= CARTESIAN_POINT('89', (15., -5.275770000000000E-8, 1.));
#417= NODE('89', (#415), #36, #67);
#419= CARTESIAN_POINT('90', (16., -5.275770000000000E-8, 1.));
#421= NODE('90', (#419), #36, #67);
#423= ELEMENT_MATERIAL('MAT1.1', 'Fea Material', (#435, #443, #449));
#424= MEASURE_REPRESENTATION_ITEM('representation_item_name_1',
THERMODYNAMIC_TEMPERATURE_MEASURE(70.), #10);
#425= PROPERTY_DEFINITION_REPRESENTATION(#426, #428);
#426= PROPERTY_DEFINITION('Material Property Definition', $, #427);
#427= CHARACTERIZED_OBJECT('property', $);
#428= REPRESENTATION('representation_id_1', (#424), #36);
#429= ID_ATTRIBUTE('MAT1.1', #426);
#431= DATA_ENVIRONMENT('DATA_ENV', 'Property_conditions', (#425));
#433= FEA_LINEAR_ELASTICITY('', FEA_ISOTROPIC_SYMMETRIC_TENSOR4_3D((

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1000000.,0.33));
#435= FEA_MATERIAL_PROPERTY_REPRESENTATION(#436,#438,#431);
#436= MATERIAL_PROPERTY('MAT1.1.0',$,#437);
#437= CHARACTERIZED_OBJECT('material_property',$);
#438= REPRESENTATION('representation_id_2',(#433),#36);
#439= DESCRIPTION_ATTRIBUTE('Elasticity',#435);
#442= FEA_MASS_DENSITY('',0.000254);
#443= FEA_MATERIAL_PROPERTY_REPRESENTATION(#444,#445,#431);
#444= MATERIAL_PROPERTY('MAT1.1.1',$,#437);
#445= REPRESENTATION('representation_id_3',(#442),#36);
#446= DESCRIPTION_ATTRIBUTE('MassDensity',#443);
#448= FEA_TANGENTIAL_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION('',
ISOTROPIC_SYMMETRIC_TENSOR2_3D(0.));
#449= FEA_MATERIAL_PROPERTY_REPRESENTATION(#450,#451,#431);
#450= MATERIAL_PROPERTY('MAT1.1.2',$,#437);
#451= REPRESENTATION('representation_id_4',(#448),#36);
#452= DESCRIPTION_ATTRIBUTE('TangentCTE',#449);
#454= SURFACE_3D_ELEMENT_REPRESENTATION('1',(#463),#455,(#80,#89,#133,
#129),#67,#468,#465,#423);
#455=
/* GEOMETRIC_REPRESENTATION_CONTEXT+PARAMETRIC_REPRESENTATION_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)PARAMETRIC_REPRESENTATION_CONTEXT()
REPRESENTATION_CONTEXT('REP_CONTEXT_FEA','3D'));
#457= REPRESENTATION('Default SimDM Fea representation',(#459),#455);
#459= REPRESENTATION_ITEM('Default SimDM item');
#460= ID_ATTRIBUTE('Default SimDM Fea representation',#457);
#461= DESCRIPTION_ATTRIBUTE('Default SimDM Fea representation',#457);
#463= PARAMETRIC_SURFACE_3D_ELEMENT_COORDINATE_SYSTEM('',1,0.);
#465= SURFACE_ELEMENT_PROPERTY('PSHELL.1','',#466);
#466= SURFACE_SECTION_FIELD_CONSTANT(#467);
#467= UNIFORM_SURFACE_SECTION(UNSPECIFIED_VALUE(.UNSPECIFIED.),
UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),2.,
UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.));
#468= SURFACE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER.,
'LINEAR_QUADRILATERAL.CQUAD4',((ENUMERATED_SURFACE_ELEMENT_PURPOSE(
.MEMBRANE_DIRECT.),ENUMERATED_SURFACE_ELEMENT_PURPOSE(.MEMBRANE_SHEAR.))
,(ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_DIRECT.)),
ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_TORSION.)),(
ENUMERATED_SURFACE_ELEMENT_PURPOSE(.NORMAL_TO_PLANE_SHEAR.))),
.QUADRILATERAL.);
#473= SURFACE_3D_ELEMENT_REPRESENTATION('2',(#463),#455,(#89,#93,#137,
#133),#67,#468,#465,#423);
#476= SURFACE_3D_ELEMENT_REPRESENTATION('3',(#463),#455,(#93,#97,#141,
#137),#67,#468,#465,#423);
#479= SURFACE_3D_ELEMENT_REPRESENTATION('4',(#463),#455,(#97,#101,#145,
#141),#67,#468,#465,#423);
#482= SURFACE_3D_ELEMENT_REPRESENTATION('5',(#463),#455,(#101,#105,#149,
#145),#67,#468,#465,#423);
#485= SURFACE_3D_ELEMENT_REPRESENTATION('6',(#463),#455,(#105,#109,#153,
#149),#67,#468,#465,#423);
#488= SURFACE_3D_ELEMENT_REPRESENTATION('7',(#463),#455,(#109,#113,#157,
#153),#67,#468,#465,#423);
#491= SURFACE_3D_ELEMENT_REPRESENTATION('8',(#463),#455,(#113,#117,#161,
#157),#67,#468,#465,#423);
#494= SURFACE_3D_ELEMENT_REPRESENTATION('9',(#463),#455,(#117,#121,#165,
#161),#67,#468,#465,#423);
#497= SURFACE_3D_ELEMENT_REPRESENTATION('10',(#463),#455,(#121,#125,#169,
#165),#67,#468,#465,#423);
#500= SURFACE_3D_ELEMENT_REPRESENTATION('11',(#463),#455,(#129,#133,#177,
#173),#67,#468,#465,#423);
#503= SURFACE_3D_ELEMENT_REPRESENTATION('12',(#463),#455,(#133,#137,#181,
#177),#67,#468,#465,#423);
#506= SURFACE_3D_ELEMENT_REPRESENTATION('13',(#463),#455,(#137,#141,#185,
#181),#67,#468,#465,#423);
#509= SURFACE_3D_ELEMENT_REPRESENTATION('14',(#463),#455,(#141,#145,#189,
#185),#67,#468,#465,#423);
#512= SURFACE_3D_ELEMENT_REPRESENTATION('15',(#463),#455,(#145,#149,#193,
#189),#67,#468,#465,#423);
#515= SURFACE_3D_ELEMENT_REPRESENTATION('16',(#463),#455,(#149,#153,#197,
#193),#67,#468,#465,#423);
#518= SURFACE_3D_ELEMENT_REPRESENTATION('17',(#463),#455,(#153,#157,#201

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, #197), #67, #468, #465, #423);
#521= SURFACE_3D_ELEMENT_REPRESENTATION('18', (#463), #455, (#157, #161, #205
, #201), #67, #468, #465, #423);
#524= SURFACE_3D_ELEMENT_REPRESENTATION('19', (#463), #455, (#161, #165, #209
, #205), #67, #468, #465, #423);
#527= SURFACE_3D_ELEMENT_REPRESENTATION('20', (#463), #455, (#165, #169, #213
, #209), #67, #468, #465, #423);
#530= SURFACE_3D_ELEMENT_REPRESENTATION('21', (#463), #455, (#173, #177, #221
, #217), #67, #468, #465, #423);
#533= SURFACE_3D_ELEMENT_REPRESENTATION('22', (#463), #455, (#177, #181, #225
, #221), #67, #468, #465, #423);
#536= SURFACE_3D_ELEMENT_REPRESENTATION('23', (#463), #455, (#181, #185, #229
, #225), #67, #468, #465, #423);
#539= SURFACE_3D_ELEMENT_REPRESENTATION('24', (#463), #455, (#185, #189, #233
, #229), #67, #468, #465, #423);
#542= SURFACE_3D_ELEMENT_REPRESENTATION('25', (#463), #455, (#189, #193, #237
, #233), #67, #468, #465, #423);
#545= SURFACE_3D_ELEMENT_REPRESENTATION('26', (#463), #455, (#193, #197, #241
, #237), #67, #468, #465, #423);
#548= SURFACE_3D_ELEMENT_REPRESENTATION('27', (#463), #455, (#197, #201, #245
, #241), #67, #468, #465, #423);
#551= SURFACE_3D_ELEMENT_REPRESENTATION('28', (#463), #455, (#201, #205, #249
, #245), #67, #468, #465, #423);
#554= SURFACE_3D_ELEMENT_REPRESENTATION('29', (#463), #455, (#205, #209, #253
, #249), #67, #468, #465, #423);
#557= SURFACE_3D_ELEMENT_REPRESENTATION('30', (#463), #455, (#209, #213, #257
, #253), #67, #468, #465, #423);
#560= SURFACE_3D_ELEMENT_REPRESENTATION('31', (#463), #455, (#217, #221, #261
, #261), #67, #468, #465, #423);
#563= SURFACE_3D_ELEMENT_REPRESENTATION('32', (#463), #455, (#221, #225, #265
, #265), #67, #468, #465, #423);
#566= SURFACE_3D_ELEMENT_REPRESENTATION('33', (#463), #455, (#225, #229, #269
, #269), #67, #468, #465, #423);
#569= SURFACE_3D_ELEMENT_REPRESENTATION('34', (#463), #455, (#229, #233, #273
, #273), #67, #468, #465, #423);
#572= SURFACE_3D_ELEMENT_REPRESENTATION('35', (#463), #455, (#233, #237, #281
, #277), #67, #468, #465, #423);
#575= SURFACE_3D_ELEMENT_REPRESENTATION('36', (#463), #455, (#237, #241, #285
, #281), #67, #468, #465, #423);
#578= SURFACE_3D_ELEMENT_REPRESENTATION('37', (#463), #455, (#241, #245, #289
, #285), #67, #468, #465, #423);
#581= SURFACE_3D_ELEMENT_REPRESENTATION('38', (#463), #455, (#245, #249, #293
, #289), #67, #468, #465, #423);
#584= SURFACE_3D_ELEMENT_REPRESENTATION('39', (#463), #455, (#249, #253, #297
, #293), #67, #468, #465, #423);
#587= SURFACE_3D_ELEMENT_REPRESENTATION('40', (#463), #455, (#253, #257, #301
, #297), #67, #468, #465, #423);
#590= SURFACE_3D_ELEMENT_REPRESENTATION('41', (#592), #455, (#329, #169, #125
), #67, #594, #465, #423);
#592= PARAMETRIC_SURFACE_3D_ELEMENT_COORDINATE_SYSTEM('1, 1, 0.);
#594= SURFACE_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER.,
'LINEAR_TRIANGLE.CTRIA3', ((ENUMERATED_SURFACE_ELEMENT_PURPOSE(
.MEMBRANE_DIRECT.), ENUMERATED_SURFACE_ELEMENT_PURPOSE(.MEMBRANE_SHEAR.))
, (ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_DIRECT.)),
ENUMERATED_SURFACE_ELEMENT_PURPOSE(.BENDING_TORSION.)), (
ENUMERATED_SURFACE_ELEMENT_PURPOSE(.NORMAL_TO_PLANE_SHEAR.))), .TRIANGLE.
);
#599= SURFACE_3D_ELEMENT_REPRESENTATION('42', (#592), #455, (#125, #305, #329
), #67, #594, #465, #423);
#602= SURFACE_3D_ELEMENT_REPRESENTATION('43', (#592), #455, (#305, #309, #329
), #67, #594, #465, #423);
#605= SURFACE_3D_ELEMENT_REPRESENTATION('44', (#592), #455, (#333, #329, #309
), #67, #594, #465, #423);
#608= SURFACE_3D_ELEMENT_REPRESENTATION('45', (#592), #455, (#337, #333, #309
), #67, #594, #465, #423);
#611= SURFACE_3D_ELEMENT_REPRESENTATION('46', (#592), #455, (#309, #313, #337
), #67, #594, #465, #423);
#614= SURFACE_3D_ELEMENT_REPRESENTATION('47', (#592), #455, (#313, #317, #337
), #67, #594, #465, #423);
#617= SURFACE_3D_ELEMENT_REPRESENTATION('48', (#592), #455, (#341, #337, #317
), #67, #594, #465, #423);

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#620= SURFACE_3D_ELEMENT_REPRESENTATION('49', (#592), #455, (#345, #341, #317
), #67, #594, #465, #423);
#623= SURFACE_3D_ELEMENT_REPRESENTATION('50', (#592), #455, (#317, #321, #345
), #67, #594, #465, #423);
#626= SURFACE_3D_ELEMENT_REPRESENTATION('51', (#592), #455, (#321, #325, #345
), #67, #594, #465, #423);
#629= SURFACE_3D_ELEMENT_REPRESENTATION('52', (#592), #455, (#349, #345, #325
), #67, #594, #465, #423);
#632= SURFACE_3D_ELEMENT_REPRESENTATION('53', (#592), #455, (#169, #329, #213
), #67, #594, #465, #423);
#635= SURFACE_3D_ELEMENT_REPRESENTATION('54', (#592), #455, (#353, #213, #329
), #67, #594, #465, #423);
#638= SURFACE_3D_ELEMENT_REPRESENTATION('55', (#592), #455, (#357, #353, #329
), #67, #594, #465, #423);
#641= SURFACE_3D_ELEMENT_REPRESENTATION('56', (#592), #455, (#329, #333, #357
), #67, #594, #465, #423);
#644= SURFACE_3D_ELEMENT_REPRESENTATION('57', (#592), #455, (#333, #337, #357
), #67, #594, #465, #423);
#647= SURFACE_3D_ELEMENT_REPRESENTATION('58', (#592), #455, (#361, #357, #337
), #67, #594, #465, #423);
#650= SURFACE_3D_ELEMENT_REPRESENTATION('59', (#592), #455, (#365, #361, #337
), #67, #594, #465, #423);
#653= SURFACE_3D_ELEMENT_REPRESENTATION('60', (#592), #455, (#337, #341, #365
), #67, #594, #465, #423);
#656= SURFACE_3D_ELEMENT_REPRESENTATION('61', (#592), #455, (#341, #345, #365
), #67, #594, #465, #423);
#659= SURFACE_3D_ELEMENT_REPRESENTATION('62', (#592), #455, (#369, #365, #345
), #67, #594, #465, #423);
#662= SURFACE_3D_ELEMENT_REPRESENTATION('63', (#592), #455, (#373, #369, #345
), #67, #594, #465, #423);
#665= SURFACE_3D_ELEMENT_REPRESENTATION('64', (#592), #455, (#345, #349, #373
), #67, #594, #465, #423);
#668= SURFACE_3D_ELEMENT_REPRESENTATION('65', (#592), #455, (#377, #257, #213
), #67, #594, #465, #423);
#671= SURFACE_3D_ELEMENT_REPRESENTATION('66', (#592), #455, (#213, #353, #377
), #67, #594, #465, #423);
#674= SURFACE_3D_ELEMENT_REPRESENTATION('67', (#592), #455, (#353, #357, #377
), #67, #594, #465, #423);
#677= SURFACE_3D_ELEMENT_REPRESENTATION('68', (#592), #455, (#381, #377, #357
), #67, #594, #465, #423);
#680= SURFACE_3D_ELEMENT_REPRESENTATION('69', (#592), #455, (#385, #381, #357
), #67, #594, #465, #423);
#683= SURFACE_3D_ELEMENT_REPRESENTATION('70', (#592), #455, (#357, #361, #385
), #67, #594, #465, #423);
#686= SURFACE_3D_ELEMENT_REPRESENTATION('71', (#592), #455, (#361, #365, #385
), #67, #594, #465, #423);
#689= SURFACE_3D_ELEMENT_REPRESENTATION('72', (#592), #455, (#389, #385, #365
), #67, #594, #465, #423);
#692= SURFACE_3D_ELEMENT_REPRESENTATION('73', (#592), #455, (#393, #389, #365
), #67, #594, #465, #423);
#695= SURFACE_3D_ELEMENT_REPRESENTATION('74', (#592), #455, (#365, #369, #393
), #67, #594, #465, #423);
#698= SURFACE_3D_ELEMENT_REPRESENTATION('75', (#592), #455, (#369, #373, #393
), #67, #594, #465, #423);
#701= SURFACE_3D_ELEMENT_REPRESENTATION('76', (#592), #455, (#397, #393, #373
), #67, #594, #465, #423);
#704= SURFACE_3D_ELEMENT_REPRESENTATION('77', (#592), #455, (#257, #377, #301
), #67, #594, #465, #423);
#707= SURFACE_3D_ELEMENT_REPRESENTATION('78', (#592), #455, (#401, #301, #377
), #67, #594, #465, #423);
#710= SURFACE_3D_ELEMENT_REPRESENTATION('79', (#592), #455, (#405, #401, #377
), #67, #594, #465, #423);
#713= SURFACE_3D_ELEMENT_REPRESENTATION('80', (#592), #455, (#377, #381, #405
), #67, #594, #465, #423);
#716= SURFACE_3D_ELEMENT_REPRESENTATION('81', (#592), #455, (#381, #385, #405
), #67, #594, #465, #423);
#719= SURFACE_3D_ELEMENT_REPRESENTATION('82', (#592), #455, (#409, #405, #385
), #67, #594, #465, #423);
#722= SURFACE_3D_ELEMENT_REPRESENTATION('83', (#592), #455, (#413, #409, #385
), #67, #594, #465, #423);
#725= SURFACE_3D_ELEMENT_REPRESENTATION('84', (#592), #455, (#385, #389, #413

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),#67,#594,#465,#423);
#728= SURFACE_3D_ELEMENT_REPRESENTATION('85',(#592),#455,(#389,#393,#413
),#67,#594,#465,#423);
#731= SURFACE_3D_ELEMENT_REPRESENTATION('86',(#592),#455,(#417,#413,#393
),#67,#594,#465,#423);
#734= SURFACE_3D_ELEMENT_REPRESENTATION('87',(#592),#455,(#421,#417,#393
),#67,#594,#465,#423);
#737= SURFACE_3D_ELEMENT_REPRESENTATION('88',(#592),#455,(#393,#397,#421
),#67,#594,#465,#423);
#740= CONTROL(#67,'Control.0','FemConvert',
'Nastran job EAS test case ATS3m4',('<SOL>101</SOL>','TIME 600','CEND',
'<GLOBALCASE>0</GLOBALCASE>','<SUBCASE>1</SUBCASE>',
'<SUBCASE>2</SUBCASE>', '<SUBCASE>3</SUBCASE>', '<SUBCASE>4</SUBCASE>',
'ENDDATA'),('NASTRAN'));
#743= SPECIFIED_STATE('STEP DEFAULT','default_initial_state');
#744= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#740,'STATIC STEP 1',1,#743,'
',#1238);
#745= SPECIFIED_STATE('Step 1 Base Specified State',
'Relating Specified State');
#746= SPECIFIED_STATE('SPCCASE_11_21_1','Aggregator SPC 11 Step 1');
#747= SPECIFIED_STATE('SPCVALSTATE_100_21','');
#748= STATE_RELATIONSHIP(
'SPCVALSTATE_100_21 is related to SPCCASE_11_21_1','',#746,#747);
#749= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#747,#752,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#750= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.));
#752= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.0',(#744),#173,#35,(#754
),#757,#758),'');
#754= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.X_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#757= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Y_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#758= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Z_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#759= SPECIFIED_STATE('SPCVALSTATE_101_21','');
#760= STATE_RELATIONSHIP(
'SPCVALSTATE_101_21 is related to SPCCASE_11_21_1','',#746,#759);
#761= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#759,#764,#762,(
CONTEXT_DEPENDENT_MEASURE(0.));
#762= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.));
#764= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.1',(#744),#80,#35,(#754
),');
#768= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#759,#769,#762,(
CONTEXT_DEPENDENT_MEASURE(0.));
#769= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.2',(#744),#129,#35,(#754
),');
#773= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#759,#774,#762,(
CONTEXT_DEPENDENT_MEASURE(0.));
#774= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.3',(#744),#217,#35,(#754
),');
#778= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#759,#779,#762,(
CONTEXT_DEPENDENT_MEASURE(0.));
#779= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.4',(#744),#261,#35,(#754
),');
#783= SPECIFIED_STATE('SPCVALSTATE_110_21','');
#784= STATE_RELATIONSHIP(
'SPCVALSTATE_110_21 is related to SPCCASE_11_21_1','',#746,#783);
#785= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#788,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#786= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_ROTATION.));
#788= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.5',(#744),#80,#35,(#790,
#793),');
#790= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.)
,CONTEXT_DEPENDENT_MEASURE(1.));
#793= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(.Y_ROTATION.)
,CONTEXT_DEPENDENT_MEASURE(1.));
#794= SINGLE POINT CONSTRAINT ELEMENT VALUES(#783,#795,#786,(

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CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#795= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.6',(#744),#89,#35,(#790,
#793),'');
#799= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#800,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#800= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.7',(#744),#93,#35,(#790,
#793),'');
#804= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#805,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#805= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.8',(#744),#97,#35,(#790,
#793),'');
#809= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#810,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#810= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.9',(#744),#101,#35,(#790,
#793),'');
#814= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#815,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#815= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.10',(#744),#105,#35,(
#790,#793),'');
#819= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#820,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#820= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.11',(#744),#109,#35,(
#790,#793),'');
#824= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#825,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#825= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.12',(#744),#113,#35,(
#790,#793),'');
#829= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#830,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#830= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.13',(#744),#117,#35,(
#790,#793),'');
#834= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#835,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#835= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.14',(#744),#121,#35,(
#790,#793),'');
#839= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#840,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#840= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.15',(#744),#125,#35,(
#790,#793),'');
#844= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#845,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#845= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.16',(#744),#129,#35,(
#790,#793),'');
#849= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#850,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#850= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.17',(#744),#133,#35,(
#790,#793),'');
#854= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#855,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#855= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.18',(#744),#137,#35,(
#790,#793),'');
#859= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#860,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#860= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.19',(#744),#141,#35,(
#790,#793),'');
#864= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#865,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#865= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.20',(#744),#145,#35,(
#790,#793),'');
#869= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#870,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#870= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.21',(#744),#149,#35,(
#790,#793),'');
#874= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#875,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#875= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.22',(#744),#153,#35,(
#790,#793),'');
#879= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#880,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#880= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.23',(#744),#157,#35,(
#790,#793),'');

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#790,#793),'');
#974= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#975,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#975= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.42',(#744),#233,#35,(
#790,#793),'');
#979= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#980,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#980= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.43',(#744),#237,#35,(
#790,#793),'');
#984= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#985,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#985= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.44',(#744),#241,#35,(
#790,#793),'');
#989= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#990,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#990= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.45',(#744),#245,#35,(
#790,#793),'');
#994= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#995,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#995= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.46',(#744),#249,#35,(
#790,#793),'');
#999= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1000,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1000= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.47',(#744),#253,#35,(
#790,#793),'');
#1004= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1005,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1005= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.48',(#744),#257,#35,(
#790,#793),'');
#1009= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1010,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1010= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.49',(#744),#261,#35,(
#790,#793),'');
#1014= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1015,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1015= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.50',(#744),#265,#35,(
#790,#793),'');
#1019= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1020,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1020= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.51',(#744),#269,#35,(
#790,#793),'');
#1024= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1025,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1025= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.52',(#744),#273,#35,(
#790,#793),'');
#1029= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1030,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1030= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.53',(#744),#277,#35,(
#790,#793),'');
#1034= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1035,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1035= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.54',(#744),#281,#35,(
#790,#793),'');
#1039= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1040,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1040= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.55',(#744),#285,#35,(
#790,#793),'');
#1044= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1045,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1045= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.56',(#744),#289,#35,(
#790,#793),'');
#1049= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1050,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1050= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.57',(#744),#293,#35,(
#790,#793),'');
#1054= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1055,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));
#1055= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.58',(#744),#297,#35,(
#790,#793),'');
#1059= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1060,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.)));

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CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1150= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.77',(#744),#373,#35,(
#790,#793),'');
#1154= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1155,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1155= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.78',(#744),#377,#35,(
#790,#793),'');
#1159= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1160,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1160= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.79',(#744),#381,#35,(
#790,#793),'');
#1164= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1165,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1165= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.80',(#744),#385,#35,(
#790,#793),'');
#1169= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1170,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1170= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.81',(#744),#389,#35,(
#790,#793),'');
#1174= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1175,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1175= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.82',(#744),#393,#35,(
#790,#793),'');
#1179= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1180,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1180= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.83',(#744),#397,#35,(
#790,#793),'');
#1184= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1185,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1185= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.84',(#744),#401,#35,(
#790,#793),'');
#1189= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1190,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1190= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.85',(#744),#405,#35,(
#790,#793),'');
#1194= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1195,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1195= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.86',(#744),#409,#35,(
#790,#793),'');
#1199= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1200,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1200= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.87',(#744),#413,#35,(
#790,#793),'');
#1204= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1205,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1205= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.88',(#744),#417,#35,(
#790,#793),'');
#1209= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#783,#1210,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1210= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.89',(#744),#421,#35,(
#790,#793),'');
#1214= STATE_RELATIONSHIP(
'SPCCASE_11_21_1 is related to Step 1 Base Specified State','',#745,#746
);
#1215= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_21',
'Overall Factor Combined State');
#1217= STATE_COMPONENT('OverallComp','',#1215,1.);
#1219= SPECIFIED_STATE('LOADSTATECORE_200','Core Loads Specified State'
);
#1220= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#325,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-125.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1221= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#1224= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#349,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-250.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1226= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#373,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-250.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);

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#1228= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#397,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-250.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1230= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#421,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-125.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1232= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_200',
'Item Factor State');
#1233= STATE_RELATIONSHIP('LOADSTATEITEM_200 is related to OverallComp',
',',#1217,#1232);
#1234= STATE_COMPONENT('ItemComp_21_200','',#1232,1.);
#1236= STATE_RELATIONSHIP(
'LOADSTATECORE_200 is related to ItemComp_21_200','',#1234,#1219);
#1237= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_21 is related to Step 1 Base Specified State','',
#745,#1215);
#1238= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 1','',
#745);
#1239= OUTPUT_REQUEST_STATE('Step 1 Output Request State','',(#744));
#1241= NODAL_FREEDOM_VALUES(#1239,#1245,#35,#1242,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.)));
#1242= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(
.Y_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(.Z_ROTATION.)));
#1245= NODE_GROUP('','ALL',#67, (#80,#89,#93,#97,#101,#105,#109,#113,#117
,#121,#125,#129,#133,#137,#141,#145,#149,#153,#157,#161,#165,#169,#173,
#177,#181,#185,#189,#193,#197,#201,#205,#209,#213,#217,#221,#225,#229,
#233,#237,#241,#245,#249,#253,#257,#261,#265,#269,#273,#277,#281,#285,
#289,#293,#297,#301,#305,#309,#313,#317,#321,#325,#329,#333,#337,#341,
#345,#349,#353,#357,#361,#365,#369,#373,#377,#381,#385,#389,#393,#397,
#401,#405,#409,#413,#417,#421));
#1246= ID_ATTRIBUTE('ALL',#1245);
#1248= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#1239,
#468,.F.,(#1249,#1262,#1267,#1272,#1277,#1282,#1286,#1288,#1290,#1292),
VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#1249= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1250,$);
#1250= SURFACE_VOLUME_ELEMENT_LOCATION(#1251,#1259);
#1251= SURFACE_ELEMENT_LOCATION(#1252);
#1252= FEA_PARAMETRIC_POINT('sQuadN_0',(0.,0.,0.));
#1254= REPRESENTATION('dpr0',(#1252,#1265,#1270,#1275,#1280,#1298),#1255
);
#1255= PARAMETRIC_REPRESENTATION_CONTEXT('FEA parametric context',
'Parametric');
#1259= SURFACE_SECTION_ELEMENT_LOCATION_DIMENSIONLESS(.F.,(-1.));
#1262= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1263,$);
#1263= SURFACE_VOLUME_ELEMENT_LOCATION(#1264,#1259);
#1264= SURFACE_ELEMENT_LOCATION(#1265);
#1265= FEA_PARAMETRIC_POINT('sQuadN_1',(-1.,-1.,0.));
#1267= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1268,$);
#1268= SURFACE_VOLUME_ELEMENT_LOCATION(#1269,#1259);
#1269= SURFACE_ELEMENT_LOCATION(#1270);
#1270= FEA_PARAMETRIC_POINT('sQuadN_2',(1.,-1.,0.));
#1272= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1273,$);
#1273= SURFACE_VOLUME_ELEMENT_LOCATION(#1274,#1259);
#1274= SURFACE_ELEMENT_LOCATION(#1275);
#1275= FEA_PARAMETRIC_POINT('sQuadN_3',(1.,1.,0.));
#1277= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1278,$);
#1278= SURFACE_VOLUME_ELEMENT_LOCATION(#1279,#1259);
#1279= SURFACE_ELEMENT_LOCATION(#1280);
#1280= FEA_PARAMETRIC_POINT('sQuadN_4',(-1.,1.,0.));
#1282= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1283,$);

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#1283= SURFACE_VOLUME_ELEMENT_LOCATION(#1251,#1284);
#1284= SURFACE_SECTION_ELEMENT_LOCATION_DIMENSIONLESS(.F.,(1.));
#1286= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1287,$);
#1287= SURFACE_VOLUME_ELEMENT_LOCATION(#1264,#1284);
#1288= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1289,$);
#1289= SURFACE_VOLUME_ELEMENT_LOCATION(#1269,#1284);
#1290= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1291,$);
#1291= SURFACE_VOLUME_ELEMENT_LOCATION(#1274,#1284);
#1292= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1293,$);
#1293= SURFACE_VOLUME_ELEMENT_LOCATION(#1279,#1284);
#1294= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#1239,
#594,.F.,(#1295,#1303),VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#1295= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1296,$);
#1296= SURFACE_VOLUME_ELEMENT_LOCATION(#1297,#1300);
#1297= SURFACE_ELEMENT_LOCATION(#1298);
#1298= FEA_PARAMETRIC_POINT('sTriN_0',(0.,0.,0.));
#1300= SURFACE_SECTION_ELEMENT_LOCATION_DIMENSIONLESS(.F.,(-1.));
#1303= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1304,$);
#1304= SURFACE_VOLUME_ELEMENT_LOCATION(#1297,#1305);
#1305= SURFACE_SECTION_ELEMENT_LOCATION_DIMENSIONLESS(.F.,(1.));
#1307= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#740,'STATIC STEP 2',2,#743,
'',#1797);
#1308= SPECIFIED_STATE('Step 2 Base Specified State',
'Relating Specified State');
#1309= SPECIFIED_STATE('SPCCASE_12_22_2','Aggregator SPC 12 Step 2');
#1310= SPECIFIED_STATE('SPCVALSTATE_100_22','');
#1311= STATE_RELATIONSHIP(
'SPCVALSTATE_100_22 is related to SPCCASE_12_22_2','',#1309,#1310);
#1312= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1310,#1313,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1313= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.90',(#1307),#173,#35,(
#754,#757,#758),'');
#1317= SPECIFIED_STATE('SPCVALSTATE_102_22','');
#1318= STATE_RELATIONSHIP(
'SPCVALSTATE_102_22 is related to SPCCASE_12_22_2','',#1309,#1317);
#1319= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1317,#1320,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1320= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.91',(#1307),#80,#35,(
#754,#757,#758),'');
#1324= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1317,#1325,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1325= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.92',(#1307),#129,#35,(
#754,#757,#758),'');
#1329= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1317,#1330,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1330= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.93',(#1307),#217,#35,(
#754,#757,#758),'');
#1334= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1317,#1335,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1335= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.94',(#1307),#261,#35,(
#754,#757,#758),'');
#1339= SPECIFIED_STATE('SPCVALSTATE_110_22','');
#1340= STATE_RELATIONSHIP(
'SPCVALSTATE_110_22 is related to SPCCASE_12_22_2','',#1309,#1339);
#1341= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339,#1342,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1342= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.95',(#1307),#80,#35,(
#790,#793),'');
#1346= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339,#1347,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));

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#1702= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.167', (#1307), #373, #35, (
#790, #793), '');
#1706= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1707, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1707= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.168', (#1307), #377, #35, (
#790, #793), '');
#1711= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1712, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1712= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.169', (#1307), #381, #35, (
#790, #793), '');
#1716= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1717, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1717= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.170', (#1307), #385, #35, (
#790, #793), '');
#1721= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1722, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1722= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.171', (#1307), #389, #35, (
#790, #793), '');
#1726= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1727, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1727= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.172', (#1307), #393, #35, (
#790, #793), '');
#1731= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1732, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1732= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.173', (#1307), #397, #35, (
#790, #793), '');
#1736= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1737, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1737= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.174', (#1307), #401, #35, (
#790, #793), '');
#1741= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1742, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1742= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.175', (#1307), #405, #35, (
#790, #793), '');
#1746= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1747, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1747= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.176', (#1307), #409, #35, (
#790, #793), '');
#1751= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1752, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1752= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.177', (#1307), #413, #35, (
#790, #793), '');
#1756= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1757, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1757= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.178', (#1307), #417, #35, (
#790, #793), '');
#1761= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1339, #1762, #786, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#1762= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.179', (#1307), #421, #35, (
#790, #793), '');
#1766= STATE_RELATIONSHIP(
'SPCCASE_12_22_2 is related to Step 2 Base Specified State', '', #1308,
#1309);
#1767= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_22',
'Overall Factor Combined State');
#1768= STATE_COMPONENT('OverallComp', '', #1767, 1.);
#1770= SPECIFIED_STATE('LOADSTATECORE_300', 'Core Loads Specified State'
);
#1771= NODAL_FREEDOM_ACTION_DEFINITION(#1770, #301, #35, #1221, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.), .APPLIED_LOADS.);
#1773= NODAL_FREEDOM_ACTION_DEFINITION(#1770, #421, #35, #1221, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.), .APPLIED_LOADS.);
#1775= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_300',
'Item Factor State');
#1776= STATE_RELATIONSHIP('LOADSTATEITEM_300 is related to OverallComp',
'', #1768, #1775);
#1777= STATE_COMPONENT('ItemComp_22_300', '', #1775, 1.);
#1779= STATE_RELATIONSHIP(
'LOADSTATECORE 300 is related to ItemComp 22 300', '', #1777, #1770);

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#1780= SPECIFIED_STATE('LOADSTATECORE_400','Core Loads Specified State'
);
#1781= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#401,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1783= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#405,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1785= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#409,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1787= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#413,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1789= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#417,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#1791= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_400',
'Item Factor State');
#1792= STATE_RELATIONSHIP('LOADSTATEITEM_400 is related to OverallComp',
',',#1768,#1791);
#1793= STATE_COMPONENT('ItemComp_22_400','',#1791,1.);
#1795= STATE_RELATIONSHIP(
'LOADSTATECORE_400 is related to ItemComp_22_400','',#1793,#1780);
#1796= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_22 is related to Step 2 Base Specified State','',
#1308,#1767);
#1797= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 2','',
#1308);
#1798= OUTPUT_REQUEST_STATE('Step 2 Output Request State','',(#1307));
#1800= NODAL_FREEDOM_VALUES(#1798,#1245,#35,#1242,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.)));
#1802= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#1798,
#468,.F.,(#1803,#1805,#1806,#1807,#1808,#1809,#1810,#1811,#1812,#1813),
VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#1803= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1250,$);
#1805= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1263,$);
#1806= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1268,$);
#1807= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1273,$);
#1808= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1278,$);
#1809= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1283,$);
#1810= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1287,$);
#1811= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1289,$);
#1812= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1291,$);
#1813= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1293,$);
#1814= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#1798,
#594,.F.,(#1815,#1817),VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#1815= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1296,$);
#1817= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1304,$);
#1818= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#740,'STATIC STEP 3',3,#743,
',',#2291);
#1819= SPECIFIED_STATE('Step 3 Base Specified State',
'Relating Specified State');
#1820= SPECIFIED_STATE('SPCCASE_12_23_3','Aggregator SPC 12 Step 3');
#1821= SPECIFIED_STATE('SPCVLSTATE_100_23','');
#1822= STATE_RELATIONSHIP(
'SPCVALSTATE 100 23 is related to SPCCASE 12 23 3','',#1820,#1821);

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#1823= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1821,#1824,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1824= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.180',(#1818),#173,#35,(
#754,#757,#758),'');
#1828= SPECIFIED_STATE('SPCVALSTATE_102_23','');
#1829= STATE_RELATIONSHIP(
'SPCVALSTATE_102_23 is related to SPCCASE_12_23_3','',#1820,#1828);
#1830= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1828,#1831,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1831= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.181',(#1818),#80,#35,(
#754,#757,#758),'');
#1835= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1828,#1836,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1836= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.182',(#1818),#129,#35,(
#754,#757,#758),'');
#1840= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1828,#1841,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1841= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.183',(#1818),#217,#35,(
#754,#757,#758),'');
#1845= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1828,#1846,#750,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#1846= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.184',(#1818),#261,#35,(
#754,#757,#758),'');
#1850= SPECIFIED_STATE('SPCVALSTATE_110_23','');
#1851= STATE_RELATIONSHIP(
'SPCVALSTATE_110_23 is related to SPCCASE_12_23_3','',#1820,#1850);
#1852= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1853,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1853= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.185',(#1818),#80,#35,(
#790,#793),'');
#1857= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1858,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1858= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.186',(#1818),#89,#35,(
#790,#793),'');
#1862= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1863,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1863= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.187',(#1818),#93,#35,(
#790,#793),'');
#1867= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1868,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1868= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.188',(#1818),#97,#35,(
#790,#793),'');
#1872= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1873,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1873= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.189',(#1818),#101,#35,(
#790,#793),'');
#1877= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1878,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1878= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.190',(#1818),#105,#35,(
#790,#793),'');
#1882= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1883,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1883= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.191',(#1818),#109,#35,(
#790,#793),'');
#1887= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1888,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1888= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.192',(#1818),#113,#35,(
#790,#793),'');
#1892= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1893,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1893= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.193',(#1818),#117,#35,(
#790,#793),'');
#1897= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#1898,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#1898= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.194',(#1818),#121,#35,(
#790,#793),'');

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#2257= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#2258,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#2258= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.266',(#1818),#409,#35,(
#790,#793),'');
#2262= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#2263,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#2263= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.267',(#1818),#413,#35,(
#790,#793),'');
#2267= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#2268,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#2268= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.268',(#1818),#417,#35,(
#790,#793),'');
#2272= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#1850,#2273,#786,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.));
#2273= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_110.269',(#1818),#421,#35,(
#790,#793),'');
#2277= STATE_RELATIONSHIP(
'SPCCASE_12_23_3 is related to Step 3 Base Specified State','',#1819,
#1820);
#2278= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_23',
'Overall Factor Combined State');
#2279= STATE_COMPONENT('OverallComp','',#2278,1.);
#2281= STATE_RELATIONSHIP('LOADSTATEITEM_200 is related to OverallComp',
'',#2279,#1232);
#2282= STATE_COMPONENT('ItemComp_23_200','',#1232,1.);
#2283= STATE_RELATIONSHIP(
'LOADSTATECORE_200 is related to ItemComp_23_200','',#2282,#1219);
#2284= STATE_RELATIONSHIP('LOADSTATEITEM_300 is related to OverallComp',
'',#2279,#1775);
#2285= STATE_COMPONENT('ItemComp_23_300','',#1775,1.);
#2286= STATE_RELATIONSHIP(
'LOADSTATECORE_300 is related to ItemComp_23_300','',#2285,#1770);
#2287= STATE_RELATIONSHIP('LOADSTATEITEM_400 is related to OverallComp',
'',#2279,#1791);
#2288= STATE_COMPONENT('ItemComp_23_400','',#1791,1.);
#2289= STATE_RELATIONSHIP(
'LOADSTATECORE_400 is related to ItemComp_23_400','',#2288,#1780);
#2290= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_23 is related to Step 3 Base Specified State','',
#1819,#2278);
#2291= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 3','',
#1819);
#2292= OUTPUT_REQUEST_STATE('Step 3 Output Request State','',(#1818));
#2294= NODAL_FREEDOM_VALUES(#2292,#1245,#35,#1242,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.));
#2296= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#2292,
#468,.F.,(#2297,#2299,#2300,#2301,#2302,#2303,#2304,#2305,#2306,#2307),
VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2297= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1250,$);
#2299= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1263,$);
#2300= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1268,$);
#2301= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1273,$);
#2302= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1278,$);
#2303= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1283,$);
#2304= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1287,$);
#2305= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1289,$);
#2306= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1291,$);
#2307= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1293,$);
#2308= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#2292,

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#594, .F., (#2309, #2311), VOLUME_TENSOR2_3D_VARIABLE(.STRESS.);
#2309= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.), #1296, $);
#2311= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.), #1304, $);
#2312= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#740, 'STATIC STEP 4', 4, #743,
'', #2382);
#2313= SPECIFIED_STATE('Step 4 Base Specified State',
'Relating Specified State');
#2314= SPECIFIED_STATE('SPCCASE_103_500_4', 'Aggregator SPC 103 Step 4');
#2315= SPECIFIED_STATE('SPCVALSTATE_103_500', '');
#2316= STATE_RELATIONSHIP(
'SPCVALSTATE_103_500 is related to SPCCASE_103_500_4', '', #2314, #2315);
#2317= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2318, #750, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)));
#2318= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.270', (#2312), #173, #35, (
#754, #757, #758), '');
#2322= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2325, #2323, (
CONTEXT_DEPENDENT_MEASURE(0.), CONTEXT_DEPENDENT_MEASURE(0.)));
#2323= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#2325= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.271', (#2312), #373, #35, (
#757, #758), '');
#2329= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2332, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2330= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#2332= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.272', (#2312), #80, #35, (
#758), '');
#2336= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2337, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2337= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.273', (#2312), #129, #35, (
#758), '');
#2341= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2342, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2342= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.274', (#2312), #217, #35, (
#758), '');
#2346= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2347, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2347= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.275', (#2312), #261, #35, (
#758), '');
#2351= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2352, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2352= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.276', (#2312), #325, #35, (
#758), '');
#2356= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2357, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2357= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.277', (#2312), #349, #35, (
#758), '');
#2361= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2362, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2362= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.278', (#2312), #397, #35, (
#758), '');
#2366= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2315, #2367, #2330, (
CONTEXT_DEPENDENT_MEASURE(0.)));
#2367= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_103.279', (#2312), #421, #35, (
#758), '');
#2371= STATE_RELATIONSHIP(
'SPCCASE_103_500_4 is related to Step 4 Base Specified State', '', #2313,
#2314);
#2372= SPECIFIED_STATE('LOADSTATECORE_500', 'Core Loads Specified State'
);
#2373=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372, #491, CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.), 2, $);
#2374=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372, #494, CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.), 2, $);
#2375=

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SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#521,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2376=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#524,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2377=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#551,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2378=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#554,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2379=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#581,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2380=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#584,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2381= STATE_RELATIONSHIP(
'LOADSTATECORE_500 is related to Step 4 Base Specified State','',#2313,
#2372);
#2382= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 4','',
#2313);
#2383= OUTPUT_REQUEST_STATE('Step 4 Output Request State','',(#2312));
#2385= NODAL_FREEDOM_VALUES(#2383,#1245,#35,#1242,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.)));
#2387= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#2383,
#468,.F.,(#2388,#2390,#2391,#2392,#2393,#2394,#2395,#2396,#2397,#2398),
VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2388= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1250,$);
#2390= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1263,$);
#2391= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1268,$);
#2392= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1273,$);
#2393= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1278,$);
#2394= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1283,$);
#2395= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1287,$);
#2396= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1289,$);
#2397= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1291,$);
#2398= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1293,$);
#2399= SURFACE_3D_ELEMENT_LOCATION_POINT_VOLUME_VARIABLE_VALUES(#2383,
#594,.F.,(#2400,#2402),VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2400= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1296,$);
#2402= SURFACE_3D_ELEMENT_VALUE_AND_VOLUME_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#1304,$);
#2403= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#325,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-125.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2405= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#349,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-250.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2407= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#373,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-250.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);

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#2409= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#397,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-250.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2411= NODAL_FREEDOM_ACTION_DEFINITION(#1219,#421,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(-125.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2413= NODAL_FREEDOM_ACTION_DEFINITION(#1770,#301,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2415= NODAL_FREEDOM_ACTION_DEFINITION(#1770,#421,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2417= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#401,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2419= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#405,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2421= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#409,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2423= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#413,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2425= NODAL_FREEDOM_ACTION_DEFINITION(#1780,#417,#35,#1221,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-20.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2427=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#491,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2428=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#494,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2429=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#521,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2430=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#524,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2431=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#551,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2432=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#554,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2433=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#581,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
#2434=
SURFACE_3D_ELEMENT_BOUNDARY_CONSTANT_SPECIFIED_SURFACE_VARIABLE_VALUE(
#2372,#584,CONTEXT_DEPENDENT_MEASURE(125.),
BOUNDARY_SURFACE_SCALAR_VARIABLE(.PRESSURE.),2,$);
ENDSEC;
END-ISO-10303-21;

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11.4 ATS4m4.stp

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ISO-10303-21;
HEADER;

/*****
* Creation date:           Tue Feb 07 13:53:33 2017
* Schema:                 AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF
*****/

FILE_DESCRIPTION(('','2;1');
FILE_NAME(
'O:\projects\Crystal\software_FEM\converters\examples\db\e.DataRepository.Fem_Model'
,
'2017-02-07T13:53:33',
('ANONYMOUS USER'),
('ANONYMOUS ORGANISATION'),
'EDMsix Version 2.0100.a14 Jan 31 2017',
'',
'');
FILE_SCHEMA(('AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF'));
ENDSEC;

DATA;
#1= APPLICATION_CONTEXT(
'AP209_MULTIDISCIPLINARY_ANALYSIS_AND_DESIGN_MIM_LF');
#3= ID_ATTRIBUTE('to be decided',#1);
#4= DESCRIPTION_ATTRIBUTE('to be decided',#1);
#5= APPLICATION_PROTOCOL_DEFINITION('international standard',
'ap209_multidisciplinary_analysis_and_design',2011,#1);
#6= DIMENSIONAL_EXPONENTS(0.,0.,0.,0.,0.,0.,0.);
#7= /* LENGTH_UNIT+SI_UNIT */(LENGTH_UNIT()NAMED_UNIT(*)SI_UNIT($,
.METRE.));
#8= /* MASS_UNIT+SI_UNIT */(MASS_UNIT()NAMED_UNIT(*)SI_UNIT(.KILO.,
.GRAM.));
#9= /* SI_UNIT+TIME_UNIT */(NAMED_UNIT(*)SI_UNIT($,.SECOND.)TIME_UNIT()
);
#10= /* SI_UNIT+THERMODYNAMIC_TEMPERATURE_UNIT */(NAMED_UNIT(*)SI_UNIT($,
.DEGREE_CELSIUS.)THERMODYNAMIC_TEMPERATURE_UNIT());
#11= /* PLANE_ANGLE_UNIT+SI_UNIT */(NAMED_UNIT(*)PLANE_ANGLE_UNIT()
SI_UNIT($,.RADIAN.));
#12= SI_FORCE_UNIT((#13,#14,#15),*,$,.NEWTON.);
#13= DERIVED_UNIT_ELEMENT(#8,1.);
#14= DERIVED_UNIT_ELEMENT(#7,1.);
#15= DERIVED_UNIT_ELEMENT(#9,-2.);
#17= SI_FREQUENCY_UNIT((#18),*,$,.HERTZ.);
#18= DERIVED_UNIT_ELEMENT(#9,-1.);
#20= SI_PRESSURE_UNIT((#13,#21,#15),*,$,.PASCAL.);
#21= DERIVED_UNIT_ELEMENT(#7,-1.);
#23= SI_ENERGY_UNIT((#13,#24,#15),*,$,.JOULE.);
#24= DERIVED_UNIT_ELEMENT(#7,2.);
#26= SI_POWER_UNIT((#13,#24,#27),*,$,.WATT.);
#27= DERIVED_UNIT_ELEMENT(#9,-3.);
#29= DIRECTION('RefX',(1.,0.,0.));
#31= DIRECTION('AxisZ',(0.,0.,1.));
#33= CARTESIAN_POINT('',(0.,0.,0.));
#35= FEA_AXIS2_PLACEMENT_3D('0',#33,#31,#29,.CARTESIAN.,
'FEA_BASIC_COORD_SYSTEM.0');
#36= /* GEOMETRIC REPRESENTATION_CONTEXT+GLOBAL_UNIT_ASSIGNED_CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)GLOBAL_UNIT_ASSIGNED_CONTEXT((#23,
#12,#17,#7,#8,#11,#26,#20,#10,#9))REPRESENTATION_CONTEXT(
'FEA_BASIC_COORD_SYSTEM.0','3d'));
#39= ORGANIZATION($,'default-organization',$);
#40= PRODUCT('default-id.0','default-fea-part','',(#42));
#42= PRODUCT_CONTEXT('design_context',#1,'design_context');
#44= PRODUCT_RELATED_PRODUCT_CATEGORY('part',$,(#40));
#45= ID_ATTRIBUTE('',#44);
#47= APPLIED_IDENTIFICATION_ASSIGNMENT('default-id.0',#48,(#50,#56,#40)
);
#48= IDENTIFICATION_ROLE('default-role',$);
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#49= PRODUCT_RELATED_PRODUCT_CATEGORY('product',$, (#40));
#50= PRODUCT_DEFINITION_FORMATION('default-id.0',',', #40);
#51= GROUP('id', $);
#52= APPLIED_CLASSIFICATION_ASSIGNMENT(#51, #54, (#47));
#54= CLASSIFICATION_ROLE('', $);
#56= PRODUCT_DEFINITION('default-id.0', $, #50, #57);
#57= PRODUCT_DEFINITION_CONTEXT('assembly definition', #1,
'life cycle stage');
#58= APPLIED_CLASSIFICATION_ASSIGNMENT(#59, #60, (#56));
#59= GROUP('default-gpvt-type', $);
#60= CLASSIFICATION_ROLE('view_type', $);
#63= ORGANIZATION_ROLE('id context');
#64= APPLIED_ORGANIZATION_ASSIGNMENT(#39, #63, (#47));
#66= NAME_ATTRIBUTE('', #56);
#67= FEA_MODEL_3D('Identification', (#35), #36,
'NASTRAN BDF Converter v0.0.0', ('NASTRAN'), 'AnalysisModelType');
#70= STRUCTURAL_RESPONSE_PROPERTY_DEFINITION_REPRESENTATION(#71, #67);
#71= STRUCTURAL_RESPONSE_PROPERTY('structural_response_property_id_1', $,
#72);
#72= FEA_MODEL_DEFINITION('fea_model_definition_id_1', $, #73, .U.);
#73= PRODUCT_DEFINITION_SHAPE('name', $, #56);
#74= CARTESIAN_POINT('0', (0., 0., 0.));
#76= DUMMY_NODE('0', (#74), #36, #67);
#78= CARTESIAN_POINT('1', (0., -4., -3.4315200000000000E-8));
#80= NODE('1', (#78), #36, #67);
#81= SHAPE_DEFINITION_REPRESENTATION(#73, #82);
#82= POINT_REPRESENTATION('point_representation_name_1', (#83, #35), #36);
#83= NODE_SET('node_set_name_1', (#80, #89, #93, #97, #101, #105, #109, #113,
#117, #121, #125, #129, #133, #137, #141, #145, #149, #153, #157, #161, #165, #169,
#173, #177, #181, #185, #189, #193, #197, #201, #205, #209, #213, #217, #221, #225,
#229, #233, #237, #241, #245, #249, #253, #257, #261, #265, #269, #273, #277, #281,
#285, #289, #293, #297, #301, #305, #309, #313, #317, #321, #325, #329, #333, #337,
#341, #345, #349, #353, #357, #361, #365, #369, #373, #377, #381, #385, #389, #393,
#397, #401, #405, #409, #413, #417, #421, #425, #429, #433, #437, #441, #445, #449,
#453, #457, #461, #465, #469, #473, #477, #481, #485, #489, #493, #497, #501, #505,
#509, #513, #517, #521, #525, #529, #533, #537, #541, #545, #549, #553, #557, #561,
#565, #569, #573, #577, #581, #585, #589, #593, #597, #601, #605, #609, #613, #617,
#621, #625, #629, #633, #637, #641, #645, #649, #653, #657, #661, #665, #669, #673,
#677, #681, #685, #689, #693, #697, #701, #705, #709, #713, #717, #721, #725, #729,
#733, #737, #741, #745, #749, #753, #757, #761, #765, #769, #773, #777, #781, #785,
#789, #793, #797, #801, #805, #809, #813, #817, #821, #825, #829, #833, #837, #841,
#845, #849, #853, #857, #861, #865, #869, #873, #877, #881, #885, #889, #893, #897,
#901, #905, #909, #913, #917, #921, #925, #929, #933, #937, #941, #945, #949, #953,
#957, #961, #965, #969, #973, #977, #981, #985, #989, #993, #997, #1001, #1005, #1009,
#1013, #1017, #1021, #1025, #1029, #1033, #1037, #1041, #1045, #1049, #1053, #1057,
#1061, #1065, #1069, #1073, #1077, #1081, #1085, #1089, #1093, #1097, #1101));
#87= CARTESIAN_POINT('2', (0., -3., -3.4315200000000000E-8));
#89= NODE('2', (#87), #36, #67);
#91= CARTESIAN_POINT('3', (0., -2., -3.4315200000000000E-8));
#93= NODE('3', (#91), #36, #67);
#95= CARTESIAN_POINT('4', (0., -1., -3.4315200000000000E-8));
#97= NODE('4', (#95), #36, #67);
#99= CARTESIAN_POINT('5', (0., -6.0137600000000000E-9, -3.4315200000000000E-8
));
#101= NODE('5', (#99), #36, #67);
#103= CARTESIAN_POINT('6', (0., -4., 1.));
#105= NODE('6', (#103), #36, #67);
#107= CARTESIAN_POINT('7', (0., -3., 1.));
#109= NODE('7', (#107), #36, #67);
#111= CARTESIAN_POINT('8', (0., -2., 1.));
#113= NODE('8', (#111), #36, #67);
#115= CARTESIAN_POINT('9', (0., -1., 1.));
#117= NODE('9', (#115), #36, #67);
#119= CARTESIAN_POINT('10', (0., -6.0137600000000000E-9, 1.));
#121= NODE('10', (#119), #36, #67);
#123= CARTESIAN_POINT('11', (0., -4., 2.));
#125= NODE('11', (#123), #36, #67);
#127= CARTESIAN_POINT('12', (0., -3., 2.));
#129= NODE('12', (#127), #36, #67);
#131= CARTESIAN_POINT('13', (0., -2., 2.));
#133= NODE('13', (#131), #36, #67);

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#135= CARTESIAN_POINT('14', (0.,-1.,2.));
#137= NODE('14', (#135), #36, #67);
#139= CARTESIAN_POINT('15', (0.,-6.013760000000000E-9,2.));
#141= NODE('15', (#139), #36, #67);
#143= CARTESIAN_POINT('16', (1.,-4.,-2.535450000000000E-8));
#145= NODE('16', (#143), #36, #67);
#147= CARTESIAN_POINT('17', (1.,-3.,-2.090090000000000E-8));
#149= NODE('17', (#147), #36, #67);
#151= CARTESIAN_POINT('18', (1.,-2.,-3.742290000000000E-8));
#153= NODE('18', (#151), #36, #67);
#155= CARTESIAN_POINT('19', (1.,-1.,-5.394500000000000E-8));
#157= NODE('19', (#155), #36, #67);
#159= CARTESIAN_POINT('20', (1.,-2.864290000000000E-9,
-4.949130000000000E-8));
#161= NODE('20', (#159), #36, #67);
#163= CARTESIAN_POINT('21', (1.,-4.,1.));
#165= NODE('21', (#163), #36, #67);
#167= CARTESIAN_POINT('22', (1.,-3.,1.));
#169= NODE('22', (#167), #36, #67);
#171= CARTESIAN_POINT('23', (1.,-2.,1.));
#173= NODE('23', (#171), #36, #67);
#175= CARTESIAN_POINT('24', (1.,-1.,1.));
#177= NODE('24', (#175), #36, #67);
#179= CARTESIAN_POINT('25', (1.,-3.284170000000000E-9,1.));
#181= NODE('25', (#179), #36, #67);
#183= CARTESIAN_POINT('26', (1.,-4.,2.));
#185= NODE('26', (#183), #36, #67);
#187= CARTESIAN_POINT('27', (1.,-3.,2.));
#189= NODE('27', (#187), #36, #67);
#191= CARTESIAN_POINT('28', (1.,-2.,2.));
#193= NODE('28', (#191), #36, #67);
#195= CARTESIAN_POINT('29', (1.,-1.,2.));
#197= NODE('29', (#195), #36, #67);
#199= CARTESIAN_POINT('30', (1.,-3.704040000000000E-9,2.));
#201= NODE('30', (#199), #36, #67);
#203= CARTESIAN_POINT('31', (2.,-4.,-1.639380000000000E-8));
#205= NODE('31', (#203), #36, #67);
#207= CARTESIAN_POINT('32', (2.,-3.,-7.486510000000000E-9));
#209= NODE('32', (#207), #36, #67);
#211= CARTESIAN_POINT('33', (2.,-2.,-4.053060000000000E-8));
#213= NODE('33', (#211), #36, #67);
#215= CARTESIAN_POINT('34', (2.,-1.,-7.357470000000001E-8));
#217= NODE('34', (#215), #36, #67);
#219= CARTESIAN_POINT('35', (2.,2.851770000000000E-10,
-6.466740000000000E-8));
#221= NODE('35', (#219), #36, #67);
#223= CARTESIAN_POINT('36', (2.,-4.,1.));
#225= NODE('36', (#223), #36, #67);
#227= CARTESIAN_POINT('37', (2.,-3.,1.));
#229= NODE('37', (#227), #36, #67);
#231= CARTESIAN_POINT('38', (2.,-2.,1.));
#233= NODE('38', (#231), #36, #67);
#235= CARTESIAN_POINT('39', (2.,-1.,1.));
#237= NODE('39', (#235), #36, #67);
#239= CARTESIAN_POINT('40', (2.,-5.545730000000000E-10,1.));
#241= NODE('40', (#239), #36, #67);
#243= CARTESIAN_POINT('41', (2.,-4.,2.));
#245= NODE('41', (#243), #36, #67);
#247= CARTESIAN_POINT('42', (2.,-3.,2.));
#249= NODE('42', (#247), #36, #67);
#251= CARTESIAN_POINT('43', (2.,-2.,2.));
#253= NODE('43', (#251), #36, #67);
#255= CARTESIAN_POINT('44', (2.,-1.,2.));
#257= NODE('44', (#255), #36, #67);
#259= CARTESIAN_POINT('45', (2.,-1.394320000000000E-9,2.));
#261= NODE('45', (#259), #36, #67);
#263= CARTESIAN_POINT('46', (3.,-4.,-7.433150000000000E-9));
#265= NODE('46', (#263), #36, #67);
#267= CARTESIAN_POINT('47', (3.,-3.,5.927840000000000E-9));
#269= NODE('47', (#267), #36, #67);
#271= CARTESIAN_POINT('48', (3.,-2.,-4.363830000000000E-8));

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#273= NODE('48', (#271), #36, #67);
#275= CARTESIAN_POINT('49', (3., -1., -9.3204500000000001E-8));
#277= NODE('49', (#275), #36, #67);
#279= CARTESIAN_POINT('50', (3., 3.4346500000000000E-9,
-7.9843500000000000E-8));
#281= NODE('50', (#279), #36, #67);
#283= CARTESIAN_POINT('51', (3., -4., 1.));
#285= NODE('51', (#283), #36, #67);
#287= CARTESIAN_POINT('52', (3., -3., 1.));
#289= NODE('52', (#287), #36, #67);
#291= CARTESIAN_POINT('53', (3., -2., 1.));
#293= NODE('53', (#291), #36, #67);
#295= CARTESIAN_POINT('54', (3., -1., 1.));
#297= NODE('54', (#295), #36, #67);
#299= CARTESIAN_POINT('55', (3., 2.1750200000000000E-9, 1.));
#301= NODE('55', (#299), #36, #67);
#303= CARTESIAN_POINT('56', (3., -4., 2.));
#305= NODE('56', (#303), #36, #67);
#307= CARTESIAN_POINT('57', (3., -3., 2.));
#309= NODE('57', (#307), #36, #67);
#311= CARTESIAN_POINT('58', (3., -2., 2.));
#313= NODE('58', (#311), #36, #67);
#315= CARTESIAN_POINT('59', (3., -1., 2.));
#317= NODE('59', (#315), #36, #67);
#319= CARTESIAN_POINT('60', (3., 9.1540000000000000E-10, 2.));
#321= NODE('60', (#319), #36, #67);
#323= CARTESIAN_POINT('61', (4., -4., 1.5275300000000000E-9));
#325= NODE('61', (#323), #36, #67);
#327= CARTESIAN_POINT('62', (4., -3., 1.9342200000000000E-8));
#329= NODE('62', (#327), #36, #67);
#331= CARTESIAN_POINT('63', (4., -2., -4.6746000000000000E-8));
#333= NODE('63', (#331), #36, #67);
#335= CARTESIAN_POINT('64', (4., -1., -1.1283400000000000E-7));
#337= NODE('64', (#335), #36, #67);
#339= CARTESIAN_POINT('65', (4., 6.5841200000000000E-9,
-9.5019600000000001E-8));
#341= NODE('65', (#339), #36, #67);
#343= CARTESIAN_POINT('66', (4., -4., 1.));
#345= NODE('66', (#343), #36, #67);
#347= CARTESIAN_POINT('67', (4., -3., 1.));
#349= NODE('67', (#347), #36, #67);
#351= CARTESIAN_POINT('68', (4., -2., 1.));
#353= NODE('68', (#351), #36, #67);
#355= CARTESIAN_POINT('69', (4., -1., 1.));
#357= NODE('69', (#355), #36, #67);
#359= CARTESIAN_POINT('70', (4., 4.9046200000000000E-9, 1.));
#361= NODE('70', (#359), #36, #67);
#363= CARTESIAN_POINT('71', (4., -4., 2.));
#365= NODE('71', (#363), #36, #67);
#367= CARTESIAN_POINT('72', (4., -3., 2.));
#369= NODE('72', (#367), #36, #67);
#371= CARTESIAN_POINT('73', (4., -2., 2.));
#373= NODE('73', (#371), #36, #67);
#375= CARTESIAN_POINT('74', (4., -1., 2.));
#377= NODE('74', (#375), #36, #67);
#379= CARTESIAN_POINT('75', (4., 3.2251200000000000E-9, 2.));
#381= NODE('75', (#379), #36, #67);
#383= CARTESIAN_POINT('76', (10., -5.2757700000000000E-8, 0.));
#385= NODE('76', (#383), #36, #67);
#387= CARTESIAN_POINT('77', (9., -5.2757700000000000E-8, 0.));
#389= NODE('77', (#387), #36, #67);
#391= CARTESIAN_POINT('78', (8., -5.2757700000000000E-8, 0.));
#393= NODE('78', (#391), #36, #67);
#395= CARTESIAN_POINT('79', (7., -5.2757700000000000E-8, 0.));
#397= NODE('79', (#395), #36, #67);
#399= CARTESIAN_POINT('80', (6., -5.2757700000000000E-8, 0.));
#401= NODE('80', (#399), #36, #67);
#403= CARTESIAN_POINT('81', (5., -5.2757700000000000E-8, 0.));
#405= NODE('81', (#403), #36, #67);
#407= CARTESIAN_POINT('83', (10., -1., 0.));
#409= NODE('83', (#407), #36, #67);

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#411= CARTESIAN_POINT('84', (9.,-1.,0.));
#413= NODE('84', (#411), #36, #67);
#415= CARTESIAN_POINT('85', (8.,-1.,0.));
#417= NODE('85', (#415), #36, #67);
#419= CARTESIAN_POINT('86', (7.,-1.,0.));
#421= NODE('86', (#419), #36, #67);
#423= CARTESIAN_POINT('87', (6.,-1.,0.));
#425= NODE('87', (#423), #36, #67);
#427= CARTESIAN_POINT('88', (5.,-1.,0.));
#429= NODE('88', (#427), #36, #67);
#431= CARTESIAN_POINT('90', (10.,-2.,0.));
#433= NODE('90', (#431), #36, #67);
#435= CARTESIAN_POINT('91', (9.,-2.,0.));
#437= NODE('91', (#435), #36, #67);
#439= CARTESIAN_POINT('92', (8.,-2.,0.));
#441= NODE('92', (#439), #36, #67);
#443= CARTESIAN_POINT('93', (7.,-2.,0.));
#445= NODE('93', (#443), #36, #67);
#447= CARTESIAN_POINT('94', (6.,-2.,0.));
#449= NODE('94', (#447), #36, #67);
#451= CARTESIAN_POINT('95', (5.,-2.,0.));
#453= NODE('95', (#451), #36, #67);
#455= CARTESIAN_POINT('97', (10.,-3.,0.));
#457= NODE('97', (#455), #36, #67);
#459= CARTESIAN_POINT('98', (9.,-3.,0.));
#461= NODE('98', (#459), #36, #67);
#463= CARTESIAN_POINT('99', (8.,-3.,0.));
#465= NODE('99', (#463), #36, #67);
#467= CARTESIAN_POINT('100', (7.,-3.,0.));
#469= NODE('100', (#467), #36, #67);
#471= CARTESIAN_POINT('101', (6.,-3.,0.));
#473= NODE('101', (#471), #36, #67);
#475= CARTESIAN_POINT('102', (5.,-3.,0.));
#477= NODE('102', (#475), #36, #67);
#479= CARTESIAN_POINT('104', (10.,-4.,0.));
#481= NODE('104', (#479), #36, #67);
#483= CARTESIAN_POINT('105', (9.,-4.,0.));
#485= NODE('105', (#483), #36, #67);
#487= CARTESIAN_POINT('106', (8.,-4.,0.));
#489= NODE('106', (#487), #36, #67);
#491= CARTESIAN_POINT('107', (7.,-4.,0.));
#493= NODE('107', (#491), #36, #67);
#495= CARTESIAN_POINT('108', (6.,-4.,0.));
#497= NODE('108', (#495), #36, #67);
#499= CARTESIAN_POINT('109', (5.,-4.,0.));
#501= NODE('109', (#499), #36, #67);
#503= CARTESIAN_POINT('111', (10.,-5.275770000000000E-8,1.));
#505= NODE('111', (#503), #36, #67);
#507= CARTESIAN_POINT('112', (9.,-5.275770000000000E-8,1.));
#509= NODE('112', (#507), #36, #67);
#511= CARTESIAN_POINT('113', (8.,-5.275770000000000E-8,1.));
#513= NODE('113', (#511), #36, #67);
#515= CARTESIAN_POINT('114', (7.,-5.275770000000000E-8,1.));
#517= NODE('114', (#515), #36, #67);
#519= CARTESIAN_POINT('115', (6.,-5.275770000000000E-8,1.));
#521= NODE('115', (#519), #36, #67);
#523= CARTESIAN_POINT('116', (5.,-5.275770000000000E-8,1.));
#525= NODE('116', (#523), #36, #67);
#527= CARTESIAN_POINT('118', (10.,-1.,1.));
#529= NODE('118', (#527), #36, #67);
#531= CARTESIAN_POINT('119', (9.,-1.,1.));
#533= NODE('119', (#531), #36, #67);
#535= CARTESIAN_POINT('120', (8.,-1.,1.));
#537= NODE('120', (#535), #36, #67);
#539= CARTESIAN_POINT('121', (7.,-1.,1.));
#541= NODE('121', (#539), #36, #67);
#543= CARTESIAN_POINT('122', (6.,-1.,1.));
#545= NODE('122', (#543), #36, #67);
#547= CARTESIAN_POINT('123', (5.,-1.,1.));
#549= NODE('123', (#547), #36, #67);
#551= CARTESIAN_POINT('125', (10.,-2.,1.));

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#553= NODE('125', (#551), #36, #67);
#555= CARTESIAN_POINT('126', (9., -2., 1.));
#557= NODE('126', (#555), #36, #67);
#559= CARTESIAN_POINT('127', (8., -2., 1.));
#561= NODE('127', (#559), #36, #67);
#563= CARTESIAN_POINT('128', (7., -2., 1.));
#565= NODE('128', (#563), #36, #67);
#567= CARTESIAN_POINT('129', (6., -2., 1.));
#569= NODE('129', (#567), #36, #67);
#571= CARTESIAN_POINT('130', (5., -2., 1.));
#573= NODE('130', (#571), #36, #67);
#575= CARTESIAN_POINT('132', (10., -3., 1.));
#577= NODE('132', (#575), #36, #67);
#579= CARTESIAN_POINT('133', (9., -3., 1.));
#581= NODE('133', (#579), #36, #67);
#583= CARTESIAN_POINT('134', (8., -3., 1.));
#585= NODE('134', (#583), #36, #67);
#587= CARTESIAN_POINT('135', (7., -3., 1.));
#589= NODE('135', (#587), #36, #67);
#591= CARTESIAN_POINT('136', (6., -3., 1.));
#593= NODE('136', (#591), #36, #67);
#595= CARTESIAN_POINT('137', (5., -3., 1.));
#597= NODE('137', (#595), #36, #67);
#599= CARTESIAN_POINT('139', (10., -4., 1.));
#601= NODE('139', (#599), #36, #67);
#603= CARTESIAN_POINT('140', (9., -4., 1.));
#605= NODE('140', (#603), #36, #67);
#607= CARTESIAN_POINT('141', (8., -4., 1.));
#609= NODE('141', (#607), #36, #67);
#611= CARTESIAN_POINT('142', (7., -4., 1.));
#613= NODE('142', (#611), #36, #67);
#615= CARTESIAN_POINT('143', (6., -4., 1.));
#617= NODE('143', (#615), #36, #67);
#619= CARTESIAN_POINT('144', (5., -4., 1.));
#621= NODE('144', (#619), #36, #67);
#623= CARTESIAN_POINT('146', (10., -5.2757700000000000E-8, 2.));
#625= NODE('146', (#623), #36, #67);
#627= CARTESIAN_POINT('147', (9., -5.2757700000000000E-8, 2.));
#629= NODE('147', (#627), #36, #67);
#631= CARTESIAN_POINT('148', (8., -5.2757700000000000E-8, 2.));
#633= NODE('148', (#631), #36, #67);
#635= CARTESIAN_POINT('149', (7., -5.2757700000000000E-8, 2.));
#637= NODE('149', (#635), #36, #67);
#639= CARTESIAN_POINT('150', (6., -5.2757700000000000E-8, 2.));
#641= NODE('150', (#639), #36, #67);
#643= CARTESIAN_POINT('151', (5., -5.2757700000000000E-8, 2.));
#645= NODE('151', (#643), #36, #67);
#647= CARTESIAN_POINT('153', (10., -1., 2.));
#649= NODE('153', (#647), #36, #67);
#651= CARTESIAN_POINT('154', (9., -1., 2.));
#653= NODE('154', (#651), #36, #67);
#655= CARTESIAN_POINT('155', (8., -1., 2.));
#657= NODE('155', (#655), #36, #67);
#659= CARTESIAN_POINT('156', (7., -1., 2.));
#661= NODE('156', (#659), #36, #67);
#663= CARTESIAN_POINT('157', (6., -1., 2.));
#665= NODE('157', (#663), #36, #67);
#667= CARTESIAN_POINT('158', (5., -1., 2.));
#669= NODE('158', (#667), #36, #67);
#671= CARTESIAN_POINT('160', (10., -2., 2.));
#673= NODE('160', (#671), #36, #67);
#675= CARTESIAN_POINT('161', (9., -2., 2.));
#677= NODE('161', (#675), #36, #67);
#679= CARTESIAN_POINT('162', (8., -2., 2.));
#681= NODE('162', (#679), #36, #67);
#683= CARTESIAN_POINT('163', (7., -2., 2.));
#685= NODE('163', (#683), #36, #67);
#687= CARTESIAN_POINT('164', (6., -2., 2.));
#689= NODE('164', (#687), #36, #67);
#691= CARTESIAN_POINT('165', (5., -2., 2.));
#693= NODE('165', (#691), #36, #67);

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#695= CARTESIAN_POINT('167', (10., -3., 2.));
#697= NODE('167', (#695), #36, #67);
#699= CARTESIAN_POINT('168', (9., -3., 2.));
#701= NODE('168', (#699), #36, #67);
#703= CARTESIAN_POINT('169', (8., -3., 2.));
#705= NODE('169', (#703), #36, #67);
#707= CARTESIAN_POINT('170', (7., -3., 2.));
#709= NODE('170', (#707), #36, #67);
#711= CARTESIAN_POINT('171', (6., -3., 2.));
#713= NODE('171', (#711), #36, #67);
#715= CARTESIAN_POINT('172', (5., -3., 2.));
#717= NODE('172', (#715), #36, #67);
#719= CARTESIAN_POINT('174', (10., -4., 2.));
#721= NODE('174', (#719), #36, #67);
#723= CARTESIAN_POINT('175', (9., -4., 2.));
#725= NODE('175', (#723), #36, #67);
#727= CARTESIAN_POINT('176', (8., -4., 2.));
#729= NODE('176', (#727), #36, #67);
#731= CARTESIAN_POINT('177', (7., -4., 2.));
#733= NODE('177', (#731), #36, #67);
#735= CARTESIAN_POINT('178', (6., -4., 2.));
#737= NODE('178', (#735), #36, #67);
#739= CARTESIAN_POINT('179', (5., -4., 2.));
#741= NODE('179', (#739), #36, #67);
#743= CARTESIAN_POINT('181', (16., -5.275770000000000E-8, 0.));
#745= NODE('181', (#743), #36, #67);
#747= CARTESIAN_POINT('182', (15., -5.275770000000000E-8, 0.));
#749= NODE('182', (#747), #36, #67);
#751= CARTESIAN_POINT('183', (14., -5.275770000000000E-8, 0.));
#753= NODE('183', (#751), #36, #67);
#755= CARTESIAN_POINT('184', (13., -5.275770000000000E-8, 0.));
#757= NODE('184', (#755), #36, #67);
#759= CARTESIAN_POINT('185', (12., -5.275770000000000E-8, 0.));
#761= NODE('185', (#759), #36, #67);
#763= CARTESIAN_POINT('186', (11., -5.275770000000000E-8, 0.));
#765= NODE('186', (#763), #36, #67);
#767= CARTESIAN_POINT('188', (16., -1., 0.));
#769= NODE('188', (#767), #36, #67);
#771= CARTESIAN_POINT('189', (15., -1., 0.));
#773= NODE('189', (#771), #36, #67);
#775= CARTESIAN_POINT('190', (14., -1., 0.));
#777= NODE('190', (#775), #36, #67);
#779= CARTESIAN_POINT('191', (13., -1., 0.));
#781= NODE('191', (#779), #36, #67);
#783= CARTESIAN_POINT('192', (12., -1., 0.));
#785= NODE('192', (#783), #36, #67);
#787= CARTESIAN_POINT('193', (11., -1., 0.));
#789= NODE('193', (#787), #36, #67);
#791= CARTESIAN_POINT('195', (16., -2., 0.));
#793= NODE('195', (#791), #36, #67);
#795= CARTESIAN_POINT('196', (15., -2., 0.));
#797= NODE('196', (#795), #36, #67);
#799= CARTESIAN_POINT('197', (14., -2., 0.));
#801= NODE('197', (#799), #36, #67);
#803= CARTESIAN_POINT('198', (13., -2., 0.));
#805= NODE('198', (#803), #36, #67);
#807= CARTESIAN_POINT('199', (12., -2., 0.));
#809= NODE('199', (#807), #36, #67);
#811= CARTESIAN_POINT('200', (11., -2., 0.));
#813= NODE('200', (#811), #36, #67);
#815= CARTESIAN_POINT('202', (16., -3., 0.));
#817= NODE('202', (#815), #36, #67);
#819= CARTESIAN_POINT('203', (15., -3., 0.));
#821= NODE('203', (#819), #36, #67);
#823= CARTESIAN_POINT('204', (14., -3., 0.));
#825= NODE('204', (#823), #36, #67);
#827= CARTESIAN_POINT('205', (13., -3., 0.));
#829= NODE('205', (#827), #36, #67);
#831= CARTESIAN_POINT('206', (12., -3., 0.));
#833= NODE('206', (#831), #36, #67);
#835= CARTESIAN_POINT('207', (11., -3., 0.));

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#837= NODE('207', (#835), #36, #67);
#839= CARTESIAN_POINT('209', (16., -4., 0.));
#841= NODE('209', (#839), #36, #67);
#843= CARTESIAN_POINT('210', (15., -4., 0.));
#845= NODE('210', (#843), #36, #67);
#847= CARTESIAN_POINT('211', (14., -4., 0.));
#849= NODE('211', (#847), #36, #67);
#851= CARTESIAN_POINT('212', (13., -4., 0.));
#853= NODE('212', (#851), #36, #67);
#855= CARTESIAN_POINT('213', (12., -4., 0.));
#857= NODE('213', (#855), #36, #67);
#859= CARTESIAN_POINT('214', (11., -4., 0.));
#861= NODE('214', (#859), #36, #67);
#863= CARTESIAN_POINT('216', (16., -5.275770000000000E-8, 1.));
#865= NODE('216', (#863), #36, #67);
#867= CARTESIAN_POINT('217', (15., -5.275770000000000E-8, 1.));
#869= NODE('217', (#867), #36, #67);
#871= CARTESIAN_POINT('218', (14., -5.275770000000000E-8, 1.));
#873= NODE('218', (#871), #36, #67);
#875= CARTESIAN_POINT('219', (13., -5.275770000000000E-8, 1.));
#877= NODE('219', (#875), #36, #67);
#879= CARTESIAN_POINT('220', (12., -5.275770000000000E-8, 1.));
#881= NODE('220', (#879), #36, #67);
#883= CARTESIAN_POINT('221', (11., -5.275770000000000E-8, 1.));
#885= NODE('221', (#883), #36, #67);
#887= CARTESIAN_POINT('223', (16., -1., 1.));
#889= NODE('223', (#887), #36, #67);
#891= CARTESIAN_POINT('224', (15., -1., 1.));
#893= NODE('224', (#891), #36, #67);
#895= CARTESIAN_POINT('225', (14., -1., 1.));
#897= NODE('225', (#895), #36, #67);
#899= CARTESIAN_POINT('226', (13., -1., 1.));
#901= NODE('226', (#899), #36, #67);
#903= CARTESIAN_POINT('227', (12., -1., 1.));
#905= NODE('227', (#903), #36, #67);
#907= CARTESIAN_POINT('228', (11., -1., 1.));
#909= NODE('228', (#907), #36, #67);
#911= CARTESIAN_POINT('230', (16., -2., 1.));
#913= NODE('230', (#911), #36, #67);
#915= CARTESIAN_POINT('231', (15., -2., 1.));
#917= NODE('231', (#915), #36, #67);
#919= CARTESIAN_POINT('232', (14., -2., 1.));
#921= NODE('232', (#919), #36, #67);
#923= CARTESIAN_POINT('233', (13., -2., 1.));
#925= NODE('233', (#923), #36, #67);
#927= CARTESIAN_POINT('234', (12., -2., 1.));
#929= NODE('234', (#927), #36, #67);
#931= CARTESIAN_POINT('235', (11., -2., 1.));
#933= NODE('235', (#931), #36, #67);
#935= CARTESIAN_POINT('237', (16., -3., 1.));
#937= NODE('237', (#935), #36, #67);
#939= CARTESIAN_POINT('238', (15., -3., 1.));
#941= NODE('238', (#939), #36, #67);
#943= CARTESIAN_POINT('239', (14., -3., 1.));
#945= NODE('239', (#943), #36, #67);
#947= CARTESIAN_POINT('240', (13., -3., 1.));
#949= NODE('240', (#947), #36, #67);
#951= CARTESIAN_POINT('241', (12., -3., 1.));
#953= NODE('241', (#951), #36, #67);
#955= CARTESIAN_POINT('242', (11., -3., 1.));
#957= NODE('242', (#955), #36, #67);
#959= CARTESIAN_POINT('244', (16., -4., 1.));
#961= NODE('244', (#959), #36, #67);
#963= CARTESIAN_POINT('245', (15., -4., 1.));
#965= NODE('245', (#963), #36, #67);
#967= CARTESIAN_POINT('246', (14., -4., 1.));
#969= NODE('246', (#967), #36, #67);
#971= CARTESIAN_POINT('247', (13., -4., 1.));
#973= NODE('247', (#971), #36, #67);
#975= CARTESIAN_POINT('248', (12., -4., 1.));
#977= NODE('248', (#975), #36, #67);

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#979= CARTESIAN_POINT('249', (11., -4., 1.));
#981= NODE('249', (#979), #36, #67);
#983= CARTESIAN_POINT('251', (16., -5.2757700000000000E-8, 2.));
#985= NODE('251', (#983), #36, #67);
#987= CARTESIAN_POINT('252', (15., -5.2757700000000000E-8, 2.));
#989= NODE('252', (#987), #36, #67);
#991= CARTESIAN_POINT('253', (14., -5.2757700000000000E-8, 2.));
#993= NODE('253', (#991), #36, #67);
#995= CARTESIAN_POINT('254', (13., -5.2757700000000000E-8, 2.));
#997= NODE('254', (#995), #36, #67);
#999= CARTESIAN_POINT('255', (12., -5.2757700000000000E-8, 2.));
#1001= NODE('255', (#999), #36, #67);
#1003= CARTESIAN_POINT('256', (11., -5.2757700000000000E-8, 2.));
#1005= NODE('256', (#1003), #36, #67);
#1007= CARTESIAN_POINT('258', (16., -1., 2.));
#1009= NODE('258', (#1007), #36, #67);
#1011= CARTESIAN_POINT('259', (15., -1., 2.));
#1013= NODE('259', (#1011), #36, #67);
#1015= CARTESIAN_POINT('260', (14., -1., 2.));
#1017= NODE('260', (#1015), #36, #67);
#1019= CARTESIAN_POINT('261', (13., -1., 2.));
#1021= NODE('261', (#1019), #36, #67);
#1023= CARTESIAN_POINT('262', (12., -1., 2.));
#1025= NODE('262', (#1023), #36, #67);
#1027= CARTESIAN_POINT('263', (11., -1., 2.));
#1029= NODE('263', (#1027), #36, #67);
#1031= CARTESIAN_POINT('265', (16., -2., 2.));
#1033= NODE('265', (#1031), #36, #67);
#1035= CARTESIAN_POINT('266', (15., -2., 2.));
#1037= NODE('266', (#1035), #36, #67);
#1039= CARTESIAN_POINT('267', (14., -2., 2.));
#1041= NODE('267', (#1039), #36, #67);
#1043= CARTESIAN_POINT('268', (13., -2., 2.));
#1045= NODE('268', (#1043), #36, #67);
#1047= CARTESIAN_POINT('269', (12., -2., 2.));
#1049= NODE('269', (#1047), #36, #67);
#1051= CARTESIAN_POINT('270', (11., -2., 2.));
#1053= NODE('270', (#1051), #36, #67);
#1055= CARTESIAN_POINT('272', (16., -3., 2.));
#1057= NODE('272', (#1055), #36, #67);
#1059= CARTESIAN_POINT('273', (15., -3., 2.));
#1061= NODE('273', (#1059), #36, #67);
#1063= CARTESIAN_POINT('274', (14., -3., 2.));
#1065= NODE('274', (#1063), #36, #67);
#1067= CARTESIAN_POINT('275', (13., -3., 2.));
#1069= NODE('275', (#1067), #36, #67);
#1071= CARTESIAN_POINT('276', (12., -3., 2.));
#1073= NODE('276', (#1071), #36, #67);
#1075= CARTESIAN_POINT('277', (11., -3., 2.));
#1077= NODE('277', (#1075), #36, #67);
#1079= CARTESIAN_POINT('279', (16., -4., 2.));
#1081= NODE('279', (#1079), #36, #67);
#1083= CARTESIAN_POINT('280', (15., -4., 2.));
#1085= NODE('280', (#1083), #36, #67);
#1087= CARTESIAN_POINT('281', (14., -4., 2.));
#1089= NODE('281', (#1087), #36, #67);
#1091= CARTESIAN_POINT('282', (13., -4., 2.));
#1093= NODE('282', (#1091), #36, #67);
#1095= CARTESIAN_POINT('283', (12., -4., 2.));
#1097= NODE('283', (#1095), #36, #67);
#1099= CARTESIAN_POINT('284', (11., -4., 2.));
#1101= NODE('284', (#1099), #36, #67);
#1103= ELEMENT_MATERIAL('MAT1.1', 'Fea Material', (#1115, #1123, #1129));
#1104= MEASURE_REPRESENTATION_ITEM('representation_item_name_1',
THERMODYNAMIC_TEMPERATURE_MEASURE(70.), #10);
#1105= PROPERTY_DEFINITION_REPRESENTATION(#1106, #1108);
#1106= PROPERTY_DEFINITION('Material Property Definition', $, #1107);
#1107= CHARACTERIZED_OBJECT('property', $);
#1108= REPRESENTATION('representation_id_1', (#1104), #36);
#1109= ID_ATTRIBUTE('MAT1.1', #1106);
#1111= DATA_ENVIRONMENT('DATA ENV', 'Property conditions', (#1105));

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#1113= FEA_LINEAR_ELASTICITY('',FEA_ISOTROPIC_SYMMETRIC_TENSOR4_3D((
10000000.,0.33)));
#1115= FEA_MATERIAL_PROPERTY_REPRESENTATION(#1116,#1118,#1111);
#1116= MATERIAL_PROPERTY('MAT1.1.0',$,#1117);
#1117= CHARACTERIZED_OBJECT('material_property',$);
#1118= REPRESENTATION('representation_id_2',(#1113),#36);
#1119= DESCRIPTION_ATTRIBUTE('Elasticity',#1115);
#1122= FEA_MASS_DENSITY('',0.000254);
#1123= FEA_MATERIAL_PROPERTY_REPRESENTATION(#1124,#1125,#1111);
#1124= MATERIAL_PROPERTY('MAT1.1.1',$,#1117);
#1125= REPRESENTATION('representation_id_3',(#1122),#36);
#1126= DESCRIPTION_ATTRIBUTE('MassDensity',#1123);
#1128= FEA_TANGENTIAL_COEFFICIENT_OF_LINEAR_THERMAL_EXPANSION('',
ISOTROPIC_SYMMETRIC_TENSOR2_3D(0.));
#1129= FEA_MATERIAL_PROPERTY_REPRESENTATION(#1130,#1131,#1111);
#1130= MATERIAL_PROPERTY('MAT1.1.2',$,#1117);
#1131= REPRESENTATION('representation_id_4',(#1128),#36);
#1132= DESCRIPTION_ATTRIBUTE('TangentCTE',#1129);
#1134= VOLUME_3D_ELEMENT_REPRESENTATION('1',(#1143),#1135,(#80,#89,#109,
#105,#145,#149,#169,#165),#67,#1145,#1103);
#1135=
/* GEOMETRIC REPRESENTATION CONTEXT+PARAMETRIC REPRESENTATION CONTEXT */
(GEOMETRIC_REPRESENTATION_CONTEXT(3)PARAMETRIC_REPRESENTATION_CONTEXT()
REPRESENTATION_CONTEXT('REP_CONTEXT_FEA','3D'));
#1137= REPRESENTATION('Default SimDM Fea representation',(#1139),#1135);
#1139= REPRESENTATION_ITEM('Default SimDM item');
#1140= ID_ATTRIBUTE('Default SimDM Fea representation',#1137);
#1141= DESCRIPTION_ATTRIBUTE('Default SimDM Fea representation',#1137);
#1143= ARBITRARY_VOLUME_3D_ELEMENT_COORDINATE_SYSTEM('',#35);
#1145= VOLUME_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER.,
'LINEAR_HEXAHEDRON.CHEXA',(ENUMERATED_VOLUME_ELEMENT_PURPOSE(
.STRESS_DISPLACEMENT.)),.HEXAHEDRON.);
#1147= VOLUME_3D_ELEMENT_REPRESENTATION('2',(#1143),#1135,(#89,#93,#113,
#109,#149,#153,#173,#169),#67,#1145,#1103);
#1150= VOLUME_3D_ELEMENT_REPRESENTATION('3',(#1143),#1135,(#93,#97,#117,
#113,#153,#157,#177,#173),#67,#1145,#1103);
#1153= VOLUME_3D_ELEMENT_REPRESENTATION('4',(#1143),#1135,(#97,#101,#121,
#117,#157,#161,#181,#177),#67,#1145,#1103);
#1156= VOLUME_3D_ELEMENT_REPRESENTATION('5',(#1143),#1135,(#105,#109,
#129,#125,#165,#169,#189,#185),#67,#1145,#1103);
#1159= VOLUME_3D_ELEMENT_REPRESENTATION('6',(#1143),#1135,(#109,#113,
#133,#129,#169,#173,#193,#189),#67,#1145,#1103);
#1162= VOLUME_3D_ELEMENT_REPRESENTATION('7',(#1143),#1135,(#113,#117,
#137,#133,#173,#177,#197,#193),#67,#1145,#1103);
#1165= VOLUME_3D_ELEMENT_REPRESENTATION('8',(#1143),#1135,(#117,#121,
#141,#137,#177,#181,#201,#197),#67,#1145,#1103);
#1168= VOLUME_3D_ELEMENT_REPRESENTATION('9',(#1143),#1135,(#145,#149,
#169,#165,#205,#209,#229,#225),#67,#1145,#1103);
#1171= VOLUME_3D_ELEMENT_REPRESENTATION('10',(#1143),#1135,(#149,#153,
#173,#169,#209,#213,#233,#229),#67,#1145,#1103);
#1174= VOLUME_3D_ELEMENT_REPRESENTATION('11',(#1143),#1135,(#153,#157,
#177,#173,#213,#217,#237,#233),#67,#1145,#1103);
#1177= VOLUME_3D_ELEMENT_REPRESENTATION('12',(#1143),#1135,(#157,#161,
#181,#177,#217,#221,#241,#237),#67,#1145,#1103);
#1180= VOLUME_3D_ELEMENT_REPRESENTATION('13',(#1143),#1135,(#165,#169,
#189,#185,#225,#229,#249,#245),#67,#1145,#1103);
#1183= VOLUME_3D_ELEMENT_REPRESENTATION('14',(#1143),#1135,(#169,#173,
#193,#189,#229,#233,#253,#249),#67,#1145,#1103);
#1186= VOLUME_3D_ELEMENT_REPRESENTATION('15',(#1143),#1135,(#173,#177,
#197,#193,#233,#237,#257,#253),#67,#1145,#1103);
#1189= VOLUME_3D_ELEMENT_REPRESENTATION('16',(#1143),#1135,(#177,#181,
#201,#197,#237,#241,#261,#257),#67,#1145,#1103);
#1192= VOLUME_3D_ELEMENT_REPRESENTATION('17',(#1143),#1135,(#205,#209,
#229,#225,#265,#269,#289,#285),#67,#1145,#1103);
#1195= VOLUME_3D_ELEMENT_REPRESENTATION('18',(#1143),#1135,(#209,#213,
#233,#229,#269,#273,#293,#289),#67,#1145,#1103);
#1198= VOLUME_3D_ELEMENT_REPRESENTATION('19',(#1143),#1135,(#213,#217,
#237,#233,#273,#277,#297,#293),#67,#1145,#1103);
#1201= VOLUME_3D_ELEMENT_REPRESENTATION('20',(#1143),#1135,(#217,#221,
#241,#237,#277,#281,#301,#297),#67,#1145,#1103);
#1204= VOLUME_3D_ELEMENT_REPRESENTATION('21',(#1143),#1135,(#225,#229,

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#249,#245,#285,#289,#309,#305),#67,#1145,#1103);
#1207= VOLUME_3D_ELEMENT_REPRESENTATION('22',(#1143),#1135,(#229,#233,
#253,#249,#289,#293,#313,#309),#67,#1145,#1103);
#1210= VOLUME_3D_ELEMENT_REPRESENTATION('23',(#1143),#1135,(#233,#237,
#257,#253,#293,#297,#317,#313),#67,#1145,#1103);
#1213= VOLUME_3D_ELEMENT_REPRESENTATION('24',(#1143),#1135,(#237,#241,
#261,#257,#297,#301,#321,#317),#67,#1145,#1103);
#1216= VOLUME_3D_ELEMENT_REPRESENTATION('25',(#1143),#1135,(#265,#269,
#289,#285,#325,#329,#349,#345),#67,#1145,#1103);
#1219= VOLUME_3D_ELEMENT_REPRESENTATION('26',(#1143),#1135,(#269,#273,
#293,#289,#329,#333,#353,#349),#67,#1145,#1103);
#1222= VOLUME_3D_ELEMENT_REPRESENTATION('27',(#1143),#1135,(#273,#277,
#297,#293,#333,#337,#357,#353),#67,#1145,#1103);
#1225= VOLUME_3D_ELEMENT_REPRESENTATION('28',(#1143),#1135,(#277,#281,
#301,#297,#337,#341,#361,#357),#67,#1145,#1103);
#1228= VOLUME_3D_ELEMENT_REPRESENTATION('29',(#1143),#1135,(#285,#289,
#309,#305,#345,#349,#369,#365),#67,#1145,#1103);
#1231= VOLUME_3D_ELEMENT_REPRESENTATION('30',(#1143),#1135,(#289,#293,
#313,#309,#349,#353,#373,#369),#67,#1145,#1103);
#1234= VOLUME_3D_ELEMENT_REPRESENTATION('31',(#1143),#1135,(#293,#297,
#317,#313,#353,#357,#377,#373),#67,#1145,#1103);
#1237= VOLUME_3D_ELEMENT_REPRESENTATION('32',(#1143),#1135,(#297,#301,
#321,#317,#357,#361,#381,#377),#67,#1145,#1103);
#1240= VOLUME_3D_ELEMENT_REPRESENTATION('33',(#1143),#1135,(#385,#409,
#505,#389),#67,#1243,#1103);
#1243= VOLUME_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER.,
'LINEAR_TETRAHEDRON.CTETRA',(ENUMERATED_VOLUME_ELEMENT_PURPOSE(
.STRESS_DISPLACEMENT.)),.TETRAHEDRON.);
#1245= VOLUME_3D_ELEMENT_REPRESENTATION('34',(#1143),#1135,(#529,#505,
#409,#533),#67,#1243,#1103);
#1248= VOLUME_3D_ELEMENT_REPRESENTATION('35',(#1143),#1135,(#413,#389,
#533,#409),#67,#1243,#1103);
#1251= VOLUME_3D_ELEMENT_REPRESENTATION('36',(#1143),#1135,(#509,#533,
#389,#505),#67,#1243,#1103);
#1254= VOLUME_3D_ELEMENT_REPRESENTATION('37',(#1143),#1135,(#389,#409,
#505,#533),#67,#1243,#1103);
#1257= VOLUME_3D_ELEMENT_REPRESENTATION('38',(#1143),#1135,(#413,#533,
#389,#417),#67,#1243,#1103);
#1260= VOLUME_3D_ELEMENT_REPRESENTATION('39',(#1143),#1135,(#509,#389,
#533,#513),#67,#1243,#1103);
#1263= VOLUME_3D_ELEMENT_REPRESENTATION('40',(#1143),#1135,(#393,#513,
#417,#389),#67,#1243,#1103);
#1266= VOLUME_3D_ELEMENT_REPRESENTATION('41',(#1143),#1135,(#537,#417,
#513,#533),#67,#1243,#1103);
#1269= VOLUME_3D_ELEMENT_REPRESENTATION('42',(#1143),#1135,(#389,#417,
#533,#513),#67,#1243,#1103);
#1272= VOLUME_3D_ELEMENT_REPRESENTATION('43',(#1143),#1135,(#393,#417,
#513,#397),#67,#1243,#1103);
#1275= VOLUME_3D_ELEMENT_REPRESENTATION('44',(#1143),#1135,(#537,#513,
#417,#541),#67,#1243,#1103);
#1278= VOLUME_3D_ELEMENT_REPRESENTATION('45',(#1143),#1135,(#421,#397,
#541,#417),#67,#1243,#1103);
#1281= VOLUME_3D_ELEMENT_REPRESENTATION('46',(#1143),#1135,(#517,#541,
#397,#513),#67,#1243,#1103);
#1284= VOLUME_3D_ELEMENT_REPRESENTATION('47',(#1143),#1135,(#397,#417,
#513,#541),#67,#1243,#1103);
#1287= VOLUME_3D_ELEMENT_REPRESENTATION('48',(#1143),#1135,(#421,#541,
#397,#425),#67,#1243,#1103);
#1290= VOLUME_3D_ELEMENT_REPRESENTATION('49',(#1143),#1135,(#517,#397,
#541,#521),#67,#1243,#1103);
#1293= VOLUME_3D_ELEMENT_REPRESENTATION('50',(#1143),#1135,(#401,#521,
#425,#397),#67,#1243,#1103);
#1296= VOLUME_3D_ELEMENT_REPRESENTATION('51',(#1143),#1135,(#545,#425,
#521,#541),#67,#1243,#1103);
#1299= VOLUME_3D_ELEMENT_REPRESENTATION('52',(#1143),#1135,(#397,#425,
#541,#521),#67,#1243,#1103);
#1302= VOLUME_3D_ELEMENT_REPRESENTATION('53',(#1143),#1135,(#401,#425,
#521,#405),#67,#1243,#1103);
#1305= VOLUME_3D_ELEMENT_REPRESENTATION('54',(#1143),#1135,(#545,#521,
#425,#549),#67,#1243,#1103);
#1308= VOLUME_3D_ELEMENT_REPRESENTATION('55',(#1143),#1135,(#429,#405,

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#549,#425),#67,#1243,#1103);
#1311= VOLUME_3D_ELEMENT_REPRESENTATION('56',(#1143),#1135,(#525,#549,
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#1314= VOLUME_3D_ELEMENT_REPRESENTATION('57',(#1143),#1135,(#405,#425,
#521,#549),#67,#1243,#1103);
#1317= VOLUME_3D_ELEMENT_REPRESENTATION('58',(#1143),#1135,(#429,#549,
#405,#337),#67,#1243,#1103);
#1320= VOLUME_3D_ELEMENT_REPRESENTATION('59',(#1143),#1135,(#525,#405,
#549,#361),#67,#1243,#1103);
#1323= VOLUME_3D_ELEMENT_REPRESENTATION('60',(#1143),#1135,(#341,#361,
#337,#405),#67,#1243,#1103);
#1326= VOLUME_3D_ELEMENT_REPRESENTATION('61',(#1143),#1135,(#357,#337,
#361,#549),#67,#1243,#1103);
#1329= VOLUME_3D_ELEMENT_REPRESENTATION('62',(#1143),#1135,(#405,#337,
#549,#361),#67,#1243,#1103);
#1332= VOLUME_3D_ELEMENT_REPRESENTATION('63',(#1143),#1135,(#433,#553,
#409,#437),#67,#1243,#1103);
#1335= VOLUME_3D_ELEMENT_REPRESENTATION('64',(#1143),#1135,(#529,#409,
#553,#533),#67,#1243,#1103);
#1338= VOLUME_3D_ELEMENT_REPRESENTATION('65',(#1143),#1135,(#413,#533,
#437,#409),#67,#1243,#1103);
#1341= VOLUME_3D_ELEMENT_REPRESENTATION('66',(#1143),#1135,(#557,#437,
#533,#553),#67,#1243,#1103);
#1344= VOLUME_3D_ELEMENT_REPRESENTATION('67',(#1143),#1135,(#409,#437,
#553,#533),#67,#1243,#1103);
#1347= VOLUME_3D_ELEMENT_REPRESENTATION('68',(#1143),#1135,(#413,#437,
#533,#417),#67,#1243,#1103);
#1350= VOLUME_3D_ELEMENT_REPRESENTATION('69',(#1143),#1135,(#557,#533,
#437,#561),#67,#1243,#1103);
#1353= VOLUME_3D_ELEMENT_REPRESENTATION('70',(#1143),#1135,(#441,#417,
#561,#437),#67,#1243,#1103);
#1356= VOLUME_3D_ELEMENT_REPRESENTATION('71',(#1143),#1135,(#537,#561,
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#1359= VOLUME_3D_ELEMENT_REPRESENTATION('72',(#1143),#1135,(#417,#437,
#533,#561),#67,#1243,#1103);
#1362= VOLUME_3D_ELEMENT_REPRESENTATION('73',(#1143),#1135,(#441,#561,
#417,#445),#67,#1243,#1103);
#1365= VOLUME_3D_ELEMENT_REPRESENTATION('74',(#1143),#1135,(#537,#417,
#561,#541),#67,#1243,#1103);
#1368= VOLUME_3D_ELEMENT_REPRESENTATION('75',(#1143),#1135,(#421,#541,
#445,#417),#67,#1243,#1103);
#1371= VOLUME_3D_ELEMENT_REPRESENTATION('76',(#1143),#1135,(#565,#445,
#541,#561),#67,#1243,#1103);
#1374= VOLUME_3D_ELEMENT_REPRESENTATION('77',(#1143),#1135,(#417,#445,
#561,#541),#67,#1243,#1103);
#1377= VOLUME_3D_ELEMENT_REPRESENTATION('78',(#1143),#1135,(#421,#445,
#541,#425),#67,#1243,#1103);
#1380= VOLUME_3D_ELEMENT_REPRESENTATION('79',(#1143),#1135,(#565,#541,
#445,#569),#67,#1243,#1103);
#1383= VOLUME_3D_ELEMENT_REPRESENTATION('80',(#1143),#1135,(#449,#425,
#569,#445),#67,#1243,#1103);
#1386= VOLUME_3D_ELEMENT_REPRESENTATION('81',(#1143),#1135,(#545,#569,
#425,#541),#67,#1243,#1103);
#1389= VOLUME_3D_ELEMENT_REPRESENTATION('82',(#1143),#1135,(#425,#445,
#541,#569),#67,#1243,#1103);
#1392= VOLUME_3D_ELEMENT_REPRESENTATION('83',(#1143),#1135,(#449,#569,
#425,#453),#67,#1243,#1103);
#1395= VOLUME_3D_ELEMENT_REPRESENTATION('84',(#1143),#1135,(#545,#425,
#569,#549),#67,#1243,#1103);
#1398= VOLUME_3D_ELEMENT_REPRESENTATION('85',(#1143),#1135,(#429,#549,
#453,#425),#67,#1243,#1103);
#1401= VOLUME_3D_ELEMENT_REPRESENTATION('86',(#1143),#1135,(#573,#453,
#549,#569),#67,#1243,#1103);
#1404= VOLUME_3D_ELEMENT_REPRESENTATION('87',(#1143),#1135,(#425,#453,
#569,#549),#67,#1243,#1103);
#1407= VOLUME_3D_ELEMENT_REPRESENTATION('88',(#1143),#1135,(#429,#453,
#549,#337),#67,#1243,#1103);
#1410= VOLUME_3D_ELEMENT_REPRESENTATION('89',(#1143),#1135,(#573,#549,
#453,#353),#67,#1243,#1103);
#1413= VOLUME_3D_ELEMENT_REPRESENTATION('90',(#1143),#1135,(#333,#337,
#353,#453),#67,#1243,#1103);

#1416= VOLUME_3D_ELEMENT_REPRESENTATION('91', (#1143), #1135, (#357, #353, #337, #549), #67, #1243, #1103);
#1419= VOLUME_3D_ELEMENT_REPRESENTATION('92', (#1143), #1135, (#337, #453, #549, #353), #67, #1243, #1103);
#1422= VOLUME_3D_ELEMENT_REPRESENTATION('93', (#1143), #1135, (#433, #457, #553, #437), #67, #1243, #1103);
#1425= VOLUME_3D_ELEMENT_REPRESENTATION('94', (#1143), #1135, (#577, #553, #457, #581), #67, #1243, #1103);
#1428= VOLUME_3D_ELEMENT_REPRESENTATION('95', (#1143), #1135, (#461, #437, #581, #457), #67, #1243, #1103);
#1431= VOLUME_3D_ELEMENT_REPRESENTATION('96', (#1143), #1135, (#557, #581, #437, #553), #67, #1243, #1103);
#1434= VOLUME_3D_ELEMENT_REPRESENTATION('97', (#1143), #1135, (#437, #457, #553, #581), #67, #1243, #1103);
#1437= VOLUME_3D_ELEMENT_REPRESENTATION('98', (#1143), #1135, (#461, #581, #437, #465), #67, #1243, #1103);
#1440= VOLUME_3D_ELEMENT_REPRESENTATION('99', (#1143), #1135, (#557, #437, #581, #561), #67, #1243, #1103);
#1443= VOLUME_3D_ELEMENT_REPRESENTATION('100', (#1143), #1135, (#441, #561, #465, #437), #67, #1243, #1103);
#1446= VOLUME_3D_ELEMENT_REPRESENTATION('101', (#1143), #1135, (#585, #465, #561, #581), #67, #1243, #1103);
#1449= VOLUME_3D_ELEMENT_REPRESENTATION('102', (#1143), #1135, (#437, #465, #581, #561), #67, #1243, #1103);
#1452= VOLUME_3D_ELEMENT_REPRESENTATION('103', (#1143), #1135, (#441, #465, #561, #445), #67, #1243, #1103);
#1455= VOLUME_3D_ELEMENT_REPRESENTATION('104', (#1143), #1135, (#585, #561, #465, #589), #67, #1243, #1103);
#1458= VOLUME_3D_ELEMENT_REPRESENTATION('105', (#1143), #1135, (#469, #445, #589, #465), #67, #1243, #1103);
#1461= VOLUME_3D_ELEMENT_REPRESENTATION('106', (#1143), #1135, (#565, #589, #445, #561), #67, #1243, #1103);
#1464= VOLUME_3D_ELEMENT_REPRESENTATION('107', (#1143), #1135, (#445, #465, #561, #589), #67, #1243, #1103);
#1467= VOLUME_3D_ELEMENT_REPRESENTATION('108', (#1143), #1135, (#469, #589, #445, #473), #67, #1243, #1103);
#1470= VOLUME_3D_ELEMENT_REPRESENTATION('109', (#1143), #1135, (#565, #445, #589, #569), #67, #1243, #1103);
#1473= VOLUME_3D_ELEMENT_REPRESENTATION('110', (#1143), #1135, (#449, #569, #473, #445), #67, #1243, #1103);
#1476= VOLUME_3D_ELEMENT_REPRESENTATION('111', (#1143), #1135, (#593, #473, #569, #589), #67, #1243, #1103);
#1479= VOLUME_3D_ELEMENT_REPRESENTATION('112', (#1143), #1135, (#445, #473, #589, #569), #67, #1243, #1103);
#1482= VOLUME_3D_ELEMENT_REPRESENTATION('113', (#1143), #1135, (#449, #473, #569, #453), #67, #1243, #1103);
#1485= VOLUME_3D_ELEMENT_REPRESENTATION('114', (#1143), #1135, (#593, #569, #473, #597), #67, #1243, #1103);
#1488= VOLUME_3D_ELEMENT_REPRESENTATION('115', (#1143), #1135, (#477, #453, #597, #473), #67, #1243, #1103);
#1491= VOLUME_3D_ELEMENT_REPRESENTATION('116', (#1143), #1135, (#573, #597, #453, #569), #67, #1243, #1103);
#1494= VOLUME_3D_ELEMENT_REPRESENTATION('117', (#1143), #1135, (#453, #473, #569, #597), #67, #1243, #1103);
#1497= VOLUME_3D_ELEMENT_REPRESENTATION('118', (#1143), #1135, (#477, #597, #453, #329), #67, #1243, #1103);
#1500= VOLUME_3D_ELEMENT_REPRESENTATION('119', (#1143), #1135, (#573, #453, #597, #353), #67, #1243, #1103);
#1503= VOLUME_3D_ELEMENT_REPRESENTATION('120', (#1143), #1135, (#333, #353, #329, #453), #67, #1243, #1103);
#1506= VOLUME_3D_ELEMENT_REPRESENTATION('121', (#1143), #1135, (#349, #329, #353, #597), #67, #1243, #1103);
#1509= VOLUME_3D_ELEMENT_REPRESENTATION('122', (#1143), #1135, (#453, #329, #597, #353), #67, #1243, #1103);
#1512= VOLUME_3D_ELEMENT_REPRESENTATION('123', (#1143), #1135, (#481, #601, #457, #485), #67, #1243, #1103);
#1515= VOLUME_3D_ELEMENT_REPRESENTATION('124', (#1143), #1135, (#577, #457, #601, #581), #67, #1243, #1103);
#1518= VOLUME_3D_ELEMENT_REPRESENTATION('125', (#1143), #1135, (#461, #581, #485, #457), #67, #1243, #1103);
#1521= VOLUME_3D_ELEMENT_REPRESENTATION('126', (#1143), #1135, (#605, #485,

#581,#601),#67,#1243,#1103);
#1524= VOLUME_3D_ELEMENT_REPRESENTATION('127',(#1143),#1135,(#457,#485,
#601,#581),#67,#1243,#1103);
#1527= VOLUME_3D_ELEMENT_REPRESENTATION('128',(#1143),#1135,(#461,#485,
#581,#465),#67,#1243,#1103);
#1530= VOLUME_3D_ELEMENT_REPRESENTATION('129',(#1143),#1135,(#605,#581,
#485,#609),#67,#1243,#1103);
#1533= VOLUME_3D_ELEMENT_REPRESENTATION('130',(#1143),#1135,(#489,#465,
#609,#485),#67,#1243,#1103);
#1536= VOLUME_3D_ELEMENT_REPRESENTATION('131',(#1143),#1135,(#585,#609,
#465,#581),#67,#1243,#1103);
#1539= VOLUME_3D_ELEMENT_REPRESENTATION('132',(#1143),#1135,(#465,#485,
#581,#609),#67,#1243,#1103);
#1542= VOLUME_3D_ELEMENT_REPRESENTATION('133',(#1143),#1135,(#489,#609,
#465,#493),#67,#1243,#1103);
#1545= VOLUME_3D_ELEMENT_REPRESENTATION('134',(#1143),#1135,(#585,#465,
#609,#589),#67,#1243,#1103);
#1548= VOLUME_3D_ELEMENT_REPRESENTATION('135',(#1143),#1135,(#469,#589,
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#1551= VOLUME_3D_ELEMENT_REPRESENTATION('136',(#1143),#1135,(#613,#493,
#589,#609),#67,#1243,#1103);
#1554= VOLUME_3D_ELEMENT_REPRESENTATION('137',(#1143),#1135,(#465,#493,
#609,#589),#67,#1243,#1103);
#1557= VOLUME_3D_ELEMENT_REPRESENTATION('138',(#1143),#1135,(#469,#493,
#589,#473),#67,#1243,#1103);
#1560= VOLUME_3D_ELEMENT_REPRESENTATION('139',(#1143),#1135,(#613,#589,
#493,#617),#67,#1243,#1103);
#1563= VOLUME_3D_ELEMENT_REPRESENTATION('140',(#1143),#1135,(#497,#473,
#617,#493),#67,#1243,#1103);
#1566= VOLUME_3D_ELEMENT_REPRESENTATION('141',(#1143),#1135,(#593,#617,
#473,#589),#67,#1243,#1103);
#1569= VOLUME_3D_ELEMENT_REPRESENTATION('142',(#1143),#1135,(#473,#493,
#589,#617),#67,#1243,#1103);
#1572= VOLUME_3D_ELEMENT_REPRESENTATION('143',(#1143),#1135,(#497,#617,
#473,#501),#67,#1243,#1103);
#1575= VOLUME_3D_ELEMENT_REPRESENTATION('144',(#1143),#1135,(#593,#473,
#617,#597),#67,#1243,#1103);
#1578= VOLUME_3D_ELEMENT_REPRESENTATION('145',(#1143),#1135,(#477,#597,
#501,#473),#67,#1243,#1103);
#1581= VOLUME_3D_ELEMENT_REPRESENTATION('146',(#1143),#1135,(#621,#501,
#597,#617),#67,#1243,#1103);
#1584= VOLUME_3D_ELEMENT_REPRESENTATION('147',(#1143),#1135,(#473,#501,
#617,#597),#67,#1243,#1103);
#1587= VOLUME_3D_ELEMENT_REPRESENTATION('148',(#1143),#1135,(#477,#501,
#597,#329),#67,#1243,#1103);
#1590= VOLUME_3D_ELEMENT_REPRESENTATION('149',(#1143),#1135,(#621,#597,
#501,#345),#67,#1243,#1103);
#1593= VOLUME_3D_ELEMENT_REPRESENTATION('150',(#1143),#1135,(#325,#329,
#345,#501),#67,#1243,#1103);
#1596= VOLUME_3D_ELEMENT_REPRESENTATION('151',(#1143),#1135,(#349,#345,
#329,#597),#67,#1243,#1103);
#1599= VOLUME_3D_ELEMENT_REPRESENTATION('152',(#1143),#1135,(#329,#501,
#597,#345),#67,#1243,#1103);
#1602= VOLUME_3D_ELEMENT_REPRESENTATION('153',(#1143),#1135,(#529,#649,
#505,#533),#67,#1243,#1103);
#1605= VOLUME_3D_ELEMENT_REPRESENTATION('154',(#1143),#1135,(#625,#505,
#649,#629),#67,#1243,#1103);
#1608= VOLUME_3D_ELEMENT_REPRESENTATION('155',(#1143),#1135,(#509,#629,
#533,#505),#67,#1243,#1103);
#1611= VOLUME_3D_ELEMENT_REPRESENTATION('156',(#1143),#1135,(#653,#533,
#629,#649),#67,#1243,#1103);
#1614= VOLUME_3D_ELEMENT_REPRESENTATION('157',(#1143),#1135,(#505,#533,
#649,#629),#67,#1243,#1103);
#1617= VOLUME_3D_ELEMENT_REPRESENTATION('158',(#1143),#1135,(#509,#533,
#629,#513),#67,#1243,#1103);
#1620= VOLUME_3D_ELEMENT_REPRESENTATION('159',(#1143),#1135,(#653,#629,
#533,#657),#67,#1243,#1103);
#1623= VOLUME_3D_ELEMENT_REPRESENTATION('160',(#1143),#1135,(#537,#513,
#657,#533),#67,#1243,#1103);
#1626= VOLUME_3D_ELEMENT_REPRESENTATION('161',(#1143),#1135,(#633,#657,
#513,#629),#67,#1243,#1103);

#1629= VOLUME_3D_ELEMENT_REPRESENTATION('162', (#1143), #1135, (#513, #533, #629, #657), #67, #1243, #1103);
#1632= VOLUME_3D_ELEMENT_REPRESENTATION('163', (#1143), #1135, (#537, #657, #513, #541), #67, #1243, #1103);
#1635= VOLUME_3D_ELEMENT_REPRESENTATION('164', (#1143), #1135, (#633, #513, #657, #637), #67, #1243, #1103);
#1638= VOLUME_3D_ELEMENT_REPRESENTATION('165', (#1143), #1135, (#517, #637, #541, #513), #67, #1243, #1103);
#1641= VOLUME_3D_ELEMENT_REPRESENTATION('166', (#1143), #1135, (#661, #541, #637, #657), #67, #1243, #1103);
#1644= VOLUME_3D_ELEMENT_REPRESENTATION('167', (#1143), #1135, (#513, #541, #657, #637), #67, #1243, #1103);
#1647= VOLUME_3D_ELEMENT_REPRESENTATION('168', (#1143), #1135, (#517, #541, #637, #521), #67, #1243, #1103);
#1650= VOLUME_3D_ELEMENT_REPRESENTATION('169', (#1143), #1135, (#661, #637, #541, #665), #67, #1243, #1103);
#1653= VOLUME_3D_ELEMENT_REPRESENTATION('170', (#1143), #1135, (#545, #521, #665, #541), #67, #1243, #1103);
#1656= VOLUME_3D_ELEMENT_REPRESENTATION('171', (#1143), #1135, (#641, #665, #521, #637), #67, #1243, #1103);
#1659= VOLUME_3D_ELEMENT_REPRESENTATION('172', (#1143), #1135, (#521, #541, #637, #665), #67, #1243, #1103);
#1662= VOLUME_3D_ELEMENT_REPRESENTATION('173', (#1143), #1135, (#545, #665, #521, #549), #67, #1243, #1103);
#1665= VOLUME_3D_ELEMENT_REPRESENTATION('174', (#1143), #1135, (#641, #521, #665, #645), #67, #1243, #1103);
#1668= VOLUME_3D_ELEMENT_REPRESENTATION('175', (#1143), #1135, (#525, #645, #549, #521), #67, #1243, #1103);
#1671= VOLUME_3D_ELEMENT_REPRESENTATION('176', (#1143), #1135, (#669, #549, #645, #665), #67, #1243, #1103);
#1674= VOLUME_3D_ELEMENT_REPRESENTATION('177', (#1143), #1135, (#521, #549, #665, #645), #67, #1243, #1103);
#1677= VOLUME_3D_ELEMENT_REPRESENTATION('178', (#1143), #1135, (#525, #549, #645, #361), #67, #1243, #1103);
#1680= VOLUME_3D_ELEMENT_REPRESENTATION('179', (#1143), #1135, (#669, #645, #549, #377), #67, #1243, #1103);
#1683= VOLUME_3D_ELEMENT_REPRESENTATION('180', (#1143), #1135, (#357, #361, #377, #549), #67, #1243, #1103);
#1686= VOLUME_3D_ELEMENT_REPRESENTATION('181', (#1143), #1135, (#381, #377, #361, #645), #67, #1243, #1103);
#1689= VOLUME_3D_ELEMENT_REPRESENTATION('182', (#1143), #1135, (#361, #549, #645, #377), #67, #1243, #1103);
#1692= VOLUME_3D_ELEMENT_REPRESENTATION('183', (#1143), #1135, (#529, #553, #649, #533), #67, #1243, #1103);
#1695= VOLUME_3D_ELEMENT_REPRESENTATION('184', (#1143), #1135, (#673, #649, #553, #677), #67, #1243, #1103);
#1698= VOLUME_3D_ELEMENT_REPRESENTATION('185', (#1143), #1135, (#557, #533, #677, #553), #67, #1243, #1103);
#1701= VOLUME_3D_ELEMENT_REPRESENTATION('186', (#1143), #1135, (#653, #677, #533, #649), #67, #1243, #1103);
#1704= VOLUME_3D_ELEMENT_REPRESENTATION('187', (#1143), #1135, (#533, #553, #649, #677), #67, #1243, #1103);
#1707= VOLUME_3D_ELEMENT_REPRESENTATION('188', (#1143), #1135, (#557, #677, #533, #561), #67, #1243, #1103);
#1710= VOLUME_3D_ELEMENT_REPRESENTATION('189', (#1143), #1135, (#653, #533, #677, #657), #67, #1243, #1103);
#1713= VOLUME_3D_ELEMENT_REPRESENTATION('190', (#1143), #1135, (#537, #657, #561, #533), #67, #1243, #1103);
#1716= VOLUME_3D_ELEMENT_REPRESENTATION('191', (#1143), #1135, (#681, #561, #657, #677), #67, #1243, #1103);
#1719= VOLUME_3D_ELEMENT_REPRESENTATION('192', (#1143), #1135, (#533, #561, #677, #657), #67, #1243, #1103);
#1722= VOLUME_3D_ELEMENT_REPRESENTATION('193', (#1143), #1135, (#537, #561, #657, #541), #67, #1243, #1103);
#1725= VOLUME_3D_ELEMENT_REPRESENTATION('194', (#1143), #1135, (#681, #657, #561, #685), #67, #1243, #1103);
#1728= VOLUME_3D_ELEMENT_REPRESENTATION('195', (#1143), #1135, (#565, #541, #685, #561), #67, #1243, #1103);
#1731= VOLUME_3D_ELEMENT_REPRESENTATION('196', (#1143), #1135, (#661, #685, #541, #657), #67, #1243, #1103);
#1734= VOLUME_3D_ELEMENT_REPRESENTATION('197', (#1143), #1135, (#541, #561,

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#657,#685),#67,#1243,#1103);
#1737= VOLUME_3D_ELEMENT_REPRESENTATION('198',(#1143),#1135,(#565,#685,
#541,#569),#67,#1243,#1103);
#1740= VOLUME_3D_ELEMENT_REPRESENTATION('199',(#1143),#1135,(#661,#541,
#685,#665),#67,#1243,#1103);
#1743= VOLUME_3D_ELEMENT_REPRESENTATION('200',(#1143),#1135,(#545,#665,
#569,#541),#67,#1243,#1103);
#1746= VOLUME_3D_ELEMENT_REPRESENTATION('201',(#1143),#1135,(#689,#569,
#665,#685),#67,#1243,#1103);
#1749= VOLUME_3D_ELEMENT_REPRESENTATION('202',(#1143),#1135,(#541,#569,
#685,#665),#67,#1243,#1103);
#1752= VOLUME_3D_ELEMENT_REPRESENTATION('203',(#1143),#1135,(#545,#569,
#665,#549),#67,#1243,#1103);
#1755= VOLUME_3D_ELEMENT_REPRESENTATION('204',(#1143),#1135,(#689,#665,
#569,#693),#67,#1243,#1103);
#1758= VOLUME_3D_ELEMENT_REPRESENTATION('205',(#1143),#1135,(#573,#549,
#693,#569),#67,#1243,#1103);
#1761= VOLUME_3D_ELEMENT_REPRESENTATION('206',(#1143),#1135,(#669,#693,
#549,#665),#67,#1243,#1103);
#1764= VOLUME_3D_ELEMENT_REPRESENTATION('207',(#1143),#1135,(#549,#569,
#665,#693),#67,#1243,#1103);
#1767= VOLUME_3D_ELEMENT_REPRESENTATION('208',(#1143),#1135,(#573,#693,
#549,#353),#67,#1243,#1103);
#1770= VOLUME_3D_ELEMENT_REPRESENTATION('209',(#1143),#1135,(#669,#549,
#693,#377),#67,#1243,#1103);
#1773= VOLUME_3D_ELEMENT_REPRESENTATION('210',(#1143),#1135,(#357,#377,
#353,#549),#67,#1243,#1103);
#1776= VOLUME_3D_ELEMENT_REPRESENTATION('211',(#1143),#1135,(#373,#353,
#377,#693),#67,#1243,#1103);
#1779= VOLUME_3D_ELEMENT_REPRESENTATION('212',(#1143),#1135,(#549,#353,
#693,#377),#67,#1243,#1103);
#1782= VOLUME_3D_ELEMENT_REPRESENTATION('213',(#1143),#1135,(#577,#697,
#553,#581),#67,#1243,#1103);
#1785= VOLUME_3D_ELEMENT_REPRESENTATION('214',(#1143),#1135,(#673,#553,
#697,#677),#67,#1243,#1103);
#1788= VOLUME_3D_ELEMENT_REPRESENTATION('215',(#1143),#1135,(#557,#677,
#581,#553),#67,#1243,#1103);
#1791= VOLUME_3D_ELEMENT_REPRESENTATION('216',(#1143),#1135,(#701,#581,
#677,#697),#67,#1243,#1103);
#1794= VOLUME_3D_ELEMENT_REPRESENTATION('217',(#1143),#1135,(#553,#581,
#697,#677),#67,#1243,#1103);
#1797= VOLUME_3D_ELEMENT_REPRESENTATION('218',(#1143),#1135,(#557,#581,
#677,#561),#67,#1243,#1103);
#1800= VOLUME_3D_ELEMENT_REPRESENTATION('219',(#1143),#1135,(#701,#677,
#581,#705),#67,#1243,#1103);
#1803= VOLUME_3D_ELEMENT_REPRESENTATION('220',(#1143),#1135,(#585,#561,
#705,#581),#67,#1243,#1103);
#1806= VOLUME_3D_ELEMENT_REPRESENTATION('221',(#1143),#1135,(#681,#705,
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#1809= VOLUME_3D_ELEMENT_REPRESENTATION('222',(#1143),#1135,(#561,#581,
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#1812= VOLUME_3D_ELEMENT_REPRESENTATION('223',(#1143),#1135,(#585,#705,
#561,#589),#67,#1243,#1103);
#1815= VOLUME_3D_ELEMENT_REPRESENTATION('224',(#1143),#1135,(#681,#561,
#705,#685),#67,#1243,#1103);
#1818= VOLUME_3D_ELEMENT_REPRESENTATION('225',(#1143),#1135,(#565,#685,
#589,#561),#67,#1243,#1103);
#1821= VOLUME_3D_ELEMENT_REPRESENTATION('226',(#1143),#1135,(#709,#589,
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#1824= VOLUME_3D_ELEMENT_REPRESENTATION('227',(#1143),#1135,(#561,#589,
#705,#685),#67,#1243,#1103);
#1827= VOLUME_3D_ELEMENT_REPRESENTATION('228',(#1143),#1135,(#565,#589,
#685,#569),#67,#1243,#1103);
#1830= VOLUME_3D_ELEMENT_REPRESENTATION('229',(#1143),#1135,(#709,#685,
#589,#713),#67,#1243,#1103);
#1833= VOLUME_3D_ELEMENT_REPRESENTATION('230',(#1143),#1135,(#593,#569,
#713,#589),#67,#1243,#1103);
#1836= VOLUME_3D_ELEMENT_REPRESENTATION('231',(#1143),#1135,(#689,#713,
#569,#685),#67,#1243,#1103);
#1839= VOLUME_3D_ELEMENT_REPRESENTATION('232',(#1143),#1135,(#569,#589,
#685,#713),#67,#1243,#1103);
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#1842= VOLUME_3D_ELEMENT_REPRESENTATION('233', (#1143), #1135, (#593, #713, #569, #597), #67, #1243, #1103);
#1845= VOLUME_3D_ELEMENT_REPRESENTATION('234', (#1143), #1135, (#689, #569, #713, #693), #67, #1243, #1103);
#1848= VOLUME_3D_ELEMENT_REPRESENTATION('235', (#1143), #1135, (#573, #693, #597, #569), #67, #1243, #1103);
#1851= VOLUME_3D_ELEMENT_REPRESENTATION('236', (#1143), #1135, (#717, #597, #693, #713), #67, #1243, #1103);
#1854= VOLUME_3D_ELEMENT_REPRESENTATION('237', (#1143), #1135, (#569, #597, #713, #693), #67, #1243, #1103);
#1857= VOLUME_3D_ELEMENT_REPRESENTATION('238', (#1143), #1135, (#573, #597, #693, #353), #67, #1243, #1103);
#1860= VOLUME_3D_ELEMENT_REPRESENTATION('239', (#1143), #1135, (#717, #693, #597, #369), #67, #1243, #1103);
#1863= VOLUME_3D_ELEMENT_REPRESENTATION('240', (#1143), #1135, (#349, #353, #369, #597), #67, #1243, #1103);
#1866= VOLUME_3D_ELEMENT_REPRESENTATION('241', (#1143), #1135, (#373, #369, #353, #693), #67, #1243, #1103);
#1869= VOLUME_3D_ELEMENT_REPRESENTATION('242', (#1143), #1135, (#353, #597, #693, #369), #67, #1243, #1103);
#1872= VOLUME_3D_ELEMENT_REPRESENTATION('243', (#1143), #1135, (#577, #601, #697, #581), #67, #1243, #1103);
#1875= VOLUME_3D_ELEMENT_REPRESENTATION('244', (#1143), #1135, (#721, #697, #601, #725), #67, #1243, #1103);
#1878= VOLUME_3D_ELEMENT_REPRESENTATION('245', (#1143), #1135, (#605, #581, #725, #601), #67, #1243, #1103);
#1881= VOLUME_3D_ELEMENT_REPRESENTATION('246', (#1143), #1135, (#701, #725, #581, #697), #67, #1243, #1103);
#1884= VOLUME_3D_ELEMENT_REPRESENTATION('247', (#1143), #1135, (#581, #601, #697, #725), #67, #1243, #1103);
#1887= VOLUME_3D_ELEMENT_REPRESENTATION('248', (#1143), #1135, (#605, #725, #581, #609), #67, #1243, #1103);
#1890= VOLUME_3D_ELEMENT_REPRESENTATION('249', (#1143), #1135, (#701, #581, #725, #705), #67, #1243, #1103);
#1893= VOLUME_3D_ELEMENT_REPRESENTATION('250', (#1143), #1135, (#585, #705, #609, #581), #67, #1243, #1103);
#1896= VOLUME_3D_ELEMENT_REPRESENTATION('251', (#1143), #1135, (#729, #609, #705, #725), #67, #1243, #1103);
#1899= VOLUME_3D_ELEMENT_REPRESENTATION('252', (#1143), #1135, (#581, #609, #725, #705), #67, #1243, #1103);
#1902= VOLUME_3D_ELEMENT_REPRESENTATION('253', (#1143), #1135, (#585, #609, #705, #589), #67, #1243, #1103);
#1905= VOLUME_3D_ELEMENT_REPRESENTATION('254', (#1143), #1135, (#729, #705, #609, #733), #67, #1243, #1103);
#1908= VOLUME_3D_ELEMENT_REPRESENTATION('255', (#1143), #1135, (#613, #589, #733, #609), #67, #1243, #1103);
#1911= VOLUME_3D_ELEMENT_REPRESENTATION('256', (#1143), #1135, (#709, #733, #589, #705), #67, #1243, #1103);
#1914= VOLUME_3D_ELEMENT_REPRESENTATION('257', (#1143), #1135, (#589, #609, #705, #733), #67, #1243, #1103);
#1917= VOLUME_3D_ELEMENT_REPRESENTATION('258', (#1143), #1135, (#613, #733, #589, #617), #67, #1243, #1103);
#1920= VOLUME_3D_ELEMENT_REPRESENTATION('259', (#1143), #1135, (#709, #589, #733, #713), #67, #1243, #1103);
#1923= VOLUME_3D_ELEMENT_REPRESENTATION('260', (#1143), #1135, (#593, #713, #617, #589), #67, #1243, #1103);
#1926= VOLUME_3D_ELEMENT_REPRESENTATION('261', (#1143), #1135, (#737, #617, #713, #733), #67, #1243, #1103);
#1929= VOLUME_3D_ELEMENT_REPRESENTATION('262', (#1143), #1135, (#589, #617, #733, #713), #67, #1243, #1103);
#1932= VOLUME_3D_ELEMENT_REPRESENTATION('263', (#1143), #1135, (#593, #617, #713, #597), #67, #1243, #1103);
#1935= VOLUME_3D_ELEMENT_REPRESENTATION('264', (#1143), #1135, (#737, #713, #617, #741), #67, #1243, #1103);
#1938= VOLUME_3D_ELEMENT_REPRESENTATION('265', (#1143), #1135, (#621, #597, #741, #617), #67, #1243, #1103);
#1941= VOLUME_3D_ELEMENT_REPRESENTATION('266', (#1143), #1135, (#717, #741, #597, #713), #67, #1243, #1103);
#1944= VOLUME_3D_ELEMENT_REPRESENTATION('267', (#1143), #1135, (#597, #617, #713, #741), #67, #1243, #1103);
#1947= VOLUME_3D_ELEMENT_REPRESENTATION('268', (#1143), #1135, (#621, #741,


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#597,#345),#67,#1243,#1103);
#1950= VOLUME_3D_ELEMENT_REPRESENTATION('269',(#1143),#1135,(#717,#597,
#741,#369),#67,#1243,#1103);
#1953= VOLUME_3D_ELEMENT_REPRESENTATION('270',(#1143),#1135,(#349,#369,
#345,#597),#67,#1243,#1103);
#1956= VOLUME_3D_ELEMENT_REPRESENTATION('271',(#1143),#1135,(#365,#345,
#369,#741),#67,#1243,#1103);
#1959= VOLUME_3D_ELEMENT_REPRESENTATION('272',(#1143),#1135,(#597,#345,
#741,#369),#67,#1243,#1103);
#1962= VOLUME_3D_ELEMENT_REPRESENTATION('273',(#1143),#1135,(#773,#769,
#745,#893,#889,#865),#67,#1965,#1103);
#1965= VOLUME_3D_ELEMENT_DESCRIPTOR(.LINEAR_ORDER.,'LINEAR_WEDGE.CPENTA',
(ENUMERATED_VOLUME_ELEMENT_PURPOSE(.STRESS_DISPLACEMENT.)),.WEDGE.);
#1967= VOLUME_3D_ELEMENT_REPRESENTATION('274',(#1143),#1135,(#745,#749,
#773,#865,#869,#893),#67,#1965,#1103);
#1970= VOLUME_3D_ELEMENT_REPRESENTATION('275',(#1143),#1135,(#749,#753,
#773,#869,#873,#893),#67,#1965,#1103);
#1973= VOLUME_3D_ELEMENT_REPRESENTATION('276',(#1143),#1135,(#777,#773,
#753,#897,#893,#873),#67,#1965,#1103);
#1976= VOLUME_3D_ELEMENT_REPRESENTATION('277',(#1143),#1135,(#781,#777,
#753,#901,#897,#873),#67,#1965,#1103);
#1979= VOLUME_3D_ELEMENT_REPRESENTATION('278',(#1143),#1135,(#753,#757,
#781,#873,#877,#901),#67,#1965,#1103);
#1982= VOLUME_3D_ELEMENT_REPRESENTATION('279',(#1143),#1135,(#757,#761,
#781,#877,#881,#901),#67,#1965,#1103);
#1985= VOLUME_3D_ELEMENT_REPRESENTATION('280',(#1143),#1135,(#785,#781,
#761,#905,#901,#881),#67,#1965,#1103);
#1988= VOLUME_3D_ELEMENT_REPRESENTATION('281',(#1143),#1135,(#789,#785,
#761,#909,#905,#881),#67,#1965,#1103);
#1991= VOLUME_3D_ELEMENT_REPRESENTATION('282',(#1143),#1135,(#761,#765,
#789,#881,#885,#909),#67,#1965,#1103);
#1994= VOLUME_3D_ELEMENT_REPRESENTATION('283',(#1143),#1135,(#765,#385,
#789,#885,#505,#909),#67,#1965,#1103);
#1997= VOLUME_3D_ELEMENT_REPRESENTATION('284',(#1143),#1135,(#409,#789,
#385,#529,#909,#505),#67,#1965,#1103);
#2000= VOLUME_3D_ELEMENT_REPRESENTATION('285',(#1143),#1135,(#769,#773,
#793,#889,#893,#913),#67,#1965,#1103);
#2003= VOLUME_3D_ELEMENT_REPRESENTATION('286',(#1143),#1135,(#797,#793,
#773,#917,#913,#893),#67,#1965,#1103);
#2006= VOLUME_3D_ELEMENT_REPRESENTATION('287',(#1143),#1135,(#801,#797,
#773,#921,#917,#893),#67,#1965,#1103);
#2009= VOLUME_3D_ELEMENT_REPRESENTATION('288',(#1143),#1135,(#773,#777,
#801,#893,#897,#921),#67,#1965,#1103);
#2012= VOLUME_3D_ELEMENT_REPRESENTATION('289',(#1143),#1135,(#777,#781,
#801,#897,#901,#921),#67,#1965,#1103);
#2015= VOLUME_3D_ELEMENT_REPRESENTATION('290',(#1143),#1135,(#805,#801,
#781,#925,#921,#901),#67,#1965,#1103);
#2018= VOLUME_3D_ELEMENT_REPRESENTATION('291',(#1143),#1135,(#809,#805,
#781,#929,#925,#901),#67,#1965,#1103);
#2021= VOLUME_3D_ELEMENT_REPRESENTATION('292',(#1143),#1135,(#781,#785,
#809,#901,#905,#929),#67,#1965,#1103);
#2024= VOLUME_3D_ELEMENT_REPRESENTATION('293',(#1143),#1135,(#785,#789,
#809,#905,#909,#929),#67,#1965,#1103);
#2027= VOLUME_3D_ELEMENT_REPRESENTATION('294',(#1143),#1135,(#813,#809,
#789,#933,#929,#909),#67,#1965,#1103);
#2030= VOLUME_3D_ELEMENT_REPRESENTATION('295',(#1143),#1135,(#433,#813,
#789,#553,#933,#909),#67,#1965,#1103);
#2033= VOLUME_3D_ELEMENT_REPRESENTATION('296',(#1143),#1135,(#789,#409,
#433,#909,#529,#553),#67,#1965,#1103);
#2036= VOLUME_3D_ELEMENT_REPRESENTATION('297',(#1143),#1135,(#821,#817,
#793,#941,#937,#913),#67,#1965,#1103);
#2039= VOLUME_3D_ELEMENT_REPRESENTATION('298',(#1143),#1135,(#793,#797,
#821,#913,#917,#941),#67,#1965,#1103);
#2042= VOLUME_3D_ELEMENT_REPRESENTATION('299',(#1143),#1135,(#797,#801,
#821,#917,#921,#941),#67,#1965,#1103);
#2045= VOLUME_3D_ELEMENT_REPRESENTATION('300',(#1143),#1135,(#825,#821,
#801,#945,#941,#921),#67,#1965,#1103);
#2048= VOLUME_3D_ELEMENT_REPRESENTATION('301',(#1143),#1135,(#829,#825,
#801,#949,#945,#921),#67,#1965,#1103);
#2051= VOLUME_3D_ELEMENT_REPRESENTATION('302',(#1143),#1135,(#801,#805,
#829,#921,#925,#949),#67,#1965,#1103);

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#2054= VOLUME_3D_ELEMENT_REPRESENTATION('303', (#1143), #1135, (#805, #809,
#829, #925, #929, #949), #67, #1965, #1103);
#2057= VOLUME_3D_ELEMENT_REPRESENTATION('304', (#1143), #1135, (#833, #829,
#809, #953, #949, #929), #67, #1965, #1103);
#2060= VOLUME_3D_ELEMENT_REPRESENTATION('305', (#1143), #1135, (#837, #833,
#809, #957, #953, #929), #67, #1965, #1103);
#2063= VOLUME_3D_ELEMENT_REPRESENTATION('306', (#1143), #1135, (#809, #813,
#837, #929, #933, #957), #67, #1965, #1103);
#2066= VOLUME_3D_ELEMENT_REPRESENTATION('307', (#1143), #1135, (#813, #433,
#837, #933, #553, #957), #67, #1965, #1103);
#2069= VOLUME_3D_ELEMENT_REPRESENTATION('308', (#1143), #1135, (#457, #837,
#433, #577, #957, #553), #67, #1965, #1103);
#2072= VOLUME_3D_ELEMENT_REPRESENTATION('309', (#1143), #1135, (#817, #821,
#841, #937, #941, #961), #67, #1965, #1103);
#2075= VOLUME_3D_ELEMENT_REPRESENTATION('310', (#1143), #1135, (#845, #841,
#821, #965, #961, #941), #67, #1965, #1103);
#2078= VOLUME_3D_ELEMENT_REPRESENTATION('311', (#1143), #1135, (#849, #845,
#821, #969, #965, #941), #67, #1965, #1103);
#2081= VOLUME_3D_ELEMENT_REPRESENTATION('312', (#1143), #1135, (#821, #825,
#849, #941, #945, #969), #67, #1965, #1103);
#2084= VOLUME_3D_ELEMENT_REPRESENTATION('313', (#1143), #1135, (#825, #829,
#849, #945, #949, #969), #67, #1965, #1103);
#2087= VOLUME_3D_ELEMENT_REPRESENTATION('314', (#1143), #1135, (#853, #849,
#829, #973, #969, #949), #67, #1965, #1103);
#2090= VOLUME_3D_ELEMENT_REPRESENTATION('315', (#1143), #1135, (#857, #853,
#829, #977, #973, #949), #67, #1965, #1103);
#2093= VOLUME_3D_ELEMENT_REPRESENTATION('316', (#1143), #1135, (#829, #833,
#857, #949, #953, #977), #67, #1965, #1103);
#2096= VOLUME_3D_ELEMENT_REPRESENTATION('317', (#1143), #1135, (#833, #837,
#857, #953, #957, #977), #67, #1965, #1103);
#2099= VOLUME_3D_ELEMENT_REPRESENTATION('318', (#1143), #1135, (#861, #857,
#837, #981, #977, #957), #67, #1965, #1103);
#2102= VOLUME_3D_ELEMENT_REPRESENTATION('319', (#1143), #1135, (#481, #861,
#837, #601, #981, #957), #67, #1965, #1103);
#2105= VOLUME_3D_ELEMENT_REPRESENTATION('320', (#1143), #1135, (#837, #457,
#481, #957, #577, #601), #67, #1965, #1103);
#2108= VOLUME_3D_ELEMENT_REPRESENTATION('321', (#1143), #1135, (#893, #889,
#865, #1013, #1009, #985), #67, #1965, #1103);
#2111= VOLUME_3D_ELEMENT_REPRESENTATION('322', (#1143), #1135, (#865, #869,
#893, #985, #989, #1013), #67, #1965, #1103);
#2114= VOLUME_3D_ELEMENT_REPRESENTATION('323', (#1143), #1135, (#869, #873,
#893, #989, #993, #1013), #67, #1965, #1103);
#2117= VOLUME_3D_ELEMENT_REPRESENTATION('324', (#1143), #1135, (#897, #893,
#873, #1017, #1013, #993), #67, #1965, #1103);
#2120= VOLUME_3D_ELEMENT_REPRESENTATION('325', (#1143), #1135, (#901, #897,
#873, #1021, #1017, #993), #67, #1965, #1103);
#2123= VOLUME_3D_ELEMENT_REPRESENTATION('326', (#1143), #1135, (#873, #877,
#901, #993, #997, #1021), #67, #1965, #1103);
#2126= VOLUME_3D_ELEMENT_REPRESENTATION('327', (#1143), #1135, (#877, #881,
#901, #997, #1001, #1021), #67, #1965, #1103);
#2129= VOLUME_3D_ELEMENT_REPRESENTATION('328', (#1143), #1135, (#905, #901,
#881, #1025, #1021, #1001), #67, #1965, #1103);
#2132= VOLUME_3D_ELEMENT_REPRESENTATION('329', (#1143), #1135, (#909, #905,
#881, #1029, #1025, #1001), #67, #1965, #1103);
#2135= VOLUME_3D_ELEMENT_REPRESENTATION('330', (#1143), #1135, (#881, #885,
#909, #1001, #1005, #1029), #67, #1965, #1103);
#2138= VOLUME_3D_ELEMENT_REPRESENTATION('331', (#1143), #1135, (#885, #505,
#909, #1005, #625, #1029), #67, #1965, #1103);
#2141= VOLUME_3D_ELEMENT_REPRESENTATION('332', (#1143), #1135, (#529, #909,
#505, #649, #1029, #625), #67, #1965, #1103);
#2144= VOLUME_3D_ELEMENT_REPRESENTATION('333', (#1143), #1135, (#889, #893,
#913, #1009, #1013, #1033), #67, #1965, #1103);
#2147= VOLUME_3D_ELEMENT_REPRESENTATION('334', (#1143), #1135, (#917, #913,
#893, #1037, #1033, #1013), #67, #1965, #1103);
#2150= VOLUME_3D_ELEMENT_REPRESENTATION('335', (#1143), #1135, (#921, #917,
#893, #1041, #1037, #1013), #67, #1965, #1103);
#2153= VOLUME_3D_ELEMENT_REPRESENTATION('336', (#1143), #1135, (#893, #897,
#921, #1013, #1017, #1041), #67, #1965, #1103);
#2156= VOLUME_3D_ELEMENT_REPRESENTATION('337', (#1143), #1135, (#897, #901,
#921, #1017, #1021, #1041), #67, #1965, #1103);
#2159= VOLUME_3D_ELEMENT_REPRESENTATION('338', (#1143), #1135, (#925, #921,

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#901,#1045,#1041,#1021),#67,#1965,#1103);
#2162= VOLUME_3D_ELEMENT_REPRESENTATION('339',(#1143),#1135,(#929,#925,
#901,#1049,#1045,#1021),#67,#1965,#1103);
#2165= VOLUME_3D_ELEMENT_REPRESENTATION('340',(#1143),#1135,(#901,#905,
#929,#1021,#1025,#1049),#67,#1965,#1103);
#2168= VOLUME_3D_ELEMENT_REPRESENTATION('341',(#1143),#1135,(#905,#909,
#929,#1025,#1029,#1049),#67,#1965,#1103);
#2171= VOLUME_3D_ELEMENT_REPRESENTATION('342',(#1143),#1135,(#933,#929,
#909,#1053,#1049,#1029),#67,#1965,#1103);
#2174= VOLUME_3D_ELEMENT_REPRESENTATION('343',(#1143),#1135,(#553,#933,
#909,#673,#1053,#1029),#67,#1965,#1103);
#2177= VOLUME_3D_ELEMENT_REPRESENTATION('344',(#1143),#1135,(#909,#529,
#553,#1029,#649,#673),#67,#1965,#1103);
#2180= VOLUME_3D_ELEMENT_REPRESENTATION('345',(#1143),#1135,(#941,#937,
#913,#1061,#1057,#1033),#67,#1965,#1103);
#2183= VOLUME_3D_ELEMENT_REPRESENTATION('346',(#1143),#1135,(#913,#917,
#941,#1033,#1037,#1061),#67,#1965,#1103);
#2186= VOLUME_3D_ELEMENT_REPRESENTATION('347',(#1143),#1135,(#917,#921,
#941,#1037,#1041,#1061),#67,#1965,#1103);
#2189= VOLUME_3D_ELEMENT_REPRESENTATION('348',(#1143),#1135,(#945,#941,
#921,#1065,#1061,#1041),#67,#1965,#1103);
#2192= VOLUME_3D_ELEMENT_REPRESENTATION('349',(#1143),#1135,(#949,#945,
#921,#1069,#1065,#1041),#67,#1965,#1103);
#2195= VOLUME_3D_ELEMENT_REPRESENTATION('350',(#1143),#1135,(#921,#925,
#949,#1041,#1045,#1069),#67,#1965,#1103);
#2198= VOLUME_3D_ELEMENT_REPRESENTATION('351',(#1143),#1135,(#925,#929,
#949,#1045,#1049,#1069),#67,#1965,#1103);
#2201= VOLUME_3D_ELEMENT_REPRESENTATION('352',(#1143),#1135,(#953,#949,
#929,#1073,#1069,#1049),#67,#1965,#1103);
#2204= VOLUME_3D_ELEMENT_REPRESENTATION('353',(#1143),#1135,(#957,#953,
#929,#1077,#1073,#1049),#67,#1965,#1103);
#2207= VOLUME_3D_ELEMENT_REPRESENTATION('354',(#1143),#1135,(#929,#933,
#957,#1049,#1053,#1077),#67,#1965,#1103);
#2210= VOLUME_3D_ELEMENT_REPRESENTATION('355',(#1143),#1135,(#933,#553,
#957,#1053,#673,#1077),#67,#1965,#1103);
#2213= VOLUME_3D_ELEMENT_REPRESENTATION('356',(#1143),#1135,(#577,#957,
#553,#697,#1077,#673),#67,#1965,#1103);
#2216= VOLUME_3D_ELEMENT_REPRESENTATION('357',(#1143),#1135,(#937,#941,
#961,#1057,#1061,#1081),#67,#1965,#1103);
#2219= VOLUME_3D_ELEMENT_REPRESENTATION('358',(#1143),#1135,(#965,#961,
#941,#1085,#1081,#1061),#67,#1965,#1103);
#2222= VOLUME_3D_ELEMENT_REPRESENTATION('359',(#1143),#1135,(#969,#965,
#941,#1089,#1085,#1061),#67,#1965,#1103);
#2225= VOLUME_3D_ELEMENT_REPRESENTATION('360',(#1143),#1135,(#941,#945,
#969,#1061,#1065,#1089),#67,#1965,#1103);
#2228= VOLUME_3D_ELEMENT_REPRESENTATION('361',(#1143),#1135,(#945,#949,
#969,#1065,#1069,#1089),#67,#1965,#1103);
#2231= VOLUME_3D_ELEMENT_REPRESENTATION('362',(#1143),#1135,(#973,#969,
#949,#1093,#1089,#1069),#67,#1965,#1103);
#2234= VOLUME_3D_ELEMENT_REPRESENTATION('363',(#1143),#1135,(#977,#973,
#949,#1097,#1093,#1069),#67,#1965,#1103);
#2237= VOLUME_3D_ELEMENT_REPRESENTATION('364',(#1143),#1135,(#949,#953,
#977,#1069,#1073,#1097),#67,#1965,#1103);
#2240= VOLUME_3D_ELEMENT_REPRESENTATION('365',(#1143),#1135,(#953,#957,
#977,#1073,#1077,#1097),#67,#1965,#1103);
#2243= VOLUME_3D_ELEMENT_REPRESENTATION('366',(#1143),#1135,(#981,#977,
#957,#1101,#1097,#1077),#67,#1965,#1103);
#2246= VOLUME_3D_ELEMENT_REPRESENTATION('367',(#1143),#1135,(#601,#981,
#957,#721,#1101,#1077),#67,#1965,#1103);
#2249= VOLUME_3D_ELEMENT_REPRESENTATION('368',(#1143),#1135,(#957,#577,
#601,#1077,#697,#721),#67,#1965,#1103);
#2252= CONTROL(#67,'Control.0','FemConvert',
'Nastran job EAS test case ATS4m4',('<SOL>101</SOL>','TIME 600','CEND',
'<GLOBALCASE>0</GLOBALCASE>','<SUBCASE>1</SUBCASE>',
'<SUBCASE>2</SUBCASE>','<SUBCASE>3</SUBCASE>','ENDDATA'),('NASTRAN'));
#2255= SPECIFIED_STATE('STEP DEFAULT','default_initial_state');
#2256= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#2252,'STATIC STEP 1',1,#2255,
',',#2396);
#2257= SPECIFIED_STATE('Step 1 Base Specified State',
'Relating Specified State');
#2258= SPECIFIED_STATE('SPCCASE 11 21 1','Aggregator SPC 11 Step 1');

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#2259= SPECIFIED_STATE('SPCVALSTATE_100_21','');
#2260= STATE_RELATIONSHIP(
'SPCVALSTATE_100_21 is related to SPCCASE_11_21_1','',#2258,#2259);
#2261= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2259,#2264,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)));
#2262= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#2264= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.0',(#2256),#113,#35,(
#2266,#2269,#2270),'');
#2266= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.X_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#2269= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Y_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#2270= FREEDOM_AND_COEFFICIENT(ENUMERATED_DEGREE_OF_FREEDOM(
.Z_TRANSLATION.),CONTEXT_DEPENDENT_MEASURE(1.));
#2271= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2259,#2274,#2272,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2272= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#2274= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.1',(#2256),#105,#35,(
#2270),'');
#2278= SPECIFIED_STATE('SPCVALSTATE_101_21','');
#2279= STATE_RELATIONSHIP(
'SPCVALSTATE_101_21 is related to SPCCASE_11_21_1','',#2258,#2278);
#2280= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2283,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2281= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.)));
#2283= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.2',(#2256),#80,#35,(
#2266),'');
#2287= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2288,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2288= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.3',(#2256),#89,#35,(
#2266),'');
#2292= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2293,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2293= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.4',(#2256),#93,#35,(
#2266),'');
#2297= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2298,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2298= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.5',(#2256),#97,#35,(
#2266),'');
#2302= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2303,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2303= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.6',(#2256),#101,#35,(
#2266),'');
#2307= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2308,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2308= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.7',(#2256),#105,#35,(
#2266),'');
#2312= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2313,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2313= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.8',(#2256),#109,#35,(
#2266),'');
#2317= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2318,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2318= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.9',(#2256),#117,#35,(
#2266),'');
#2322= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2323,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2323= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.10',(#2256),#121,#35,(
#2266),'');
#2327= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2328,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2328= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.11',(#2256),#125,#35,(
#2266),'');
#2332= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2333,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.)));
#2333= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.12',(#2256),#129,#35,(
#2266),'');
#2337= SINGLE POINT CONSTRAINT ELEMENT VALUES(#2278,#2338,#2281,(

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CONTEXT_DEPENDENT_MEASURE(0.));
#2338= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.13',(#2256),#133,#35,(
#2266),'');
#2342= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2343,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.));
#2343= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.14',(#2256),#137,#35,(
#2266),'');
#2347= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2278,#2348,#2281,(
CONTEXT_DEPENDENT_MEASURE(0.));
#2348= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_101.15',(#2256),#141,#35,(
#2266),'');
#2352= STATE_RELATIONSHIP(
'SPCCASE_11_21_1 is related to Step 1 Base Specified State','',#2257,
#2258);
#2353= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_21',
'Overall Factor Combined State');
#2355= STATE_COMPONENT('OverallComp','',#2353,1.);
#2357= SPECIFIED_STATE('LOADSTATECORE_200','Core Loads Specified State'
);
#2358= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#745,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2359= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.)));
#2362= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#841,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2364= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#985,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2366= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#1081,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2368= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#769,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2370= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#793,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2372= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#817,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2374= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#865,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2376= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#961,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2378= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#1009,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2380= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#1033,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2382= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#1057,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2384= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#889,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-125.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2386= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#913,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-125.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2388= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#937,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-125.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2390= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_200',
'Item Factor State');
#2391= STATE_RELATIONSHIP('LOADSTATEITEM_200 is related to OverallComp',
'',#2355,#2390);

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#2392= STATE_COMPONENT('ItemComp_21_200','',#2390,1.);
#2394= STATE_RELATIONSHIP(
'LOADSTATECORE_200 is related to ItemComp_21_200','',#2392,#2357);
#2395= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_21 is related to Step 1 Base Specified State','',
#2257,#2353);
#2396= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 1','',
#2257);
#2397= OUTPUT_REQUEST_STATE('Step 1 Output Request State','',(#2256));
#2399= NODAL_FREEDOM_VALUES(#2397,#2403,#35,#2400,(UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.)));
#2400= FREEDOMS_LIST((ENUMERATED_DEGREE_OF_FREEDOM(.X_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Y_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.Z_TRANSLATION.),
ENUMERATED_DEGREE_OF_FREEDOM(.X_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(
.Y_ROTATION.),ENUMERATED_DEGREE_OF_FREEDOM(.Z_ROTATION.));
#2403= NODE_GROUP('','ALL',#67,(#80,#89,#93,#97,#101,#105,#109,#113,#117
,#121,#125,#129,#133,#137,#141,#145,#149,#153,#157,#161,#165,#169,#173,
#177,#181,#185,#189,#193,#197,#201,#205,#209,#213,#217,#221,#225,#229,
#233,#237,#241,#245,#249,#253,#257,#261,#265,#269,#273,#277,#281,#285,
#289,#293,#297,#301,#305,#309,#313,#317,#321,#325,#329,#333,#337,#341,
#345,#349,#353,#357,#361,#365,#369,#373,#377,#381,#385,#389,#393,#397,
#401,#405,#409,#413,#417,#421,#425,#429,#433,#437,#441,#445,#449,#453,
#457,#461,#465,#469,#473,#477,#481,#485,#489,#493,#497,#501,#505,#509,
#513,#517,#521,#525,#529,#533,#537,#541,#545,#549,#553,#557,#561,#565,
#569,#573,#577,#581,#585,#589,#593,#597,#601,#605,#609,#613,#617,#621,
#625,#629,#633,#637,#641,#645,#649,#653,#657,#661,#665,#669,#673,#677,
#681,#685,#689,#693,#697,#701,#705,#709,#713,#717,#721,#725,#729,#733,
#737,#741,#745,#749,#753,#757,#761,#765,#769,#773,#777,#781,#785,#789,
#793,#797,#801,#805,#809,#813,#817,#821,#825,#829,#833,#837,#841,#845,
#849,#853,#857,#861,#865,#869,#873,#877,#881,#885,#889,#893,#897,#901,
#905,#909,#913,#917,#921,#925,#929,#933,#937,#941,#945,#949,#953,#957,
#961,#965,#969,#973,#977,#981,#985,#989,#993,#997,#1001,#1005,#1009,
#1013,#1017,#1021,#1025,#1029,#1033,#1037,#1041,#1045,#1049,#1053,#1057,
#1061,#1065,#1069,#1073,#1077,#1081,#1085,#1089,#1093,#1097,#1101);
#2404= ID_ATTRIBUTE('ALL',#2403);
#2406= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2397,#1145,.F.,
(#2407,#2417,#2421,#2425,#2429,#2433,#2437,#2441,#2445),
VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2407= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2408,$);
#2408= VOLUME_ELEMENT_LOCATION(#2409);
#2409= FEA_PARAMETRIC_POINT('sHexN_0',(0.,0.,0.));
#2411= REPRESENTATION('dpr0',(#2409,#2419,#2423,#2427,#2431,#2435,#2439,
#2443,#2447,#2452,#2457,#2461,#2465,#2469,#2474,#2479,#2483,#2487,#2491,
#2495,#2499),#2412);
#2412= PARAMETRIC_REPRESENTATION_CONTEXT('FEA parametric context',
'Parametric');
#2417= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2418,$);
#2418= VOLUME_ELEMENT_LOCATION(#2419);
#2419= FEA_PARAMETRIC_POINT('sHexN_1',(-1.,-1.,-1.));
#2421= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2422,$);
#2422= VOLUME_ELEMENT_LOCATION(#2423);
#2423= FEA_PARAMETRIC_POINT('sHexN_2',(1.,-1.,-1.));
#2425= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2426,$);
#2426= VOLUME_ELEMENT_LOCATION(#2427);
#2427= FEA_PARAMETRIC_POINT('sHexN_3',(1.,1.,-1.));
#2429= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2430,$);
#2430= VOLUME_ELEMENT_LOCATION(#2431);
#2431= FEA_PARAMETRIC_POINT('sHexN_4',(-1.,1.,-1.));
#2433= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2434,$);
#2434= VOLUME_ELEMENT_LOCATION(#2435);
#2435= FEA_PARAMETRIC_POINT('sHexN_5',(-1.,-1.,1.));
#2437= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(

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.UNSPECIFIED.),#2438,$);
#2438= VOLUME_ELEMENT_LOCATION(#2439);
#2439= FEA_PARAMETRIC_POINT('sHexN_6',(1.,-1.,1.));
#2441= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2442,$);
#2442= VOLUME_ELEMENT_LOCATION(#2443);
#2443= FEA_PARAMETRIC_POINT('sHexN_7',(1.,1.,1.));
#2445= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2446,$);
#2446= VOLUME_ELEMENT_LOCATION(#2447);
#2447= FEA_PARAMETRIC_POINT('sHexN_8',(-1.,1.,1.));
#2449= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2397,#1243,.F.,
(#2450,#2455,#2459,#2463,#2467),VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2450= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2451,$);
#2451= VOLUME_ELEMENT_LOCATION(#2452);
#2452= FEA_PARAMETRIC_POINT('sTetN_0',(0.,0.,0.));
#2455= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2456,$);
#2456= VOLUME_ELEMENT_LOCATION(#2457);
#2457= FEA_PARAMETRIC_POINT('sTetN_1',(-1.,-1.,-1.));
#2459= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2460,$);
#2460= VOLUME_ELEMENT_LOCATION(#2461);
#2461= FEA_PARAMETRIC_POINT('sTetN_2',(1.,-1.,-1.));
#2463= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2464,$);
#2464= VOLUME_ELEMENT_LOCATION(#2465);
#2465= FEA_PARAMETRIC_POINT('sTetN_3',(-1.,1.,-1.));
#2467= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2468,$);
#2468= VOLUME_ELEMENT_LOCATION(#2469);
#2469= FEA_PARAMETRIC_POINT('sTetN_4',(-1.,-1.,1.));
#2471= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2397,#1965,.F.,
(#2472,#2477,#2481,#2485,#2489,#2493,#2497),VOLUME_TENSOR2_3D_VARIABLE(
.STRESS.));
#2472= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2473,$);
#2473= VOLUME_ELEMENT_LOCATION(#2474);
#2474= FEA_PARAMETRIC_POINT('sWedN_0',(0.,0.,0.));
#2477= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2478,$);
#2478= VOLUME_ELEMENT_LOCATION(#2479);
#2479= FEA_PARAMETRIC_POINT('sWedN_1',(-1.,-1.,-1.));
#2481= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2482,$);
#2482= VOLUME_ELEMENT_LOCATION(#2483);
#2483= FEA_PARAMETRIC_POINT('sWedN_2',(1.,-1.,-1.));
#2485= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2486,$);
#2486= VOLUME_ELEMENT_LOCATION(#2487);
#2487= FEA_PARAMETRIC_POINT('sWedN_3',(-1.,1.,-1.));
#2489= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2490,$);
#2490= VOLUME_ELEMENT_LOCATION(#2491);
#2491= FEA_PARAMETRIC_POINT('sWedN_4',(-1.,-1.,1.));
#2493= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2494,$);
#2494= VOLUME_ELEMENT_LOCATION(#2495);
#2495= FEA_PARAMETRIC_POINT('sWedN_5',(1.,-1.,1.));
#2497= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2498,$);
#2498= VOLUME_ELEMENT_LOCATION(#2499);
#2499= FEA_PARAMETRIC_POINT('sWedN_6',(-1.,1.,1.));
#2501= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#2252,'STATIC STEP 2',2,#2255
,'',#2647);
#2502= SPECIFIED_STATE('Step 2 Base Specified State',
'Relating Specified State');
#2503= SPECIFIED_STATE('SPCCASE_12_22_2','Aggregator SPC 12 Step 2');
#2504= SPECIFIED_STATE('SPCVALSTATE_100_22','');
#2505= STATE_RELATIONSHIP(

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'SPCVALSTATE_100_22 is related to SPCCASE_12_22_2','',#2503,#2504);
#2506= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2504,#2507,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2507= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.16',(#2501),#113,#35,(
#2266,#2269,#2270),'');
#2511= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2504,#2512,#2272,(
CONTEXT_DEPENDENT_MEASURE(0.));
#2512= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.17',(#2501),#105,#35,(
#2270),'');
#2516= SPECIFIED_STATE('SPCVALSTATE_102_22','');
#2517= STATE_RELATIONSHIP(
'SPCVALSTATE_102_22 is related to SPCCASE_12_22_2','',#2503,#2516);
#2518= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2519,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2519= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.18',(#2501),#80,#35,(
#2266,#2269,#2270),'');
#2523= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2524,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2524= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.19',(#2501),#89,#35,(
#2266,#2269,#2270),'');
#2528= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2529,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2529= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.20',(#2501),#93,#35,(
#2266,#2269,#2270),'');
#2533= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2534,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2534= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.21',(#2501),#97,#35,(
#2266,#2269,#2270),'');
#2538= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2539,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2539= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.22',(#2501),#101,#35,(
#2266,#2269,#2270),'');
#2543= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2544,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2544= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.23',(#2501),#105,#35,(
#2266,#2269,#2270),'');
#2548= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2549,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2549= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.24',(#2501),#109,#35,(
#2266,#2269,#2270),'');
#2553= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2554,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2554= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.25',(#2501),#117,#35,(
#2266,#2269,#2270),'');
#2558= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2559,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2559= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.26',(#2501),#121,#35,(
#2266,#2269,#2270),'');
#2563= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2564,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2564= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.27',(#2501),#125,#35,(
#2266,#2269,#2270),'');
#2568= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2569,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2569= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.28',(#2501),#129,#35,(
#2266,#2269,#2270),'');
#2573= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2574,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));

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#2574= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.29',(#2501),#133,#35,(
#2266,#2269,#2270),'');
#2578= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2579,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2579= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.30',(#2501),#137,#35,(
#2266,#2269,#2270),'');
#2583= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2516,#2584,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2584= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.31',(#2501),#141,#35,(
#2266,#2269,#2270),'');
#2588= STATE_RELATIONSHIP(
'SPCCASE_12_22_2 is related to Step 2 Base Specified State','',#2502,
#2503);
#2589= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_22',
'Overall Factor Combined State');
#2590= STATE_COMPONENT('OverallComp','',#2589,1.);
#2592= SPECIFIED_STATE('LOADSTATECORE_300','Core Loads Specified State'
);
#2593= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#385,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-2.5),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2595= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#625,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-2.5),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2597= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#745,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-2.5),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2599= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#985,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-2.5),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2601= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#505,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2603= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#765,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2605= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#753,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2607= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#757,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2609= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#761,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2611= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#749,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2613= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#865,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2615= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#989,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2617= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#993,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2619= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#997,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2621= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#1001,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2623= NODAL_FREEDOM_ACTION_DEFINITION(#2592,#1005,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-5.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2625= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_300',
'Item Factor State');
#2626= STATE_RELATIONSHIP('LOADSTATEITEM 300 is related to OverallComp',

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',#2590,#2625);
#2627= STATE_COMPONENT('ItemComp_22_300','',#2625,1.);
#2629= STATE_RELATIONSHIP(
'LOADSTATECORE_300 is related to ItemComp_22_300','',#2627,#2592);
#2630= SPECIFIED_STATE('LOADSTATECORE_400','Core Loads Specified State'
);
#2631= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#869,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2633= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#873,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2635= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#877,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2637= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#881,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2639= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#885,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2641= LINEARLY_SUPERIMPOSED_STATE('LOADSTATEITEM_400',
'Item Factor State');
#2642= STATE_RELATIONSHIP('LOADSTATEITEM_400 is related to OverallComp',
',#2590,#2641);
#2643= STATE_COMPONENT('ItemComp_22_400','',#2641,1.);
#2645= STATE_RELATIONSHIP(
'LOADSTATECORE_400 is related to ItemComp_22_400','',#2643,#2630);
#2646= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_22 is related to Step 2 Base Specified State','',
#2502,#2589);
#2647= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 2','',
#2502);
#2648= OUTPUT_REQUEST_STATE('Step 2 Output Request State','',(#2501));
#2650= NODAL_FREEDOM_VALUES(#2648,#2403,#35,#2400,(UNSPECIFIED_VALUE(
UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.),UNSPECIFIED_VALUE(
.UNSPECIFIED.),UNSPECIFIED_VALUE(.UNSPECIFIED.)));
#2652= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2648,#1145,.F.,
(#2653,#2655,#2656,#2657,#2658,#2659,#2660,#2661,#2662),
VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2653= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2408,$);
#2655= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2418,$);
#2656= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2422,$);
#2657= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2426,$);
#2658= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2430,$);
#2659= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2434,$);
#2660= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2438,$);
#2661= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2442,$);
#2662= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2446,$);
#2663= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2648,#1243,.F.,
(#2664,#2666,#2667,#2668,#2669),VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2664= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2451,$);
#2666= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2456,$);
#2667= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2460,$);
#2668= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2464,$);
#2669= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2468,$);

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#2670= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2648,#1965,.F.,
(#2671,#2673,#2674,#2675,#2676,#2677,#2678),VOLUME_TENSOR2_3D_VARIABLE(
.STRESS.));
#2671= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2473,$);
#2673= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2478,$);
#2674= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2482,$);
#2675= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2486,$);
#2676= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2490,$);
#2677= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2494,$);
#2678= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2498,$);
#2679= CONTROL_LINEAR_STATIC_ANALYSIS_STEP(#2252,'STATIC STEP 3',3,#2255
,',',#2780);
#2680= SPECIFIED_STATE('Step 3 Base Specified State',
'Relating Specified State');
#2681= SPECIFIED_STATE('SPCCASE_12_23_3','Aggregator SPC 12 Step 3');
#2682= SPECIFIED_STATE('SPCVALSTATE_100_23','');
#2683= STATE_RELATIONSHIP(
'SPCVALSTATE_100_23 is related to SPCCASE_12_23_3','',#2681,#2682);
#2684= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2682,#2685,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2685= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.32',(#2679),#113,#35,(
#2266,#2269,#2270),'');
#2689= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2682,#2690,#2272,(
CONTEXT_DEPENDENT_MEASURE(0.));
#2690= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_100.33',(#2679),#105,#35,(
#2270),'');
#2694= SPECIFIED_STATE('SPCVALSTATE_102_23','');
#2695= STATE_RELATIONSHIP(
'SPCVALSTATE_102_23 is related to SPCCASE_12_23_3','',#2681,#2694);
#2696= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2697,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2697= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.34',(#2679),#80,#35,(
#2266,#2269,#2270),'');
#2701= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2702,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2702= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.35',(#2679),#89,#35,(
#2266,#2269,#2270),'');
#2706= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2707,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2707= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.36',(#2679),#93,#35,(
#2266,#2269,#2270),'');
#2711= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2712,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2712= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.37',(#2679),#97,#35,(
#2266,#2269,#2270),'');
#2716= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2717,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2717= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.38',(#2679),#101,#35,(
#2266,#2269,#2270),'');
#2721= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2722,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2722= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.39',(#2679),#105,#35,(
#2266,#2269,#2270),'');
#2726= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2727,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2727= SINGLE POINT CONSTRAINT ELEMENT('SPC1_102.40',(#2679),#109,#35,(

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#2266,#2269,#2270),'');
#2731= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2732,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2732= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.41',(#2679),#117,#35,(
#2266,#2269,#2270),'');
#2736= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2737,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2737= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.42',(#2679),#121,#35,(
#2266,#2269,#2270),'');
#2741= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2742,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2742= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.43',(#2679),#125,#35,(
#2266,#2269,#2270),'');
#2746= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2747,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2747= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.44',(#2679),#129,#35,(
#2266,#2269,#2270),'');
#2751= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2752,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2752= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.45',(#2679),#133,#35,(
#2266,#2269,#2270),'');
#2756= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2757,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2757= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.46',(#2679),#137,#35,(
#2266,#2269,#2270),'');
#2761= SINGLE_POINT_CONSTRAINT_ELEMENT_VALUES(#2694,#2762,#2262,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.));
#2762= SINGLE_POINT_CONSTRAINT_ELEMENT('SPC1_102.47',(#2679),#141,#35,(
#2266,#2269,#2270),'');
#2766= STATE_RELATIONSHIP(
'SPCCASE_12_23_3 is related to Step 3 Base Specified State','',#2680,
#2681);
#2767= LINEARLY_SUPERIMPOSED_STATE('LOADSTATECOMBINATION_23',
'Overall Factor Combined State');
#2768= STATE_COMPONENT('OverallComp','',#2767,1.);
#2770= STATE_RELATIONSHIP('LOADSTATEITEM_200 is related to OverallComp',
'',#2768,#2390);
#2771= STATE_COMPONENT('ItemComp_23_200','',#2390,1.);
#2772= STATE_RELATIONSHIP(
'LOADSTATECORE_200 is related to ItemComp_23_200','',#2771,#2357);
#2773= STATE_RELATIONSHIP('LOADSTATEITEM_300 is related to OverallComp',
'',#2768,#2625);
#2774= STATE_COMPONENT('ItemComp_23_300','',#2625,1.);
#2775= STATE_RELATIONSHIP(
'LOADSTATECORE_300 is related to ItemComp_23_300','',#2774,#2592);
#2776= STATE_RELATIONSHIP('LOADSTATEITEM_400 is related to OverallComp',
'',#2768,#2641);
#2777= STATE_COMPONENT('ItemComp_23_400','',#2641,1.);
#2778= STATE_RELATIONSHIP(
'LOADSTATECORE_400 is related to ItemComp_23_400','',#2777,#2630);
#2779= STATE_RELATIONSHIP(
'LOADSTATECOMBINATION_23 is related to Step 3 Base Specified State','',
#2680,#2767);
#2780= CONTROL_LINEAR_STATIC_LOAD_INCREMENT_PROCESS('STATIC STEP 3','',
#2680);
#2781= OUTPUT_REQUEST_STATE('Step 3 Output Request State','',(#2679));
#2783= NODAL_FREEDOM_VALUES(#2781,#2403,#35,#2400,(UNSPECIFIED_VALUE(
UNSPECIFIED.),UNSPECIFIED_VALUE(UNSPECIFIED.),UNSPECIFIED_VALUE(
UNSPECIFIED.),UNSPECIFIED_VALUE(UNSPECIFIED.),UNSPECIFIED_VALUE(
UNSPECIFIED.),UNSPECIFIED_VALUE(UNSPECIFIED.)));
#2785= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2781,#1145,.F.,
(#2786,#2788,#2789,#2790,#2791,#2792,#2793,#2794,#2795),
VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2786= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(

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.UNSPECIFIED.),#2408,$);
#2788= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2418,$);
#2789= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2422,$);
#2790= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2426,$);
#2791= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2430,$);
#2792= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2434,$);
#2793= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2438,$);
#2794= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2442,$);
#2795= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2446,$);
#2796= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2781,#1243,.F.,
(#2797,#2799,#2800,#2801,#2802),VOLUME_TENSOR2_3D_VARIABLE(.STRESS.));
#2797= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2451,$);
#2799= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2456,$);
#2800= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2460,$);
#2801= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2464,$);
#2802= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2468,$);
#2803= VOLUME_3D_ELEMENT_LOCATION_POINT_VARIABLE_VALUES(#2781,#1965,.F.,
(#2804,#2806,#2807,#2808,#2809,#2810,#2811),VOLUME_TENSOR2_3D_VARIABLE(
.STRESS.));
#2804= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2473,$);
#2806= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2478,$);
#2807= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2482,$);
#2808= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2486,$);
#2809= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2490,$);
#2810= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2494,$);
#2811= VOLUME_3D_ELEMENT_VALUE_AND_LOCATION(UNSPECIFIED_VALUE(
.UNSPECIFIED.),#2498,$);
#2812= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#745,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2814= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#841,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2816= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#985,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2818= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#1081,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-31.25),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2820= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#769,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2822= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#793,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2824= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#817,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2826= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#865,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(-62.5),CONTEXT_DEPENDENT_MEASURE(0.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2828= NODAL_FREEDOM_ACTION_DEFINITION(#2357,#961,#35,#2359,(

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#2876= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#873,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2878= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#877,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2880= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#881,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
#2882= NODAL_FREEDOM_ACTION_DEFINITION(#2630,#885,#35,#2359,(
CONTEXT_DEPENDENT_MEASURE(0.),CONTEXT_DEPENDENT_MEASURE(-10.),
CONTEXT_DEPENDENT_MEASURE(0.)),.APPLIED_LOADS.);
ENDSEC;

END-ISO-10303-21;
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